MAE 545: Lecture 7 (2/28)

Shapes of growing sheets

Reminder: no lecture on Thursday (3/2)

Shapes of flowers and leaves

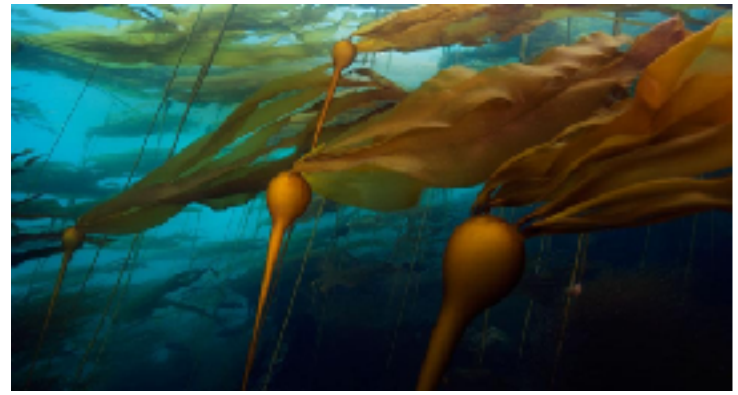
saddles

wrinkled edges

helices

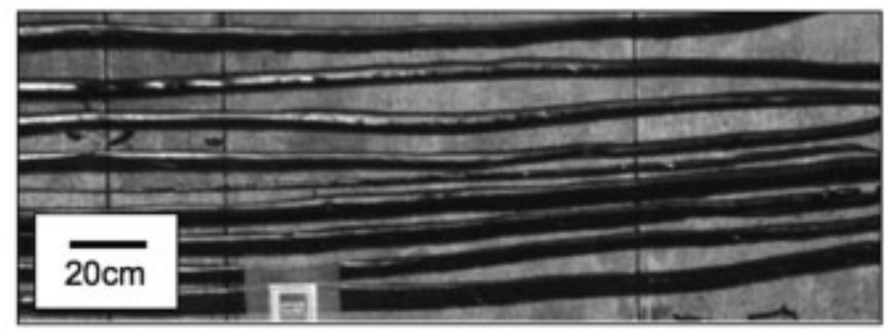
Wrinkled and straight blades in macroalgae

bull kelp
(seaweed)



Slow water flow environment (v~0.5 m/s)

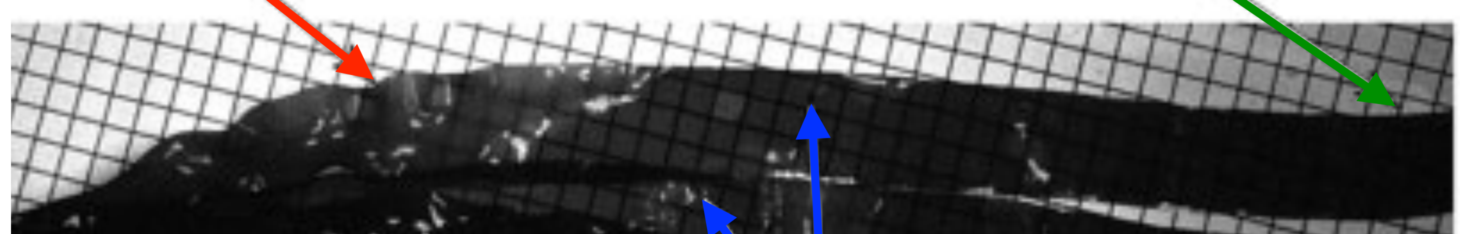
Fast water flow environment (v~1.5 m/s)



new growth after transplantation (wrinkled)

old growth before transplanted (flat)

Transplantation of blade from one environment to the other changes morphology!

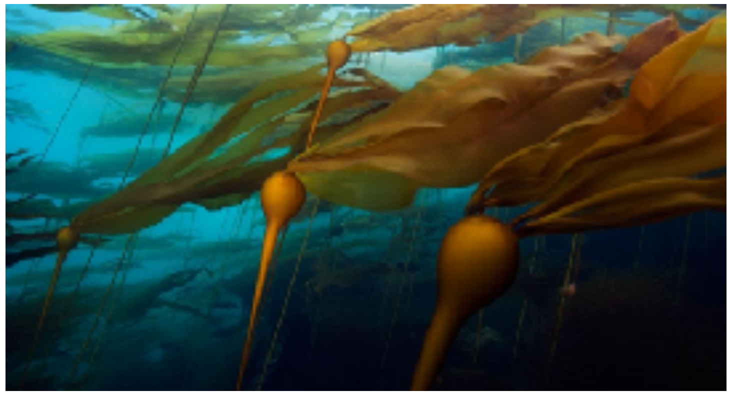


blades

M. Koehl et al., Integ. Comp. Biol. 48, 834 (2008)

Wrinkled and straight blades in macroalgae

bull kelp (seaweed)



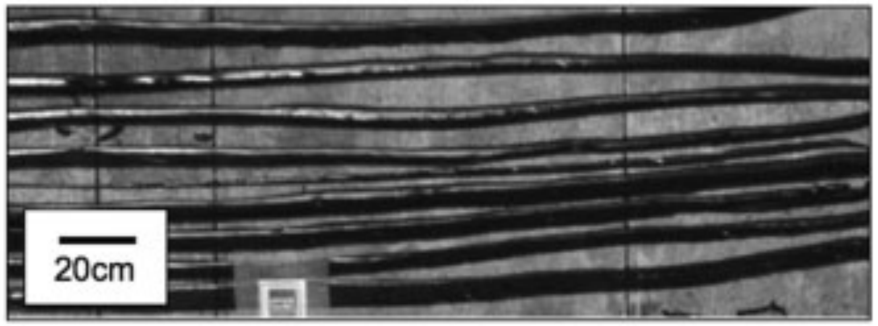
Slow water flow environment (v~0.5 m/s)

increased drag

blades flap like flags

flapping prevents bundling of blades, which can thus receive more sunlight (photosynthesis)

Fast water flow environment (v~1.5 m/s)



reduced drag to prevent detachment from base (=death)

minimal flapping

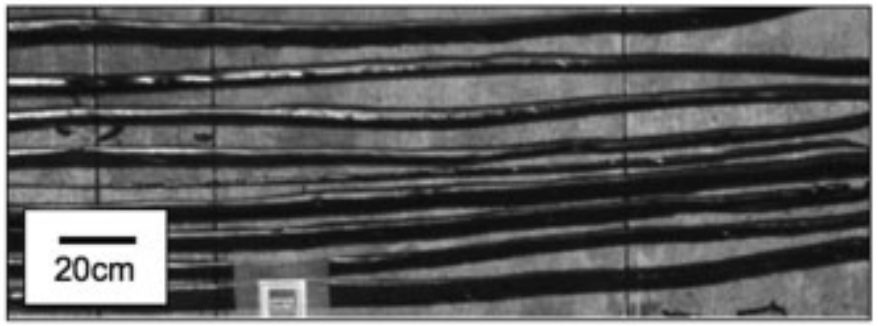
blades bundle together and some blades on the bottom receive less sunlight

M. Koehl et al., Integ. Comp. Biol. 48, 834 (2008)

Wrinkled and straight blades in macroalgae

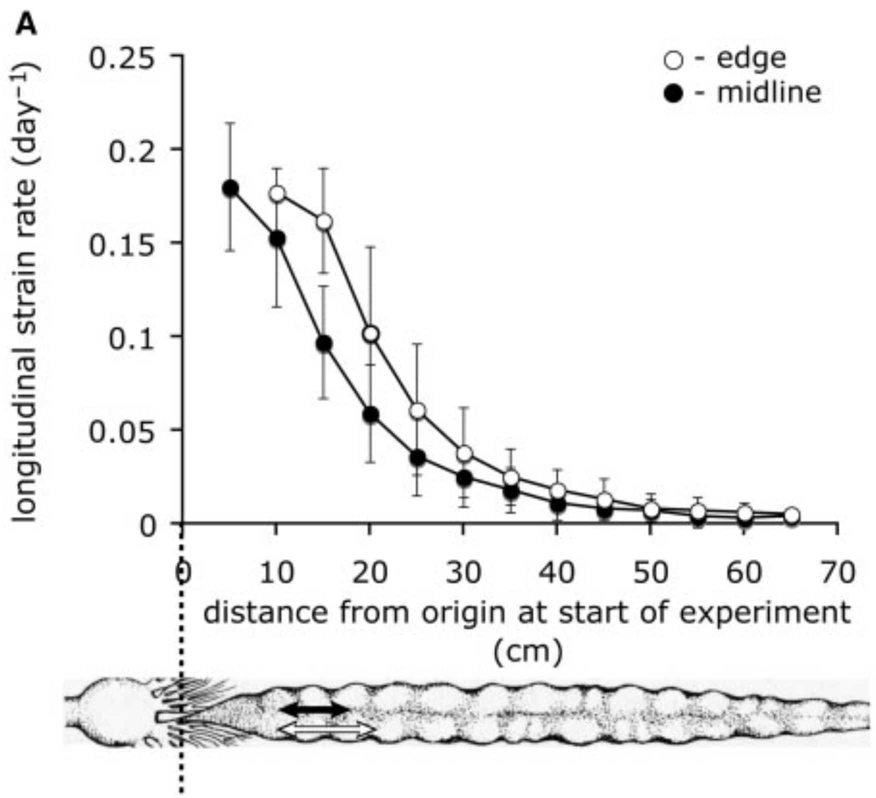
Slow water flow environment (v~0.5 m/s)

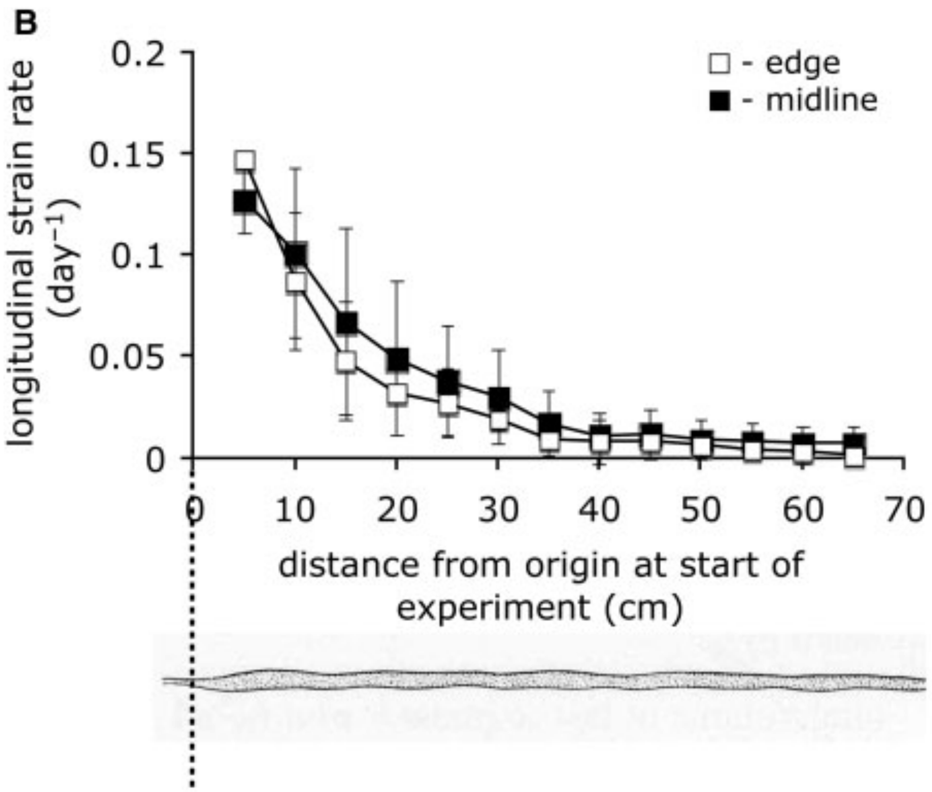
Fast water flow environment (v~1.5 m/s)



edges of blades grow faster than the midline

edges of blades grow at the same speed as the midline





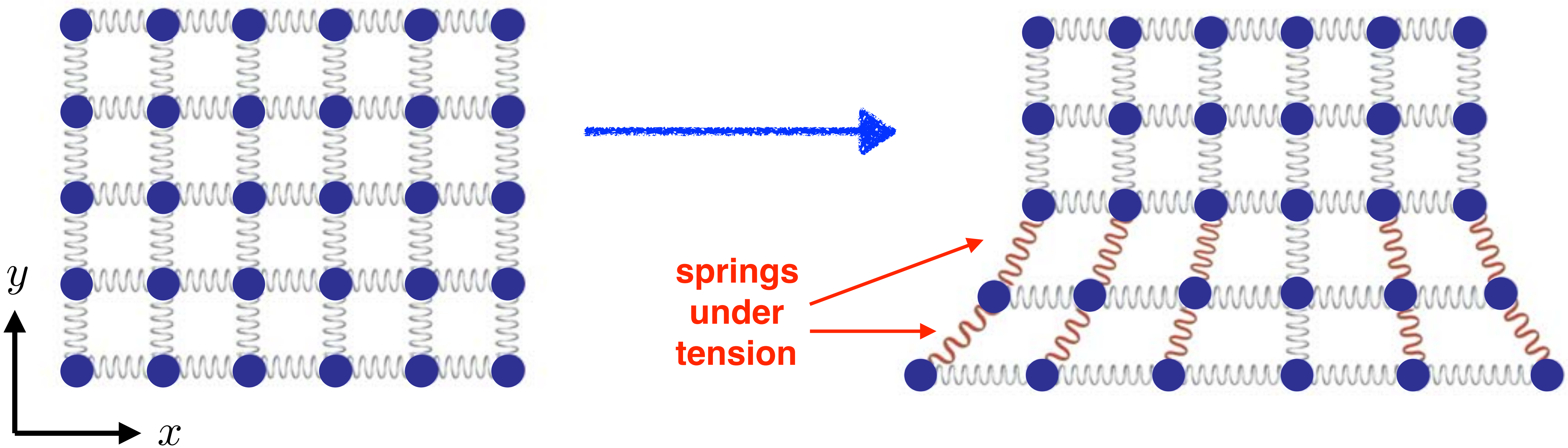
What is the effect of differential growth rate between the edge and the midline of the blade?

