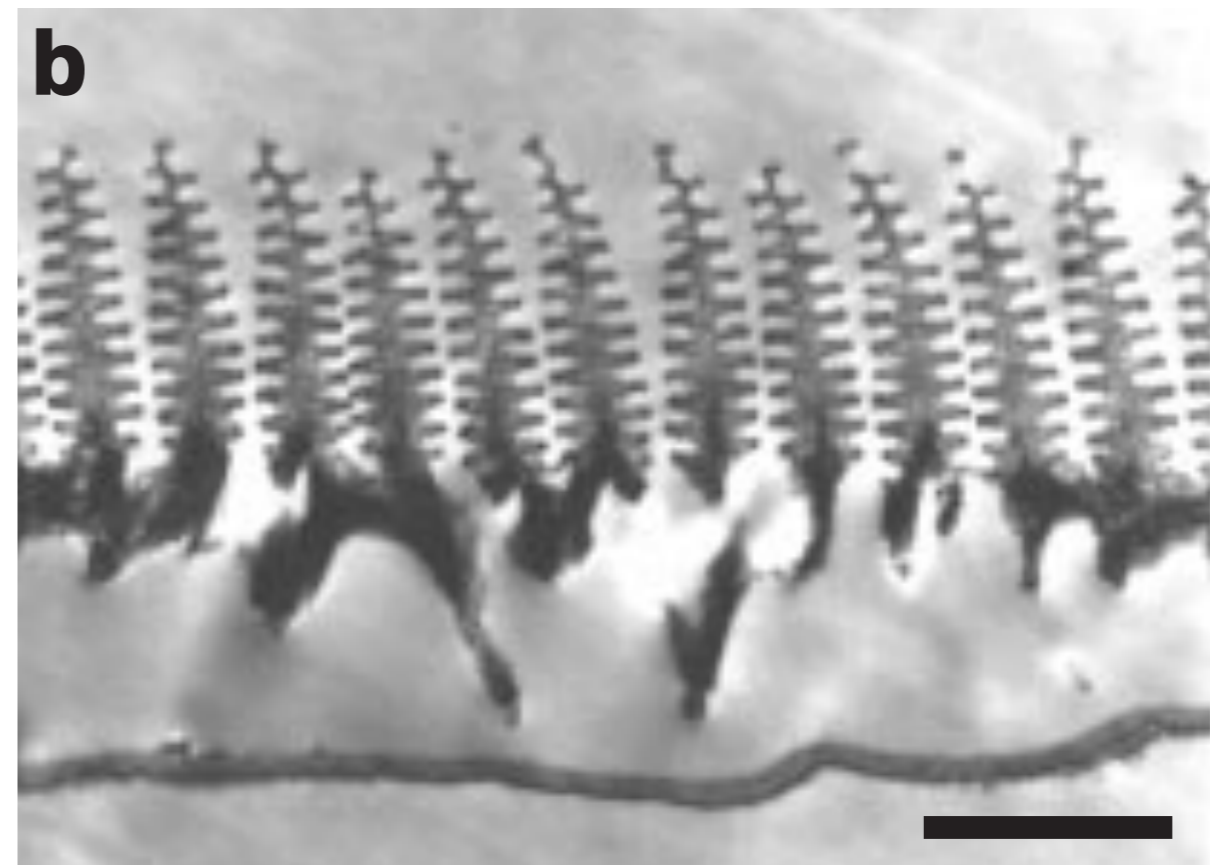


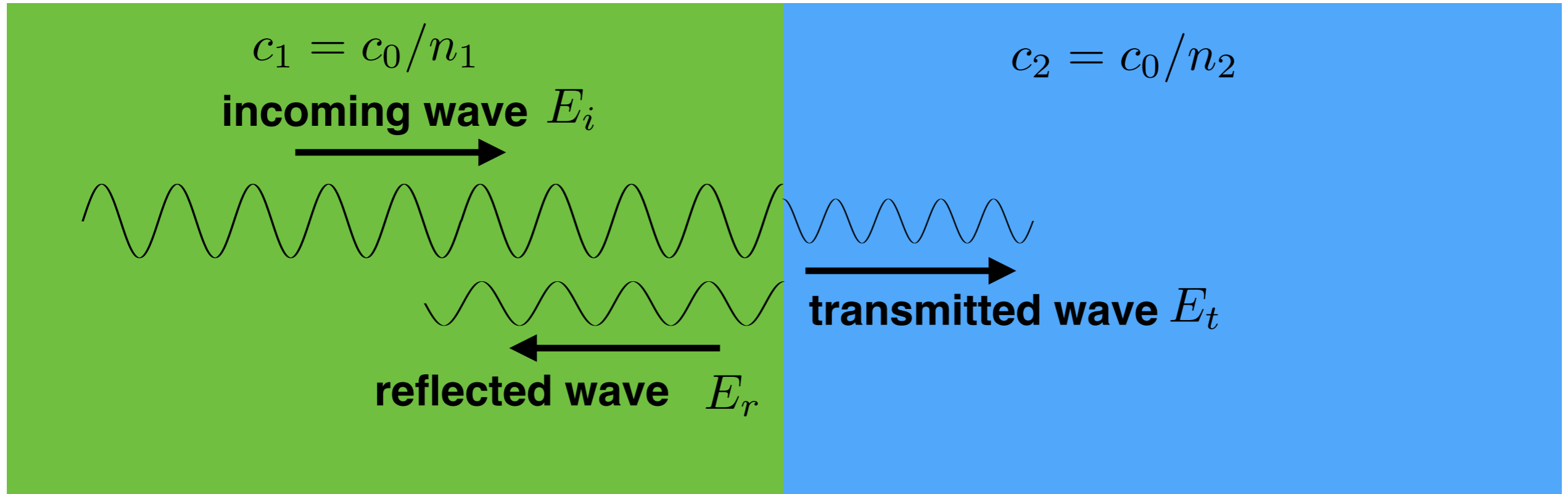
# MAE 545: Lecture 3 (2/13)

## Structural colors



1.7  $\mu\text{m}$

# Reflection of light at the interface between two media



**boundary conditions for incident waves normal to the interface:**

$$E_1 = E_2 \quad H_1 = H_2 \rightarrow \frac{\partial E_1}{\partial x} = \frac{\partial E_2}{\partial x}$$