M. Koehl et al., Integ. Comp. Biol. 48, 834 (2008)

Differential growth produces internal stress

before growth

faster growth of the bottom edge in x direction



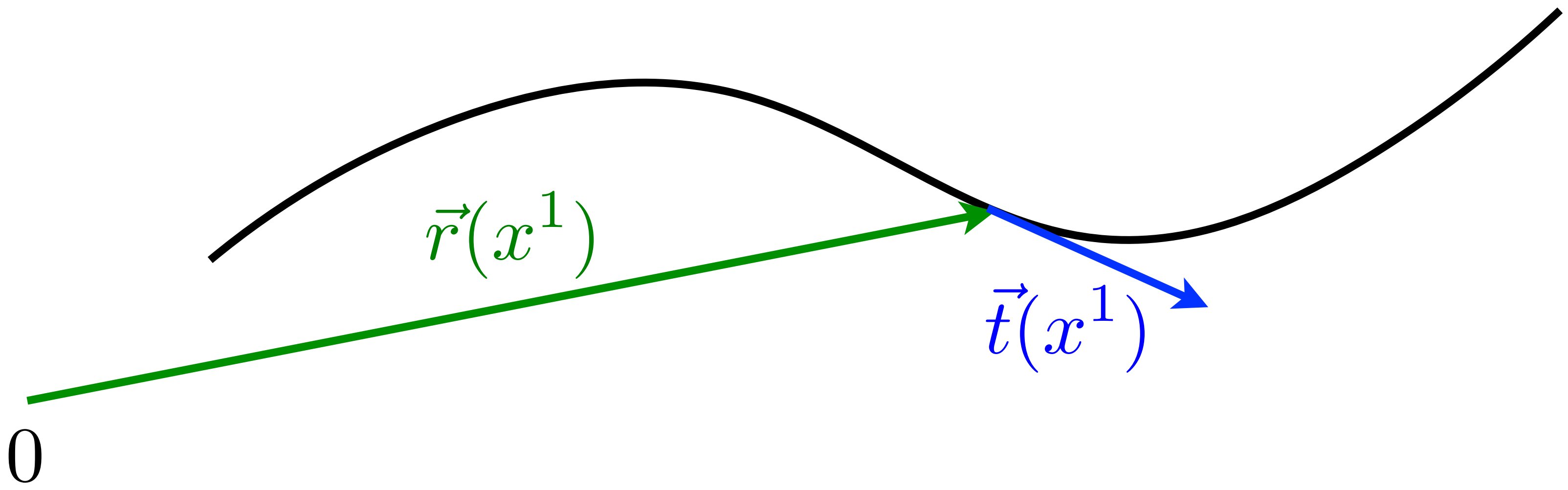
Differential growth produces internal stresses, which can be partially released via bending!

Next: Short detour to differential geometry.

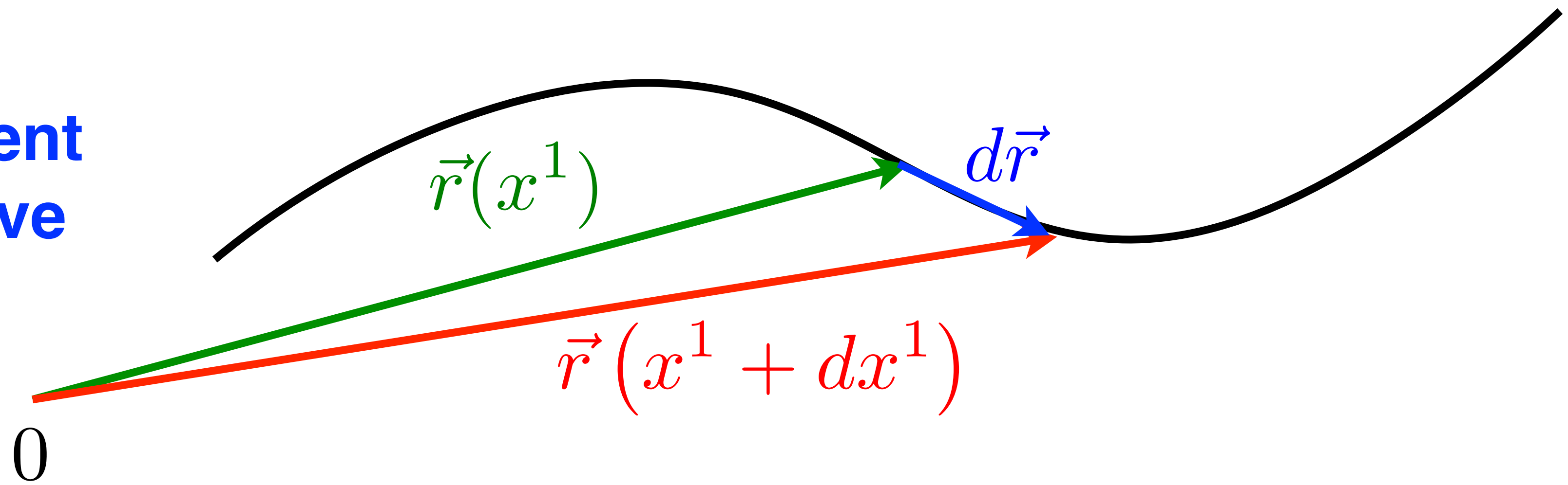
Metric for measuring distances along curves

x^1 **parameter describing position along the curve**

$\vec{r}(x^1)$ **function describing shape of the curve**



$$\vec{t}(x^1) = \frac{d\vec{r}(x^1)}{dx^1}$$ **local tangent to the curve**



metric for measuring lengths

$$d\ell^2 = d\vec{r}^{\,2} = \vec{t}^{\,2}\left(dx^1\right)^2 = g\,\left(dx^1\right)^2$$

$$g = \vec{t}^{\,2}$$

$$d\ell = \sqrt{g}\,dx^1$$

Natural parametrization corresponds to $g \equiv 1$, where x^1, measures distance along the beam.

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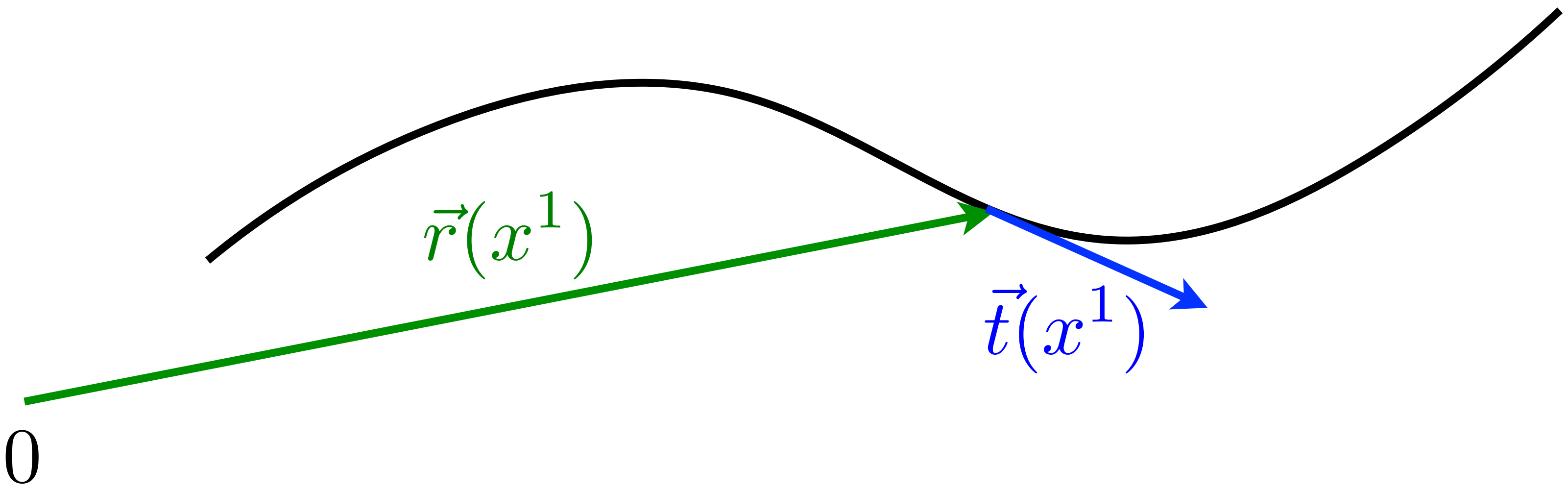

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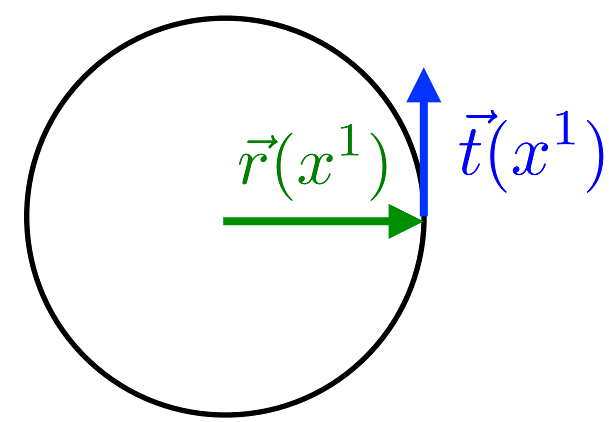
$$g = \vec{t}^{\,2}$$

$$d\ell = \sqrt{g}dx^1$$

Natural parametrization corresponds to $g \equiv 1$, where x^1, measures distance along the beam.

Example



$$\vec{r}(x^1) = R\big(\cos(\omega x^1), \sin(\omega x^1)\big)$$

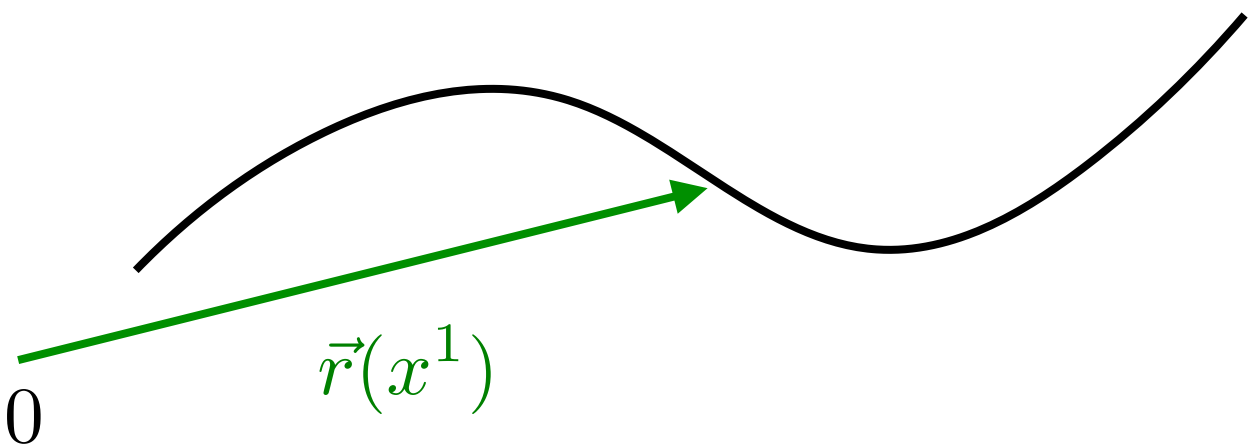
$$\vec{t}(x^1) = R\omega\big(-\sin(\omega x^1), \cos(\omega x^1)\big)$$

$$g(x^1) = R^2\omega^2$$

$$d\ell = R\omega dx^1$$

Strain and energy of beam deformations

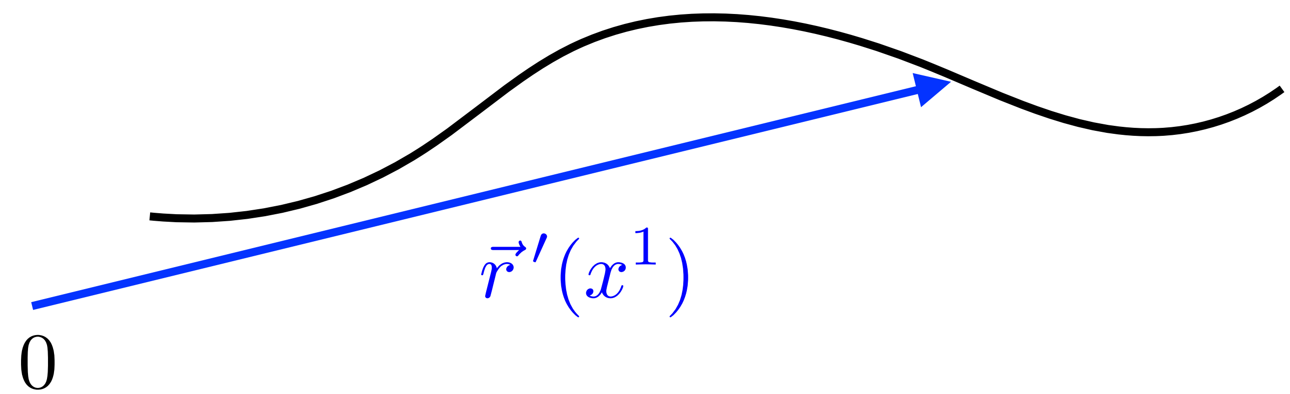
undeformed beam



$$g = \left(d\vec{r}/dx^1\right)^2$$

$$d\ell = \sqrt{g}dx^1$$

deformed beam



$$g' = \left(d\vec{r}\,'/dx^1\right)^2$$

$$d\ell' = \sqrt{g'}dx^1 = d\ell(1+\epsilon)$$

strain

$$d\ell'^2 - d\ell^2 = (2\epsilon + \epsilon^2)d\ell^2 \approx 2\epsilon\, d\ell^2$$

$$\epsilon = \frac{d\ell'^2 - d\ell^2}{2d\ell^2} = \frac{1}{2}g^{-1}\left(g' - g\right)$$

strain measures the difference of metric g' for deformed beam from the preferred metric g !

Energy cost for stretching/compressing

$$U = \int \left(\sqrt{g}dx^1\right)\, \frac{1}{2}k\epsilon^2$$

$$k = EA$$

E **- 3D Young's modulus**

A **- beam cross-section area**

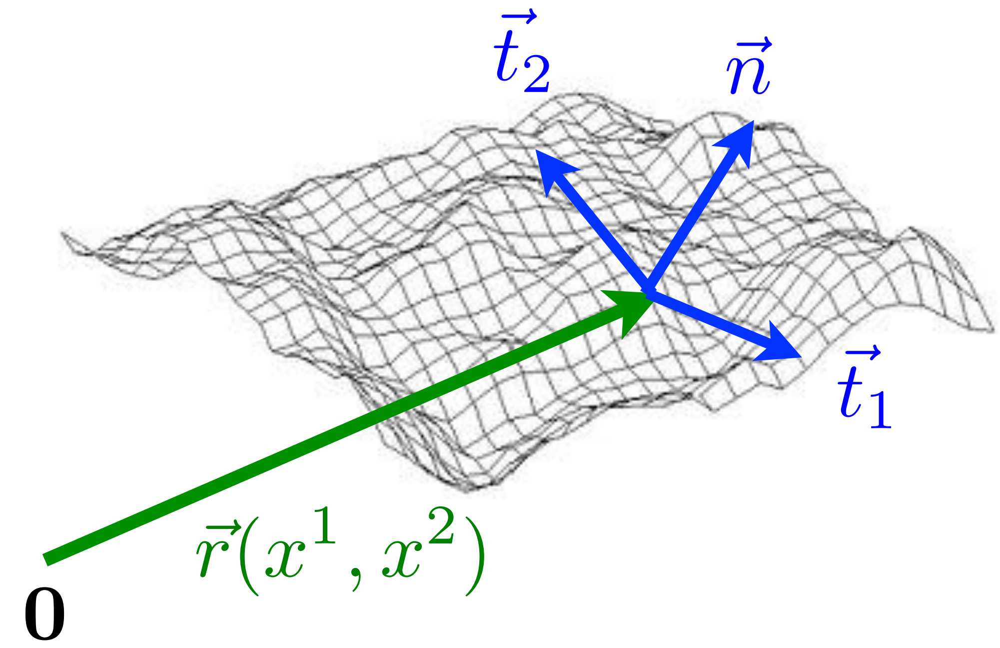
Metric tensor for measuring distances on surfaces

x^1, x^2 **parameters describing position along the surface**

$\vec{r}(x^1, x^2)$ **function describing shape of the surface**

$\vec{t}_i = \frac{\partial \vec{r}}{\partial x^i}$ **local tangent vectors to the surface**

$\vec{n} = \frac{\vec{t}_1 \times \vec{t}_2}{|\vec{t}_1 \times \vec{t}_2|}$ **unit normal vector of the surface**



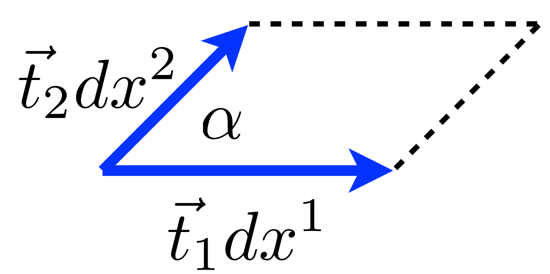
metric tensor for measuring lengths

$$d\ell^2 = d\vec{r}^{\,2} = \sum_{i,j} \vec{t}_i \cdot \vec{t}_j dx^i dx^j = \sum_{i,j} g_{ij} dx^i dx^j$$

$$g_{ij} = \vec{t}_i \cdot \vec{t}_j = \begin{pmatrix} \vec{t}_1 \cdot \vec{t}_1, & \vec{t}_1 \cdot \vec{t}_2 \\ \vec{t}_2 \cdot \vec{t}_1 & \vec{t}_2 \cdot \vec{t}_2 \end{pmatrix}$$

$$g = \det(g_{ij}) = |\vec{t}_1 \times \vec{t}_2|^2$$

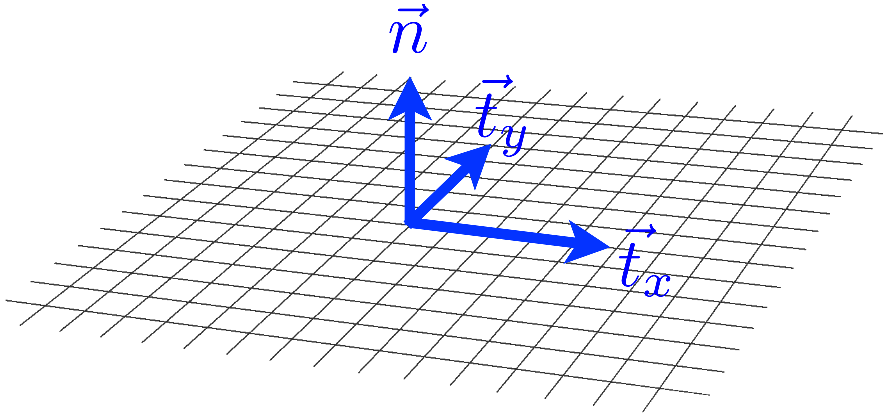
area element



$$dA = |\vec{t}_1||\vec{t}_2| \sin\alpha dx^1 dx^2$$

$$dA = \sqrt{g}\, dx^1 dx^2$$

Examples



$$\vec{r}(x,y) = (x,y,0)$$

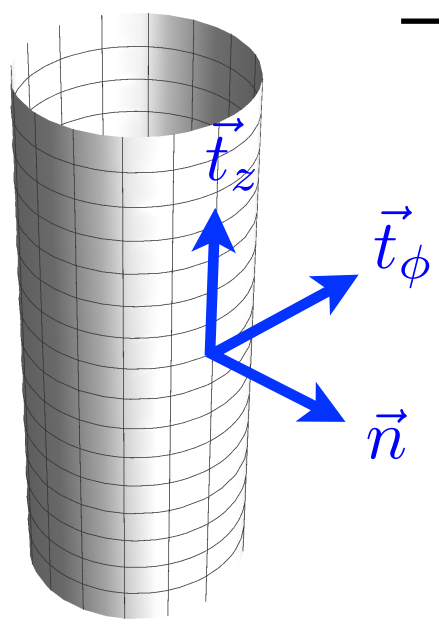
$$\vec{t}_x = \frac{\partial \vec{r}}{\partial x} = (1,0,0)$$

$$\vec{t}_y = \frac{\partial \vec{r}}{\partial y} = (0,1,0)$$

$$\vec{n} = \frac{\vec{t}_x \times \vec{t}_y}{|\vec{t}_x \times \vec{t}_y|} = (0,0,1)$$

$$g_{ij} = \vec{t}_i \cdot \vec{t}_j = \begin{pmatrix} 1, & 0 \\ 0, & 1 \end{pmatrix}$$

$$dA = dxdy$$



$$\vec{r}(\phi,z) = (R\cos\phi, R\sin\phi, z)$$

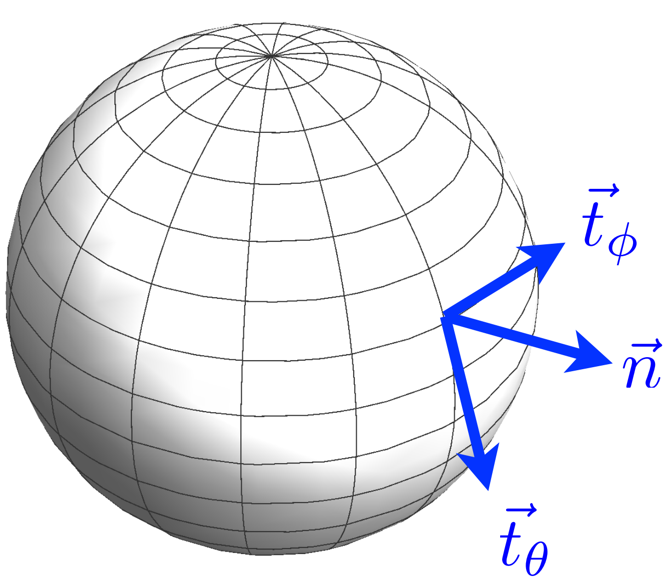
$$\vec{t}_\phi = \frac{\partial \vec{r}}{\partial \phi} = R(-\sin\phi, \cos\phi, 0)$$

$$\vec{t}_z = \frac{\partial \vec{r}}{\partial z} = (0,0,1)$$

$$\vec{n} = \frac{\vec{t}_\phi \times \vec{t}_z}{|\vec{t}_\phi \times \vec{t}_z|} = (\cos\phi, \sin\phi, 0)$$

$$g_{ij} = \vec{t}_i \cdot \vec{t}_j = \begin{pmatrix} R^2, & 0 \\ 0, & 1 \end{pmatrix}$$

$$dA = R\,d\phi dz$$



$$\vec{r}(\theta,\phi) = R(\sin\theta\cos\phi, \sin\theta\sin\phi, \cos\theta)$$

$$\vec{t}_\theta = \frac{\partial \vec{r}}{\partial \theta} = R(\cos\theta\cos\phi, \cos\theta\sin\phi, -\sin\theta)$$

$$\vec{t}_\phi = \frac{\partial \vec{r}}{\partial \phi} = R\sin\theta(-\sin\phi, \cos\phi, 0)$$

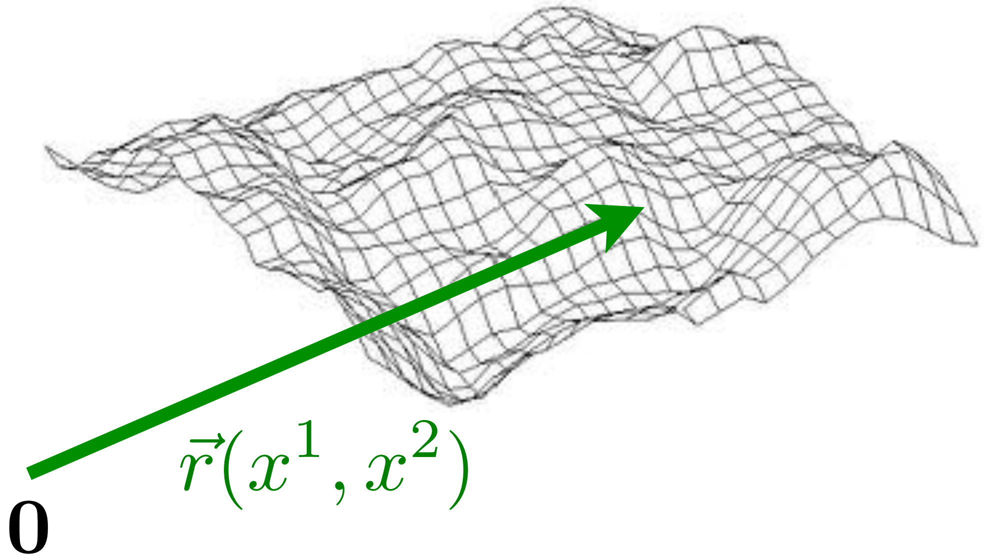
$$\vec{n} = \frac{\vec{t}_\theta \times \vec{t}_\phi}{|\vec{t}_\theta \times \vec{t}_\phi|} = (\sin\theta\cos\phi, \sin\theta\sin\phi, \cos\theta)$$

$$g_{ij} = \vec{t}_i \cdot \vec{t}_j = \begin{pmatrix} R^2, & 0 \\ 0, & R^2\sin^2\theta \end{pmatrix}$$

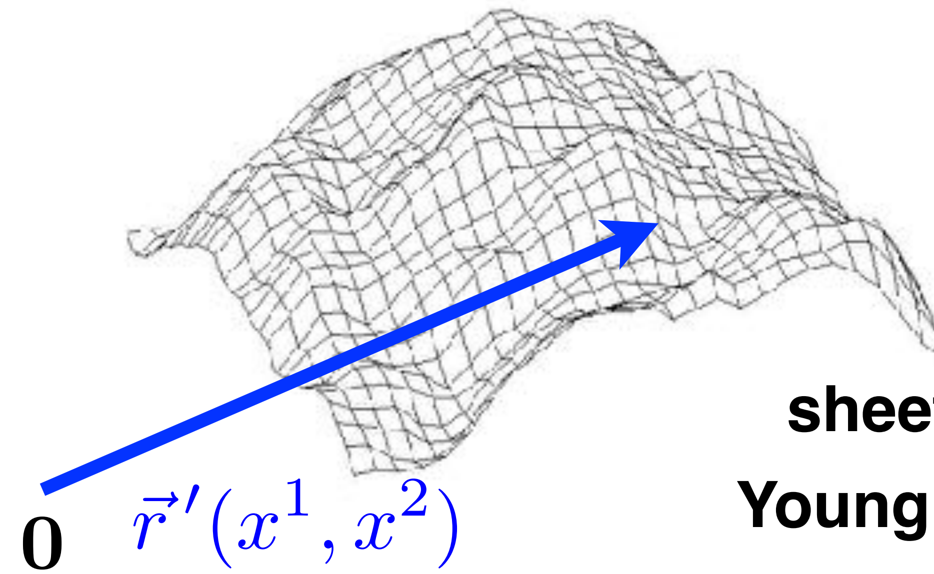
$$dA = R^2\sin\theta\,d\theta d\phi$$

Strain tensor and energy of shell deformations

undeformed shell



deformed shell



sheet thickness d

Young's modulus E

Poisson's ratio ν

$$g_{ij} = \frac{\partial \vec{r}}{\partial x^i} \cdot \frac{\partial \vec{r}}{\partial x^j}$$

$$d\ell^2 = \sum_{i,j} g_{ij} dx^i dx^j$$

$$g'_{ij} = \frac{\partial \vec{r}\,'}{\partial x^i} \cdot \frac{\partial \vec{r}\,'}{\partial x^j}$$

$$d\ell'^2 = \sum_{i,j} g'_{ij} dx^i dx^j$$

strain tensor

$$u_{ij} = \frac{1}{2} \sum_k (g^{-1})_{ik} (g'_{kj} - g_{kj})$$

inverse metric tensor

$$\sum_k (g^{-1})_{ik} g_{kj} = \sum_k g_{ik} (g^{-1})_{kj} = \delta_{ij}$$

Energy cost for stretching, compressing and shearing

$$U = \int (\sqrt{g} dx^1 dx^2)\ \frac{1}{2} \left[\lambda \left(\sum_i u_{ii} \right)^2 + 2\mu \sum_{i,j} u_{ij} u_{ji} \right]$$