**amplitude of reflected electric field**

$$r \equiv \frac{E_r}{E_i} = \frac{n_1 - n_2}{n_1 + n_2}$$

**amplitude of transmitted electric field**

$$t \equiv \frac{E_t}{E_i} = \frac{2n_1}{n_1 + n_2}$$

**energy density of electromagnetic waves**

$$\propto n|E|^2$$

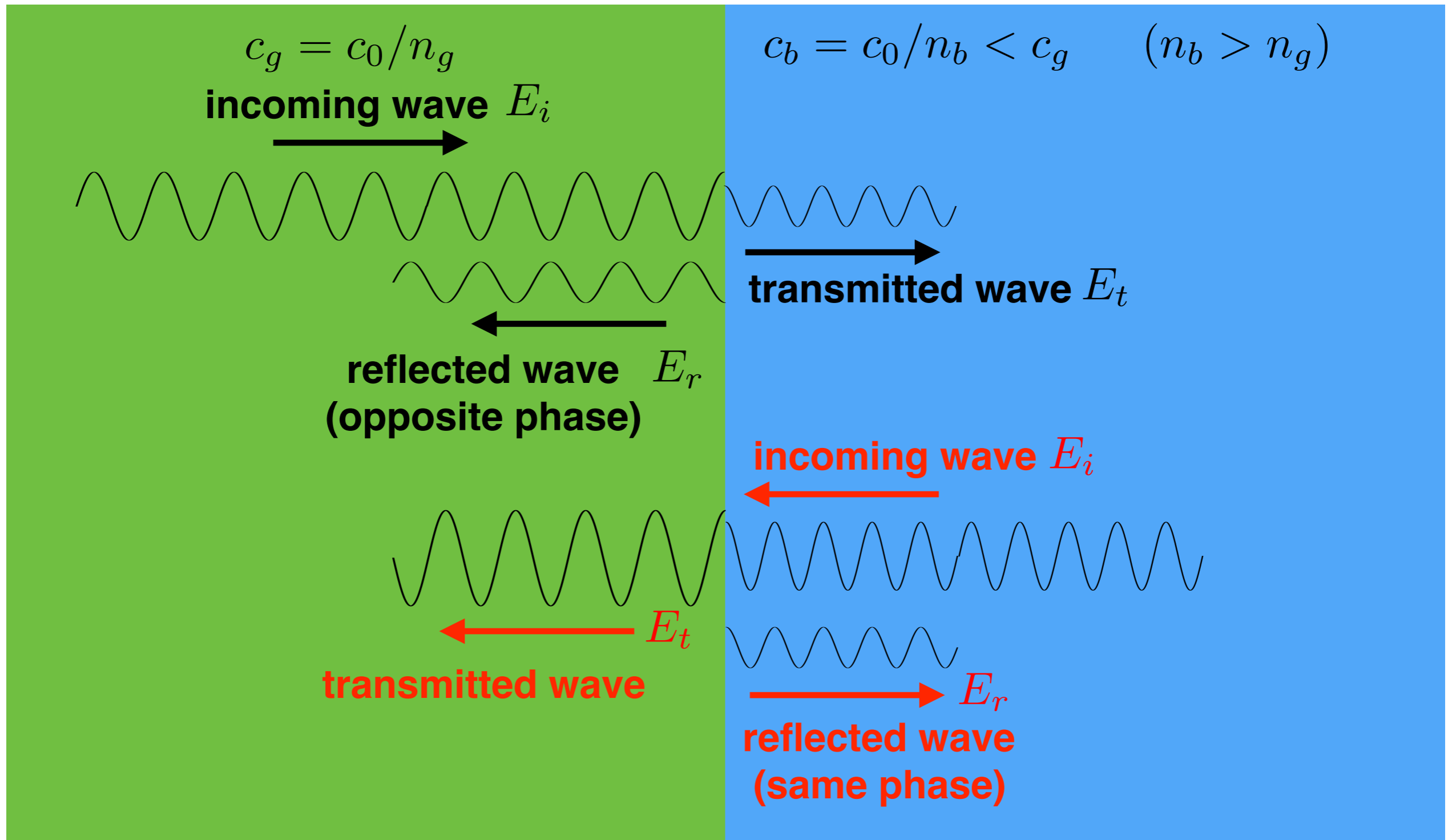