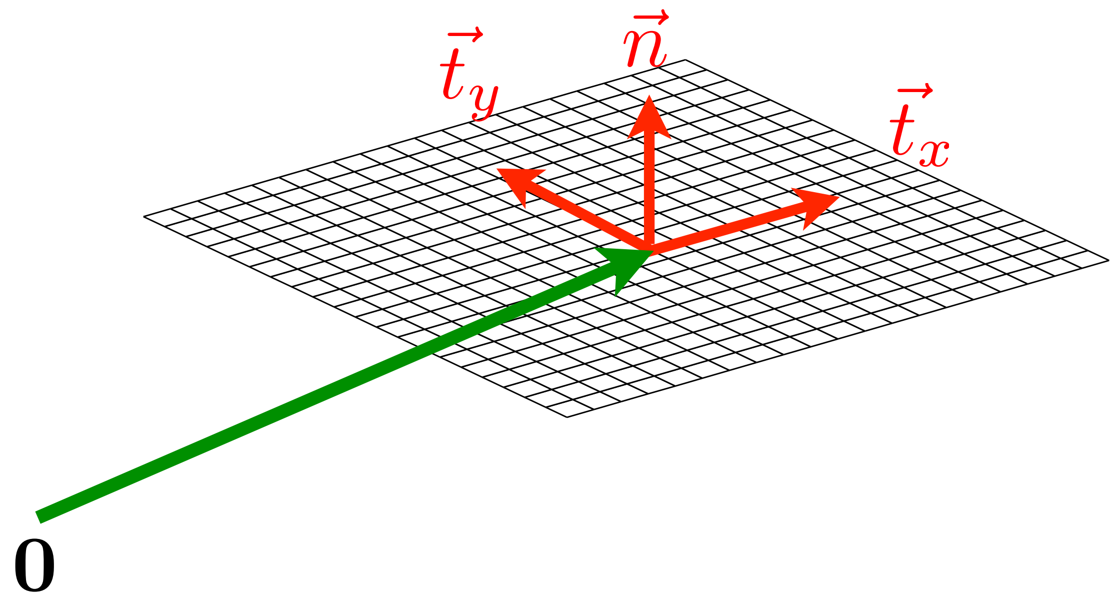
$$g = \det(g_{ij})$$

Lame constants

$$\lambda = \frac{E \nu d}{(1 - \nu^2)} \quad \mu = \frac{E d}{2(1 + \nu)}$$

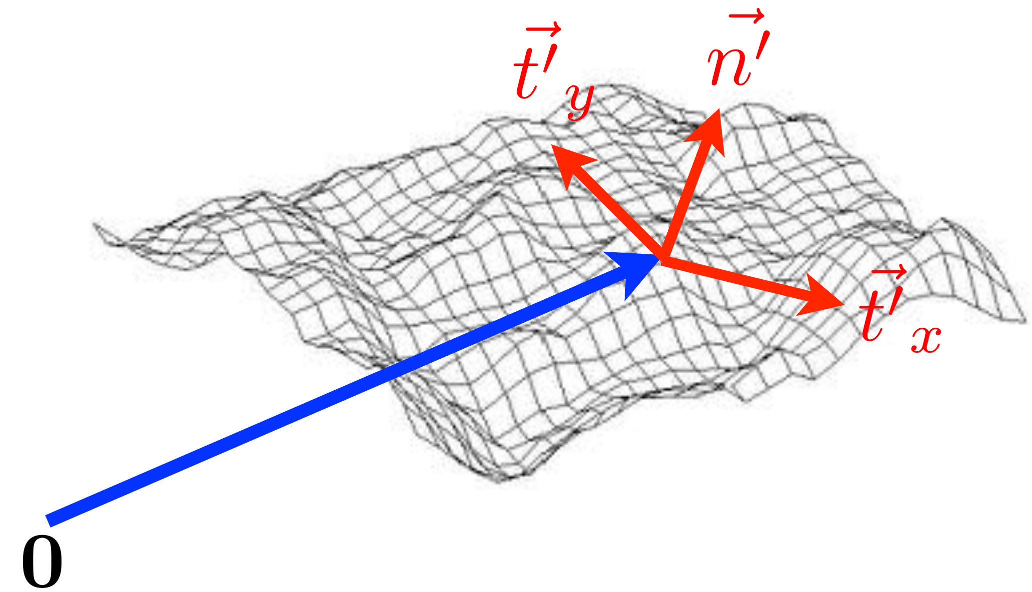
Strain tensor for deformation of flat plates

undeformed plate



$$\vec{r}(x,y) = x\vec{e}_x + y\vec{e}_y$$

deformed plate



$$\vec{r'}(x,y) = \vec{r}(x,y) + u_x(x,y)\vec{e}_x + u_y(x,y)\vec{e}_y + h(x,y)\vec{e}_z$$

$$i, j, k \in \{x, y\}$$

local tangents

$$\vec{t}_i = \partial_i \vec{r} \equiv \frac{\partial \vec{r}}{\partial i} = \vec{e}_i$$

metric tensor

$$g_{ij} = \vec{t}_i \cdot \vec{t}_j = \delta_{ij} \equiv \begin{pmatrix} 1, & 0 \\ 0, & 1 \end{pmatrix}$$

local tangents

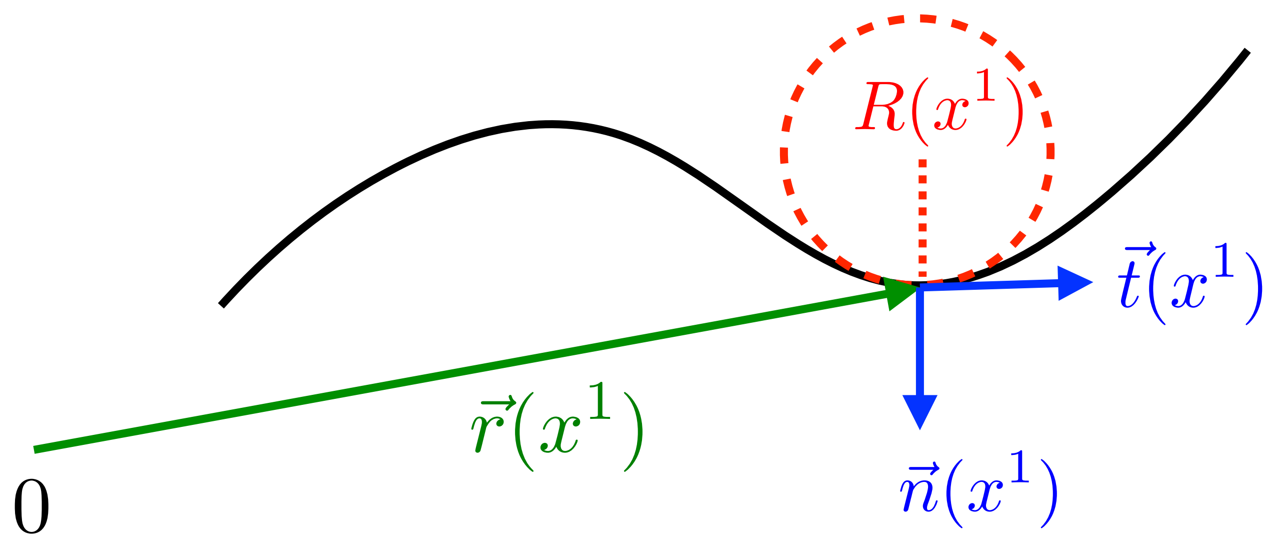
$$\vec{t'}_i = \partial_i \vec{r'} = \vec{e}_i + \sum_k (\partial_i u_k)\vec{e}_k + (\partial_i h)\vec{e}_z$$

strain tensor

$$u_{ij} = \frac{1}{2}\left(g'_{ij} - \delta_{ij}\right)$$

$$2u_{ij} = (\partial_i u_j + \partial_j u_i) + \sum_k \partial_i u_k \partial_j u_k + \partial_i h \partial_j h$$

Curvature of curves



x^1 **parameter describing position along the curve**

$\vec{r}(x^1)$ **function describing shape of the curve**

$$\vec{t}(x^1) = \frac{d\vec{r}(x^1)}{dx^1}$$ **local tangent to the curve**

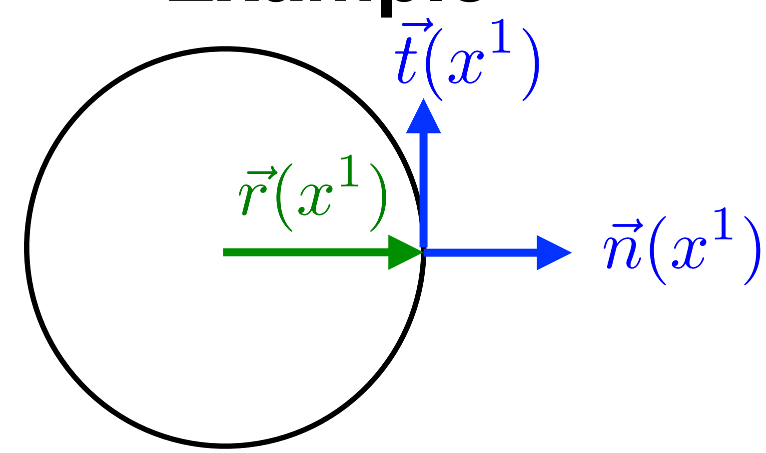
$\vec{n}(x^1)$ **local unit normal vector to the curve**

$g = \vec{t}^{\,2}$ **metric for measuring lengths**

curvature of curve

$$\frac{1}{R} = K = \frac{1}{g}\left(\vec{n} \cdot \frac{d^2\vec{r}}{d(x^1)^2}\right)$$

Example



$$\vec{r}(x^1) = R\big(\cos(\omega x^1), \sin(\omega x^1)\big)$$

$$\vec{n}(x^1) = \big(\cos(\omega x^1), \sin(\omega x^1)\big)$$

$$g(x^1) = R^2\omega^2$$

$$K = -\frac{1}{R}$$

Curvature tensor for surfaces

x^1, x^2 **parameters describing position along the surface**

$\vec{r}(x^1, x^2)$ **function describing shape of the surface**

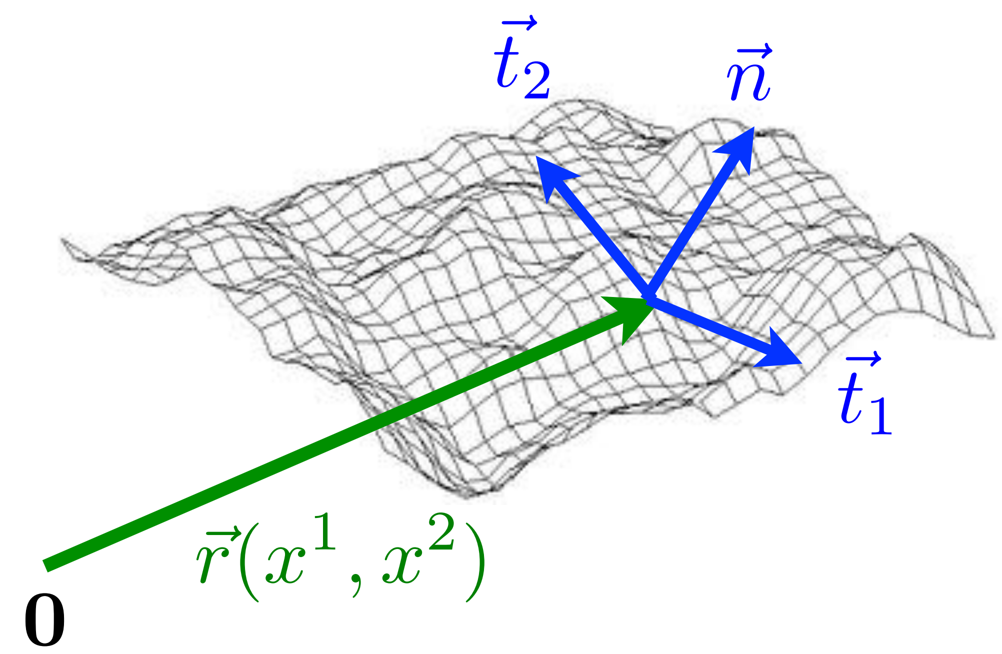
$\vec{t}_i = \frac{\partial \vec{r}}{\partial x^i}$ **local tangent vectors to the surface**

$\vec{n} = \frac{\vec{t}_1 \times \vec{t}_2}{|\vec{t}_1 \times \vec{t}_2|}$ **unit normal vector of the surface**

$g_{ij} = \vec{t}_i \cdot \vec{t}_j$ **metric tensor for measuring lengths**

curvature tensor for surfaces

$$K_{ij} = \sum_k (g^{-1})_{ik} \left(\vec{n} \cdot \frac{\partial^2 \vec{r}}{\partial x^k \partial x^j} \right)$$



principal curvatures correspond to the eigenvalues of curvature tensor

$$\frac{1}{R_1}, \frac{1}{R_2}$$

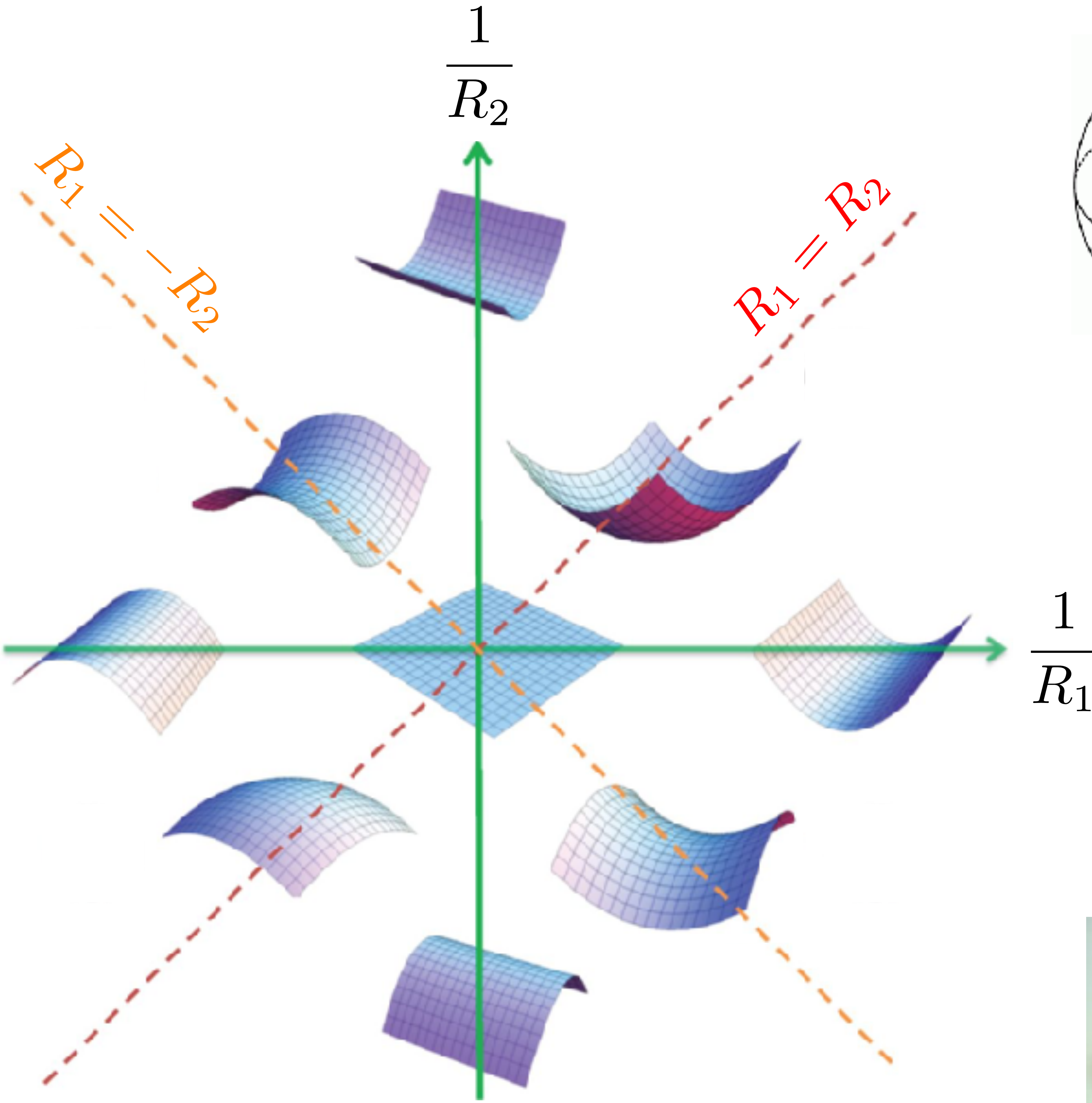
mean curvature

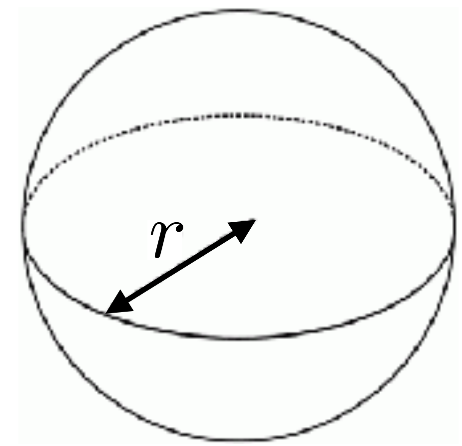
$$\frac{1}{2}\left(\frac{1}{R_1} + \frac{1}{R_2}\right) = \frac{1}{2}\sum_i K_{ii} = \frac{1}{2}\mathrm{tr}(K_{ij})$$

Gaussian curvature

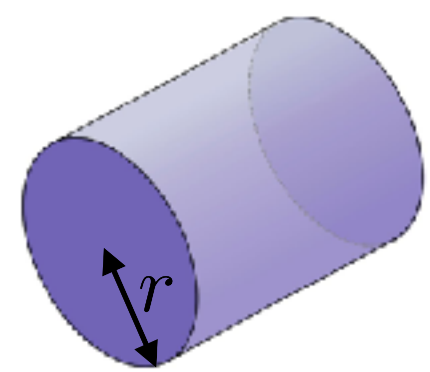
$$\frac{1}{R_1 R_2} = \det(K_{ij})$$

Surfaces of various principal curvatures





$$\frac{1}{R_1} = \frac{1}{R_2} = \frac{1}{r}$$



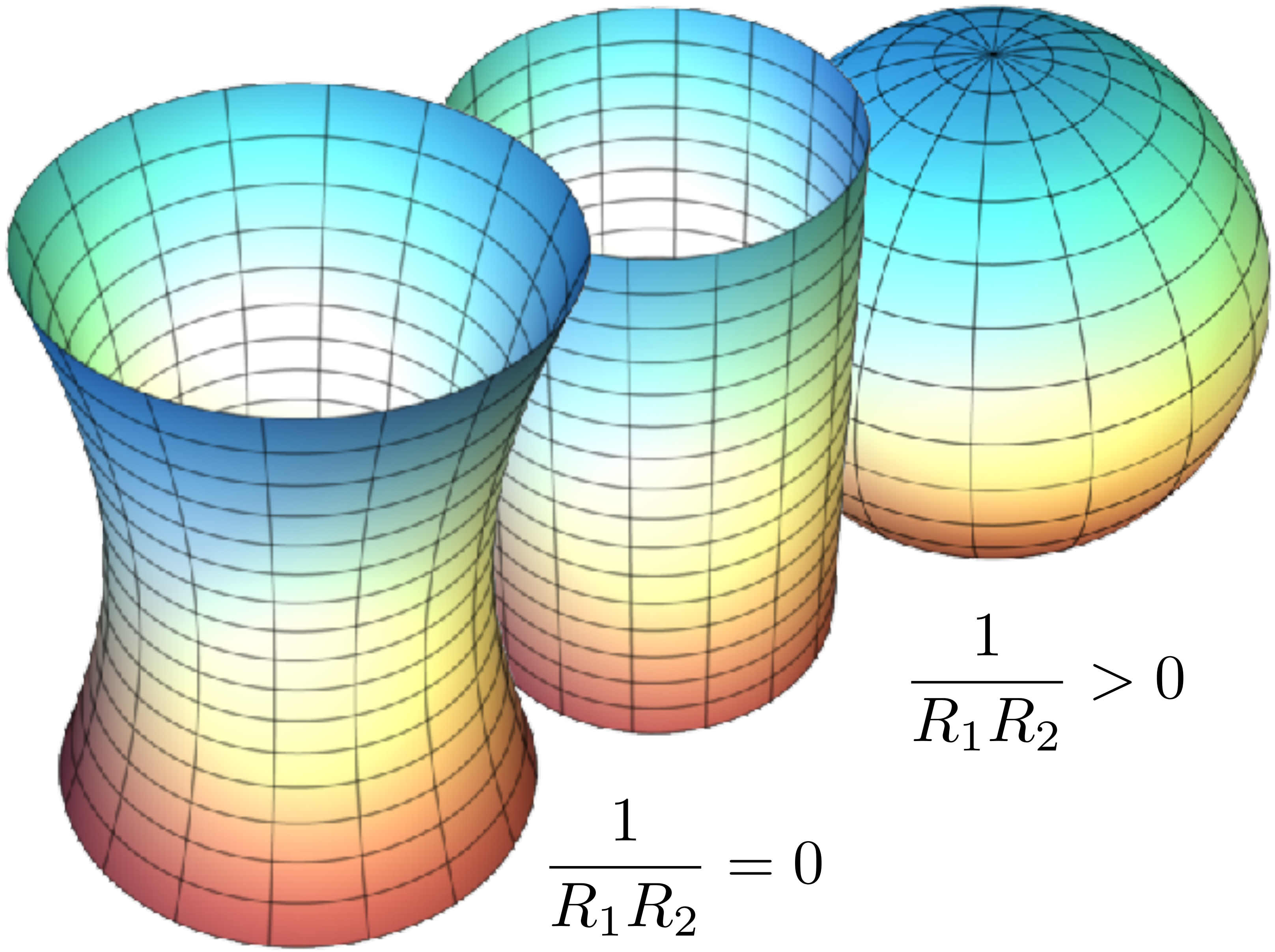
$$\frac{1}{R_1} = \frac{1}{r}$$

$$\frac{1}{R_2} = 0$$

$$\frac{1}{R_1} > 0$$

$$\frac{1}{R_2} < 0$$

Examples for Gaussian curvature



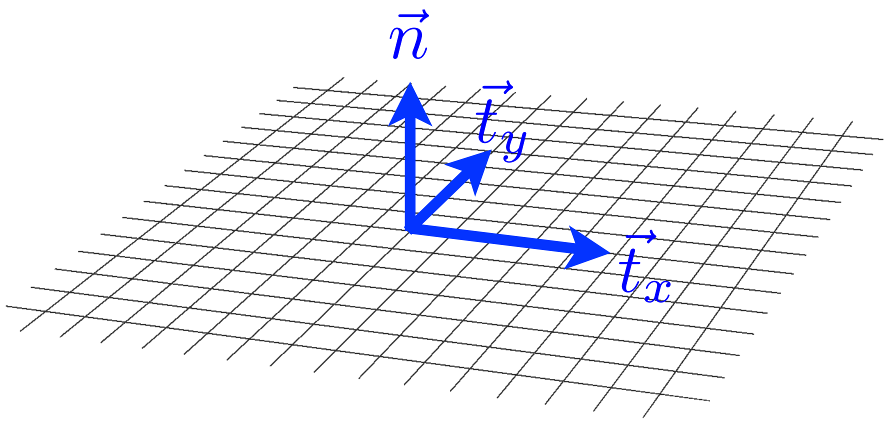
$$\frac{1}{R_1 R_2} > 0$$

$$\frac{1}{R_1 R_2} = 0$$

$$\frac{1}{R_1 R_2} < 0$$

Examples

$$K_{ij} = \sum_k \left(g^{-1}\right)_{ik} \left(\vec{n} \cdot \frac{\partial^2 \vec{r}}{\partial x^k \partial x^j}\right)$$



$$\vec{r}(x,y) = (x,y,0)$$

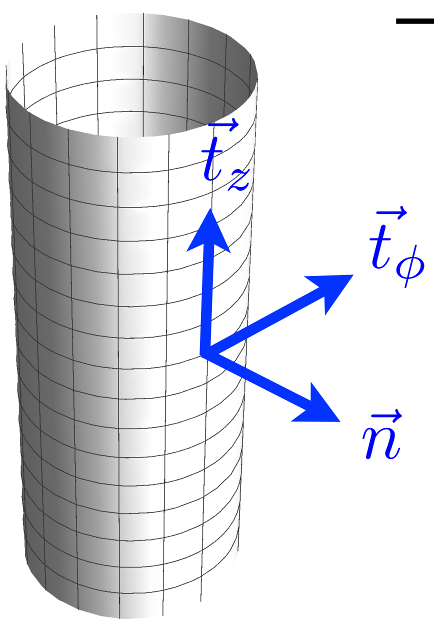
$$\vec{t}_x = \frac{\partial \vec{r}}{\partial x} = (1,0,0)$$

$$\vec{t}_y = \frac{\partial \vec{r}}{\partial y} = (0,1,0)$$

$$\vec{n} = \frac{\vec{t}_x \times \vec{t}_y}{|\vec{t}_x \times \vec{t}_y|} = (0,0,1)$$

$$g_{ij} = \vec{t}_i \cdot \vec{t}_j = \begin{pmatrix} 1, & 0 \\ 0, & 1 \end{pmatrix}$$

$$K_{ij} = \begin{pmatrix} 0, & 0 \\ 0, & 0 \end{pmatrix}$$



$$\vec{r}(\phi,z) = (R\cos\phi, R\sin\phi, z)$$

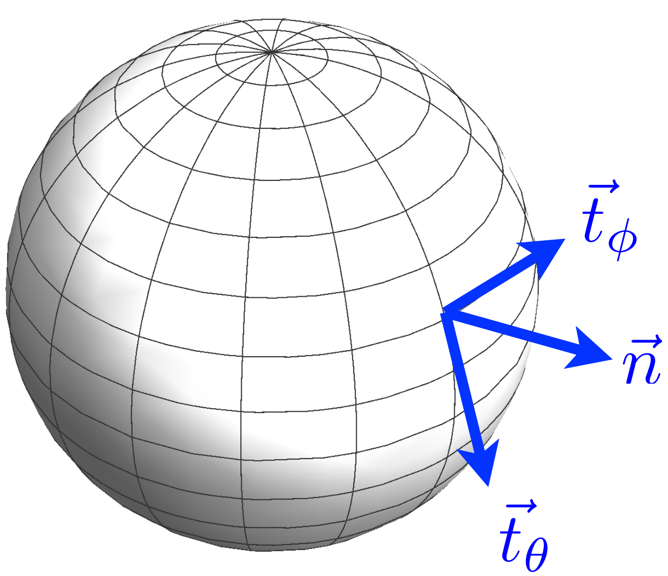
$$\vec{t}_\phi = \frac{\partial \vec{r}}{\partial \phi} = R(-\sin\phi, \cos\phi, 0)$$

$$\vec{t}_z = \frac{\partial \vec{r}}{\partial z} = (0,0,1)$$

$$\vec{n} = \frac{\vec{t}_\phi \times \vec{t}_z}{|\vec{t}_\phi \times \vec{t}_z|} = (\cos\phi, \sin\phi, 0)$$

$$g_{ij} = \vec{t}_i \cdot \vec{t}_j = \begin{pmatrix} R^2, & 0 \\ 0, & 1 \end{pmatrix}$$

$$K_{ij} = \begin{pmatrix} -\frac{1}{R}, & 0 \\ 0, & 0 \end{pmatrix}$$



$$\vec{r}(\theta,\phi) = R(\sin\theta\cos\phi, \sin\theta\sin\phi, \cos\theta)$$

$$\vec{t}_\theta = \frac{\partial \vec{r}}{\partial \theta} = R(\cos\theta\cos\phi, \cos\theta\sin\phi, -\sin\theta)$$

$$\vec{t}_\phi = \frac{\partial \vec{r}}{\partial \phi} = R\sin\theta(-\sin\phi, \cos\phi, 0)$$