**reflectance**

$$R \equiv \frac{n_1 |E_r|^2}{n_1 |E_i|^2} = |r|^2$$

**transmittance**

$$T \equiv \frac{n_2 |E_t|^2}{n_1 |E_i|^2} = |t|^2 \frac{n_2}{n_1} = 1 - R$$

# Reflection of light at the interface between two media



**amplitude of reflected electric field**

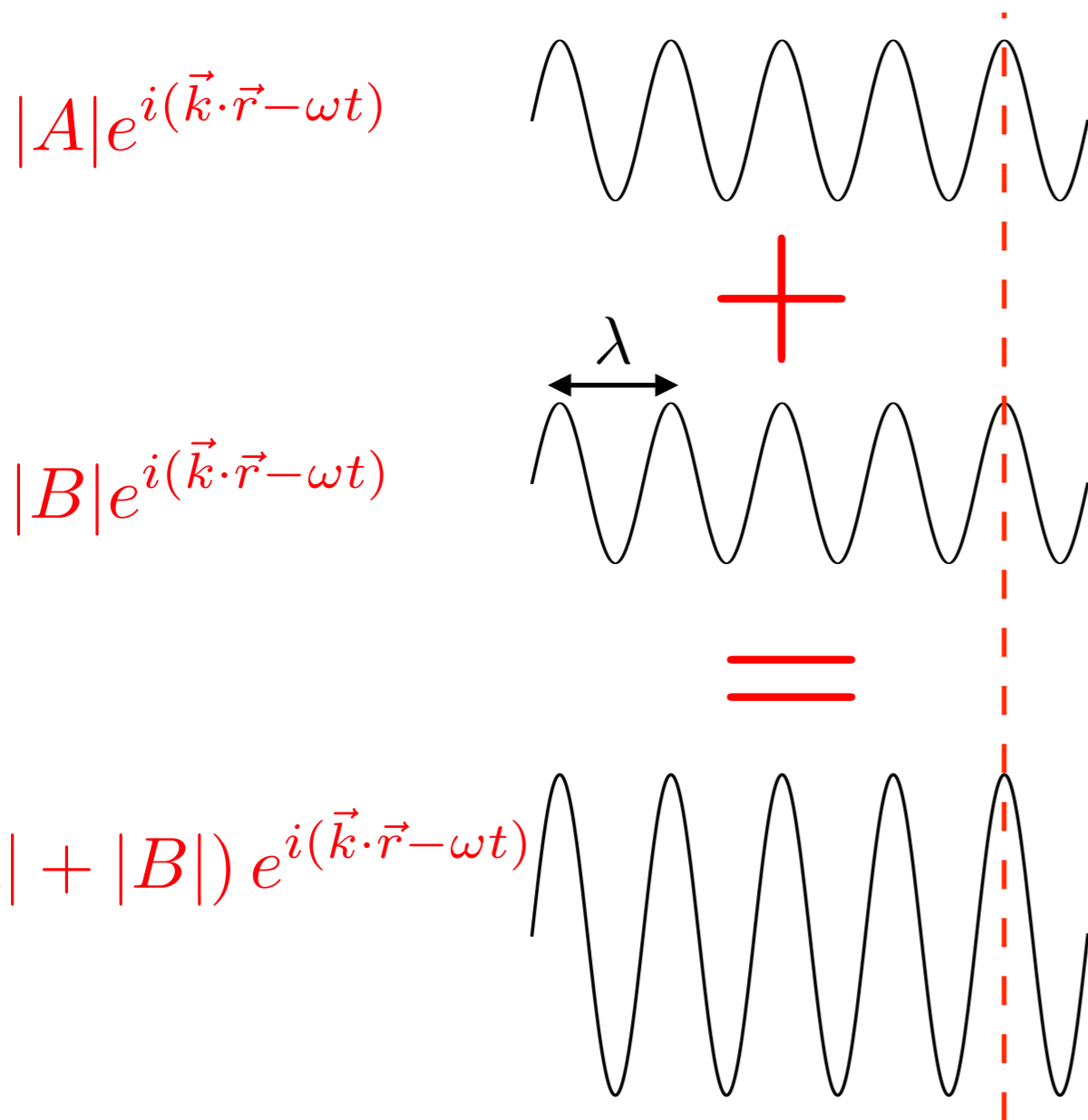
$$\frac{E_r}{E_i} = \frac{n_1 - n_2}{n_1 + n_2}$$