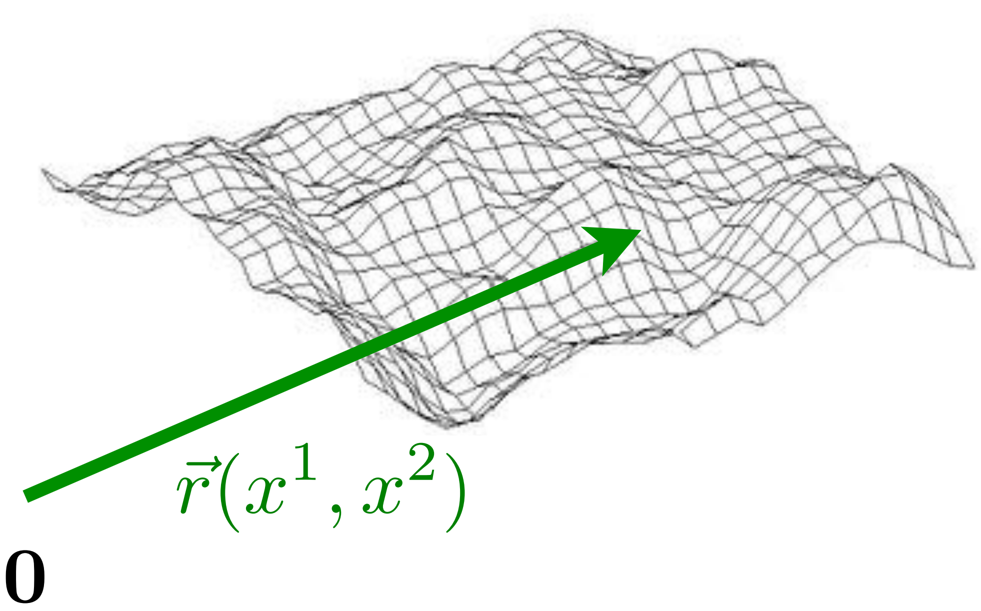
$$\vec{n} = \frac{\vec{t}_\theta \times \vec{t}_\phi}{|\vec{t}_\theta \times \vec{t}_\phi|} = (\sin\theta\cos\phi, \sin\theta\sin\phi, \cos\theta)$$

$$g_{ij} = \vec{t}_i \cdot \vec{t}_j = \begin{pmatrix} R^2, & 0 \\ 0, & R^2\sin^2\theta \end{pmatrix}$$

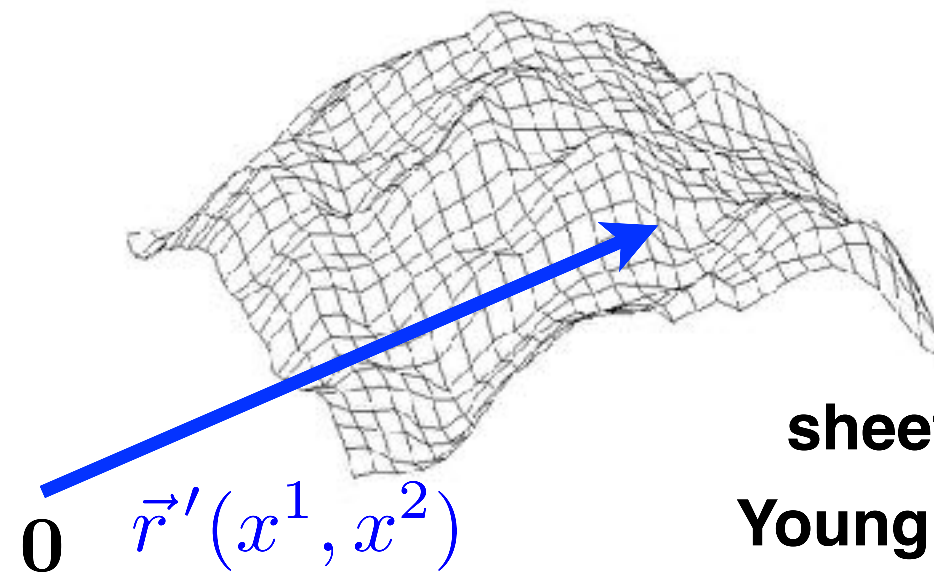
$$K_{ij} = \begin{pmatrix} -\frac{1}{R}, & 0 \\ 0, & -\frac{1}{R} \end{pmatrix}$$

Bending energy for deformation of shells

undeformed shell



deformed shell



sheet thickness d

Young's modulus E

Poisson's ratio ν

$$K_{ij} = \sum_k \left(g^{-1}\right)_{ik} \left(\vec{n} \cdot \frac{\partial^2 \vec{r}}{\partial x^k \partial x^j}\right)$$

$$K'_{ij} = \sum_k \left(g'^{-1}\right)_{ik} \left(\vec{n}' \cdot \frac{\partial^2 \vec{r}\,'}{\partial x^k \partial x^j}\right)$$

bending strain tensor

$$b_{ij} = K'_{ij} - K_{ij}$$

(local measure of deviation from preferred curvature)

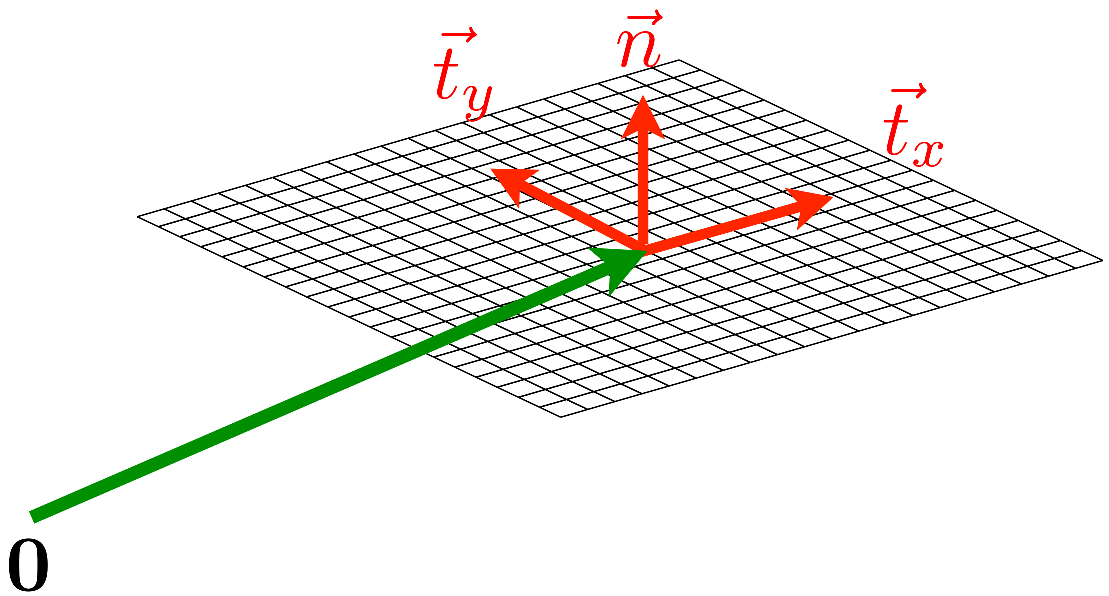
Energy cost of bending

$$U = \int \left(\sqrt{g}dx^1 dx^2\right) \left[\frac{1}{2}\kappa \left(\mathrm{tr}(b_{ij})\right)^2 + \kappa_G \det(b_{ij})\right]$$

$$\kappa = \frac{Ed^3}{12(1-\nu^2)} \qquad \kappa_G = -\frac{Ed^3}{12(1+\nu)}$$

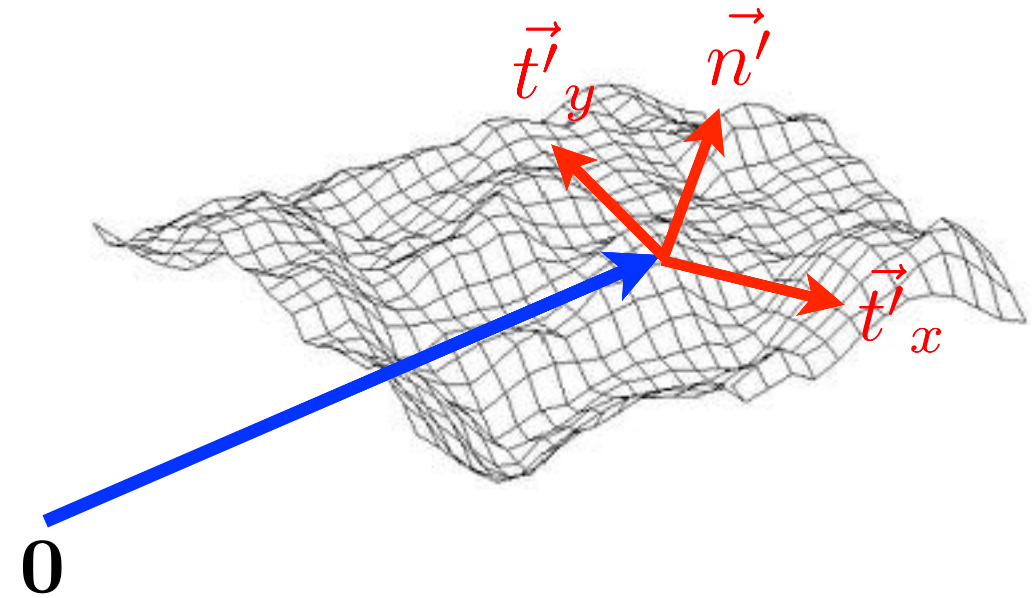
Bending strain for deformation of flat plates

undeformed plate



$$\vec{r}(x,y) = x\vec{e}_x + y\vec{e}_y$$

deformed plate



$$\vec{r'}(x,y) = \vec{r}(x,y) + u_x(x,y)\vec{e}_x + u_y(x,y)\vec{e}_y + h(x,y)\vec{e}_z$$

local normal

$$\vec{n} = \frac{\vec{t}_x \times \vec{t}_y}{|\vec{t}_x \times \vec{t}_y|} = \vec{e}_z$$

local normal (neglecting in-plane deformations)

$$\vec{n'} \approx \frac{\vec{e}_z - (\partial_x h)\,\vec{e}_x - (\partial_y h)\,\vec{e}_y}{\sqrt{1 + (\partial_x h)^2 + (\partial_y h)^2}}$$

reference curvature tensor

$$K_{ij} = \vec{n} \cdot \partial_i \partial_j \vec{r} = 0$$

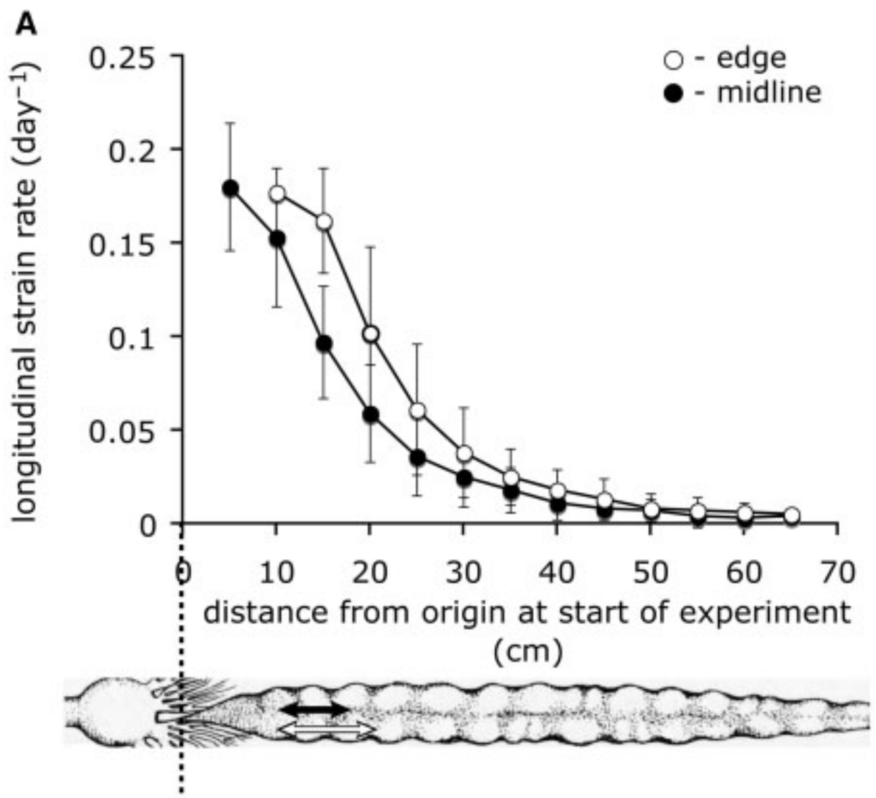
bending strain tensor

$$b_{ij} = K'_{ij} \approx \partial_i \partial_j h + \cdots$$

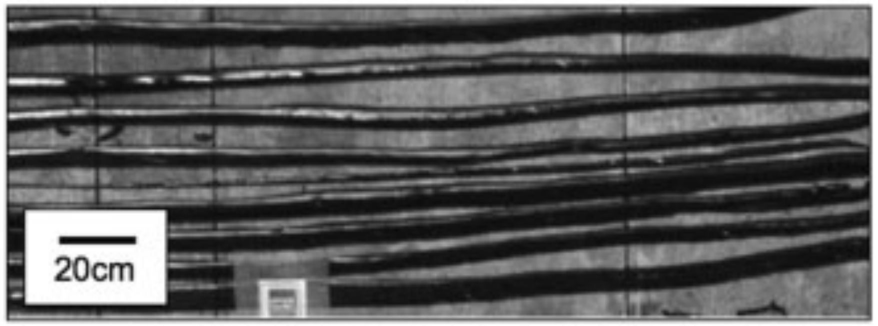
Wrinkled and straight blades in macroalgae

Slow water flow environment (v~0.5 m/s)

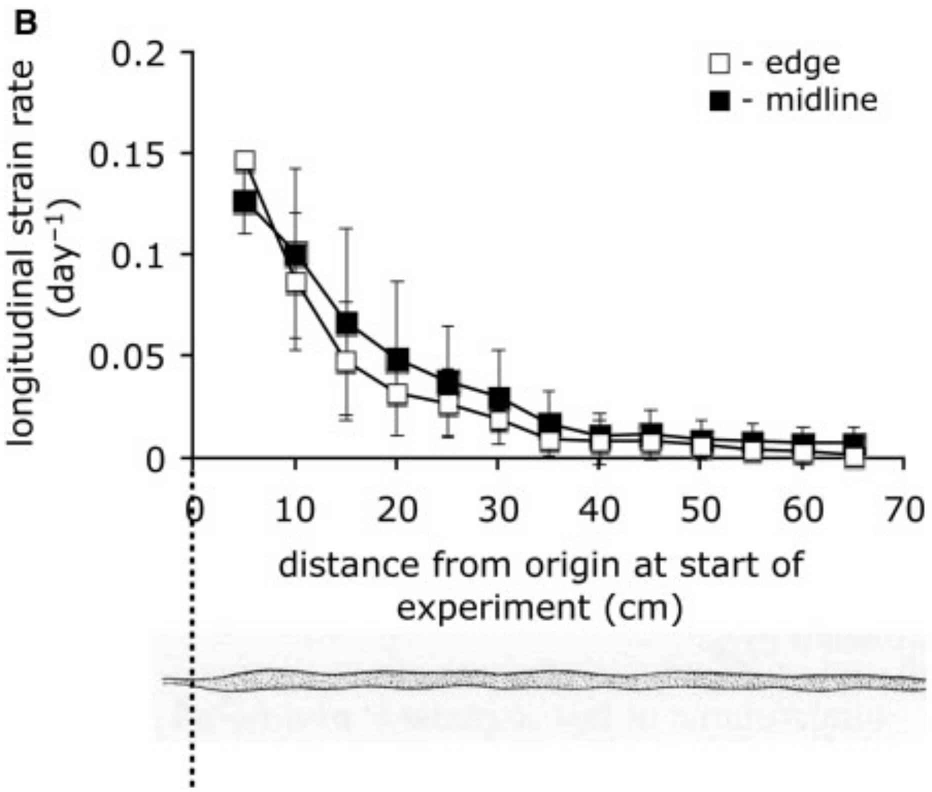
edges of blades grow faster than the midline



Fast water flow environment (v~1.5 m/s)



edges of blades grow at the same speed as the midline



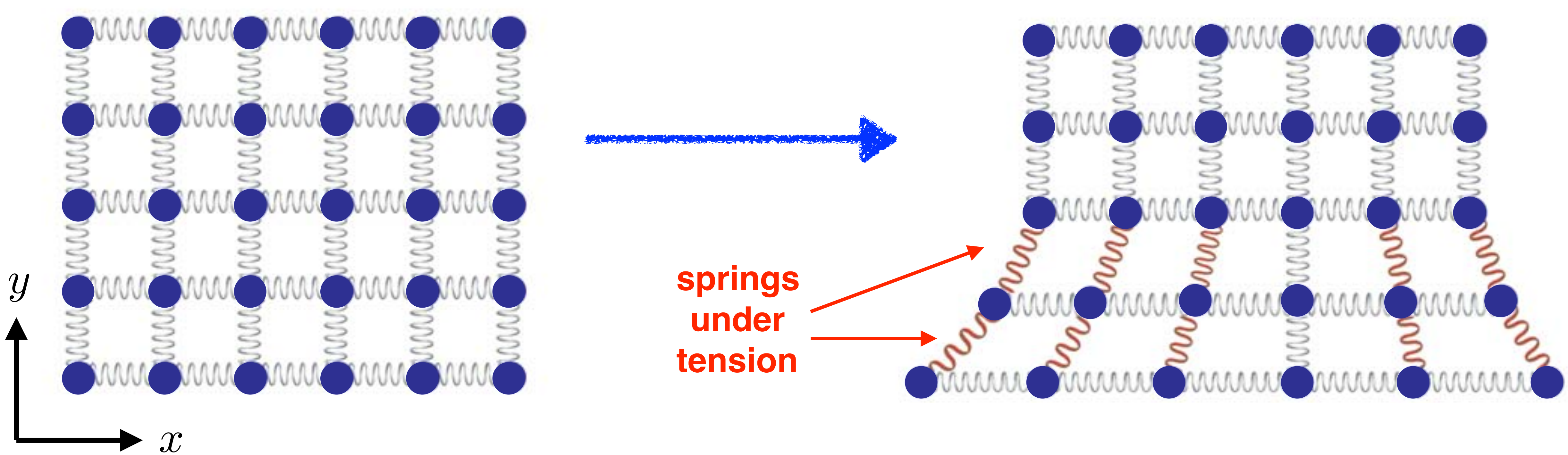
What is the effect of differential growth rate between the edge and the midline of the blade?

M. Koehl et al., Integ. Comp. Biol. 48, 834 (2008)

Differential growth produces internal stress

before growth

faster growth of the bottom edge in x direction



$$d\ell^2 = \sum_{i,j} g_{ij}\, dx^i dx^j$$

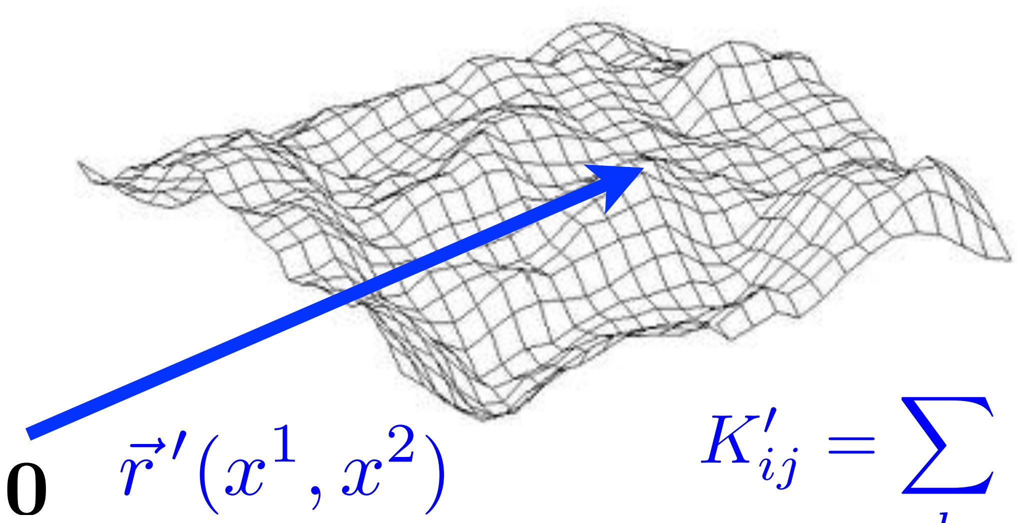
Growth modifies the metric tensor of sheet!

$$g_{ij} = \begin{pmatrix} 1, & 0 \\ 0, & 1 \end{pmatrix} \longrightarrow g_{ij} = \begin{pmatrix} f(y), & 0 \\ 0, & 1 \end{pmatrix}$$

Note: If growth is different between the top and bottom of the sheet, then the curvature tensor K_{ij} is modified as well!

Mechanics of growing sheets

Growth defines preferred metric tensor g_{ij},
and preferred curvature tensor K_{ij}.



$$g'_{ij} = \frac{\partial \vec{r}'}{\partial x^i} \cdot \frac{\partial \vec{r}'}{\partial x^j}$$

$$K'_{ij} = \sum_k \left(g'^{-1}\right)_{ik} \left(\vec{n}' \cdot \frac{\partial^2 \vec{r}'}{\partial x^k \partial x^j}\right)$$

strain tensors

$$u_{ij} = \frac{1}{2} \sum_k \left(g^{-1}\right)_{ik} \left(g'_{kj} - g_{kj}\right)$$

$$b_{ij} = K'_{ij} - K_{ij}$$

The equilibrium membrane shape $\vec{r}'(x^1, x^2)$
corresponds to the minimum of elastic energy:

$$U = \int \left(\sqrt{g} dx^1 dx^2\right) \left[\frac{1}{2}\lambda \left(\sum_i u_{ii}\right)^2 + \mu \sum_{i,j} u_{ij} u_{ji} + \frac{1}{2}\kappa \left(\mathrm{tr}(b_{ij})\right)^2 + \kappa_G \det(b_{ij})\right]$$

Growth can independently tune the metric tensor g_{ij} and the curvature tensor K_{ij}, which may not be compatible with any surface shape that would produce zero energy cost!

Zero energy shape exists only when preferred metric tensor g_{ij} and preferred curvature tensor K_{ij} satisfy Gauss-Codazzi-Mainardi relations!

Mechanics of growing membranes

One of the Gauss-Codazzi-Mainardi equations (Gauss's Theorema Egregium) relates the Gauss curvature to metric tensor

$$\det(K'_{ij}) = \mathcal{F}(g'_{ij})$$

The equilibrium membrane shape $\vec{r}\,'(x^1, x^2)$ corresponds to the minimum of elastic energy:

$$U = \int (\sqrt{g} dx^1 dx^2) \left[\frac{1}{2}\lambda \left(\sum_i u_{ii} \right)^2 + \mu \sum_{i,j} u_{ij} u_{ji} + \frac{1}{2}\kappa \left(\mathrm{tr}(b_{ij})\right)^2 + \kappa_G \det(b_{ij}) \right]$$

scaling with membrane thickness d

$$\lambda, \mu \sim Ed$$

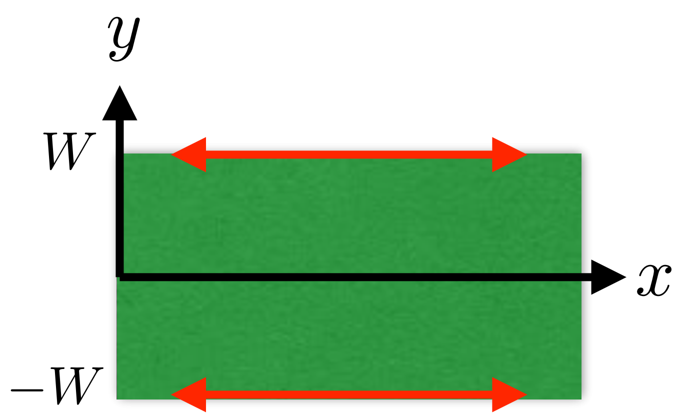
$$\kappa, \kappa_G \sim Ed^3$$

For very thin membranes the equilibrium shape matches the preferred metric tensor to avoid stretching, compressing and shearing. This also specifies the Gauss curvature!

$$g'_{ij} = g_{ij}$$

$$\det(K'_{ij}) = \mathcal{F}(g_{ij})$$

Example



Assume that differential growth in x direction produces metric tensor of the form

$$g_{ij} = \begin{pmatrix} f(y), & 0 \\ 0, & 1 \end{pmatrix} \qquad f(y) = 1 + ce^{(|y|-W)/\lambda}$$

For thin membranes the metric tensor wants to be matched

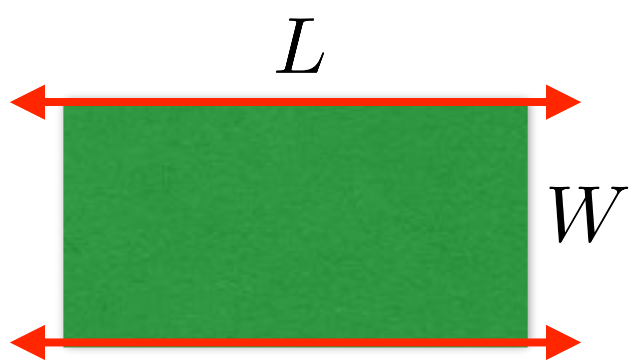
$$g'_{ij} = g_{ij}$$

Gauss's Theorema Egregium provides Gauss curvature

$$\det(K'_{ij}(y)) = \mathcal{F}(g_{ij}) = -\frac{1}{f}\frac{d^2 f(y)}{dy^2} = -\frac{1}{\lambda^2} \times \frac{ce^{(|y|-W)/\lambda}}{\left(1 + ce^{(|y|-W)/\lambda}\right)} < 0$$

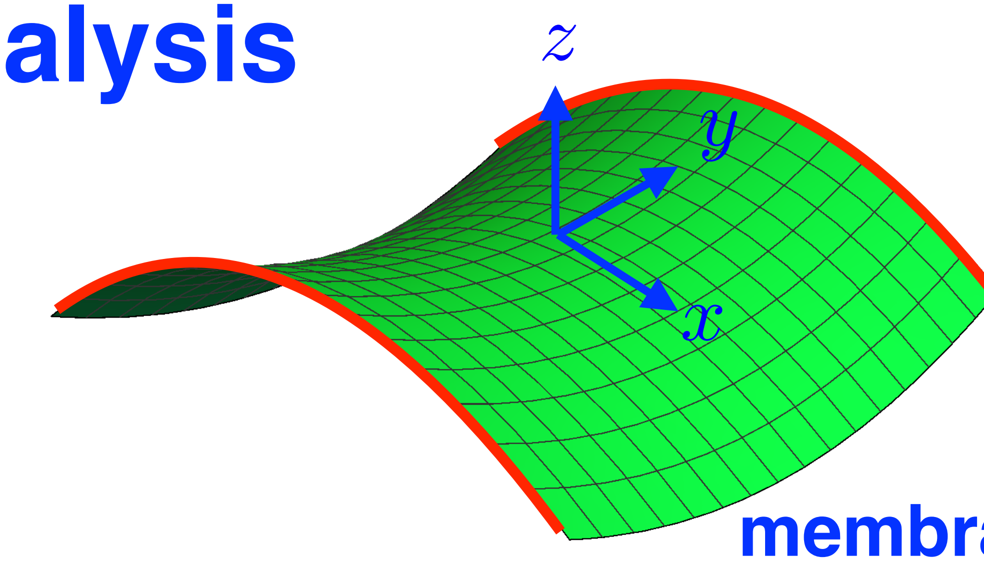
For thin membranes faster growth on edges produces shapes that locally look like saddles!

Scaling analysis



faster growth increases the edge length by factor ϵ

stress released by bending

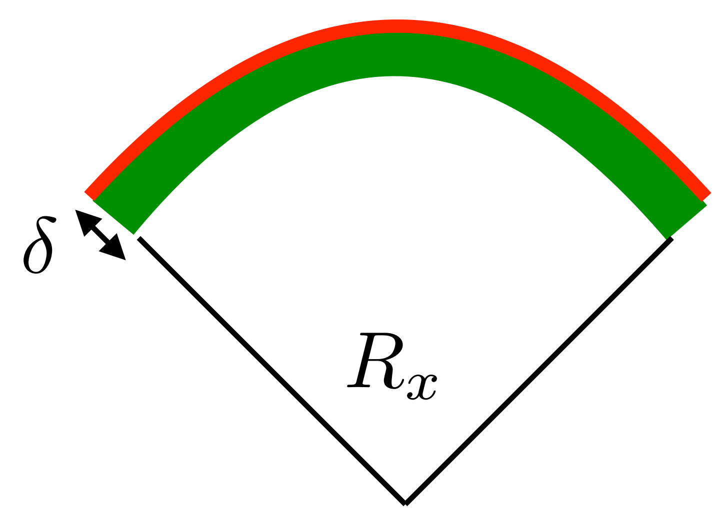


membrane thickness d

y-z cross-section

$$\frac{1}{R_y} \sim \frac{\delta}{W^2}$$

projection to x-z plane



$$\frac{L(1+\epsilon)}{L} \sim \frac{R_x+\delta}{R_x}$$

$$\frac{1}{R_x} \sim \frac{\epsilon}{\delta}$$

Membrane bending energy

$$U_b \sim A \times \kappa \times \left(\frac{1}{R_x^2} + \frac{1}{R_y^2} + \frac{1}{R_x R_y}\right) \sim A \times E_m d^3 \times \left(\frac{\epsilon^2}{\delta^2} + \frac{\delta^2}{W^4} + \frac{\epsilon}{W^2}\right)$$

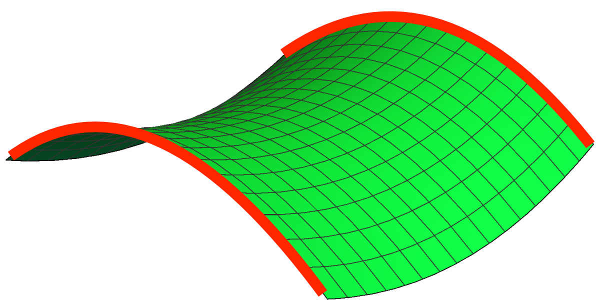
Minimize U_b with respect to δ : $\rightarrow$ $\boxed{\delta \sim W\sqrt{\epsilon}}$ $\rightarrow$ $\boxed{U_b \sim \frac{A E_m d^3 \epsilon}{W^2}}$

Scaling analysis

membrane compression

$$U_c \sim AE_m d\epsilon^2$$

membrane bending



$$U_b \sim \frac{AE_m d^3 \epsilon}{W^2}$$

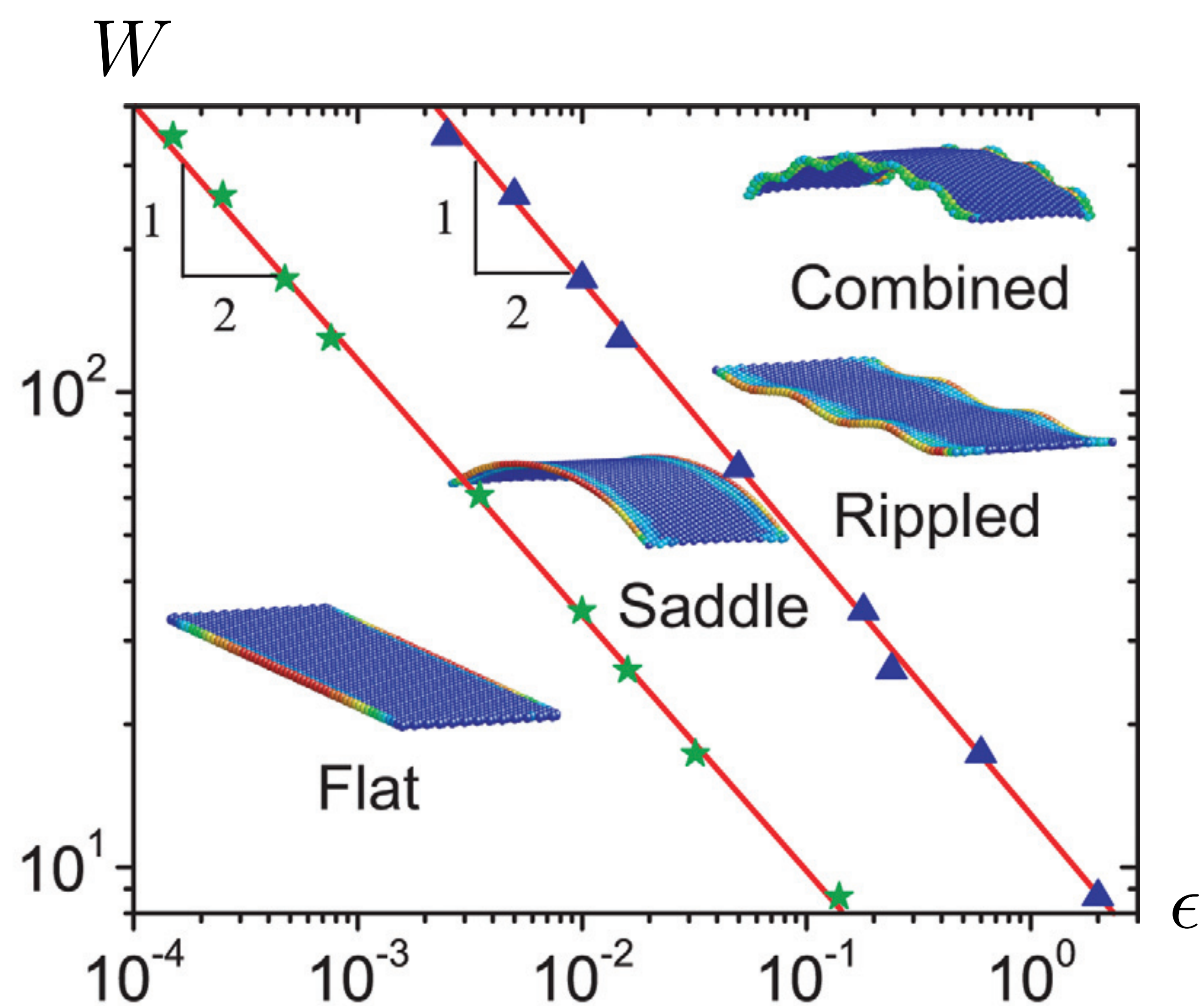
membrane bends above the critical strain

$$\epsilon > \epsilon_c \sim \frac{d^2}{W^2}$$

amplitude of bending at the critical strain

$$\delta^* \sim W\sqrt{\epsilon_c} \sim d$$

numerical simulations



H. Liang and L. Mahadevan, PNAS 106, 22049 (2009)

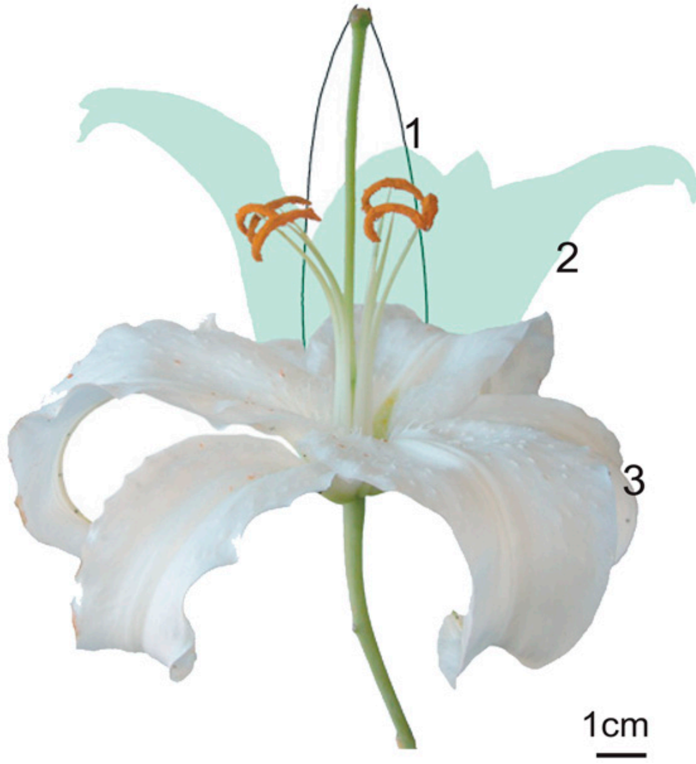
Shapes of flowers and leaves

Faster growth of the edge is consistent with observed saddles and edge wrinkles, which indeed correspond to the negative Gauss curvature!

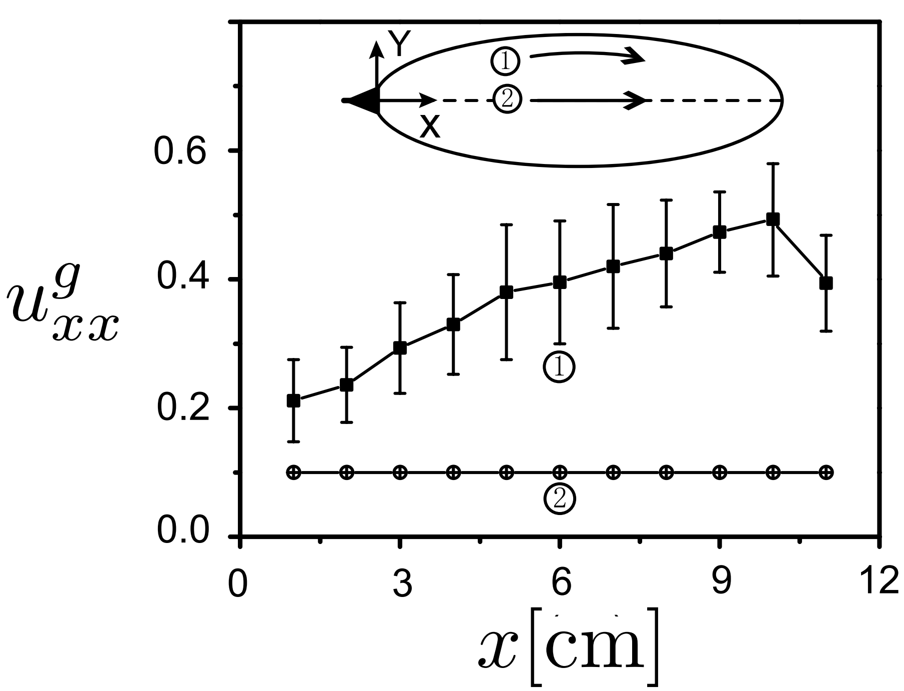
saddles

wrinkled edges (+saddles)

Growth of a blooming lily



faster growth of the edge



in lab blooming takes 4.5 days under constant fluorescent light (1 frame/min)

H. Liang and L. Mahadevan, PNAS 108, 5516 (2011)

How flowers open in the morning and close in the evening?

https://vimeo.com/98276732

When temperature increases in the morning, flowers regulate their growth pattern to grow more new cells on the inside of flower leaves. This results in curling of leaves and opening of flowers.

When temperature drops in the evening, flowers regulate their growth pattern to grow more new cells on the outside of flower leaves. This results in straightening of leaves and closing of flowers.