**amplitude of transmitted electric field**

$$\frac{E_t}{E_i} = \frac{2n_1}{n_1 + n_2}$$

# Interference

**constructive interference**



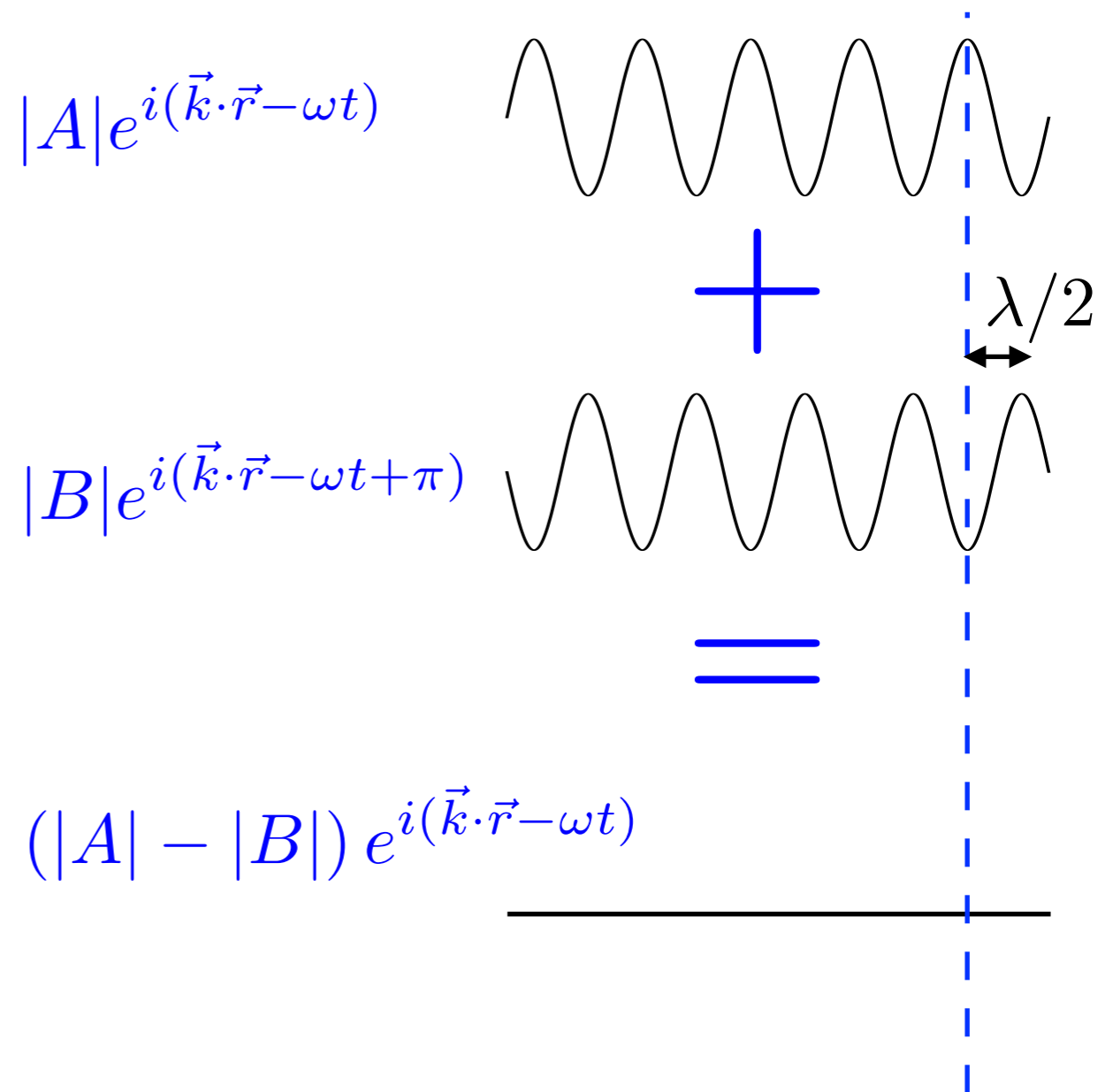
**Constructive interference occurs when the two waves are in phase:**

**waves offset by  $m\lambda$ ,**

$$m = 0, \pm 1, \pm 2, \dots$$

$$e^{ikm\lambda} = e^{i2\pi m} = +1$$

**destructive interference**



**Destructive interference occurs when the two waves are out of phase:**

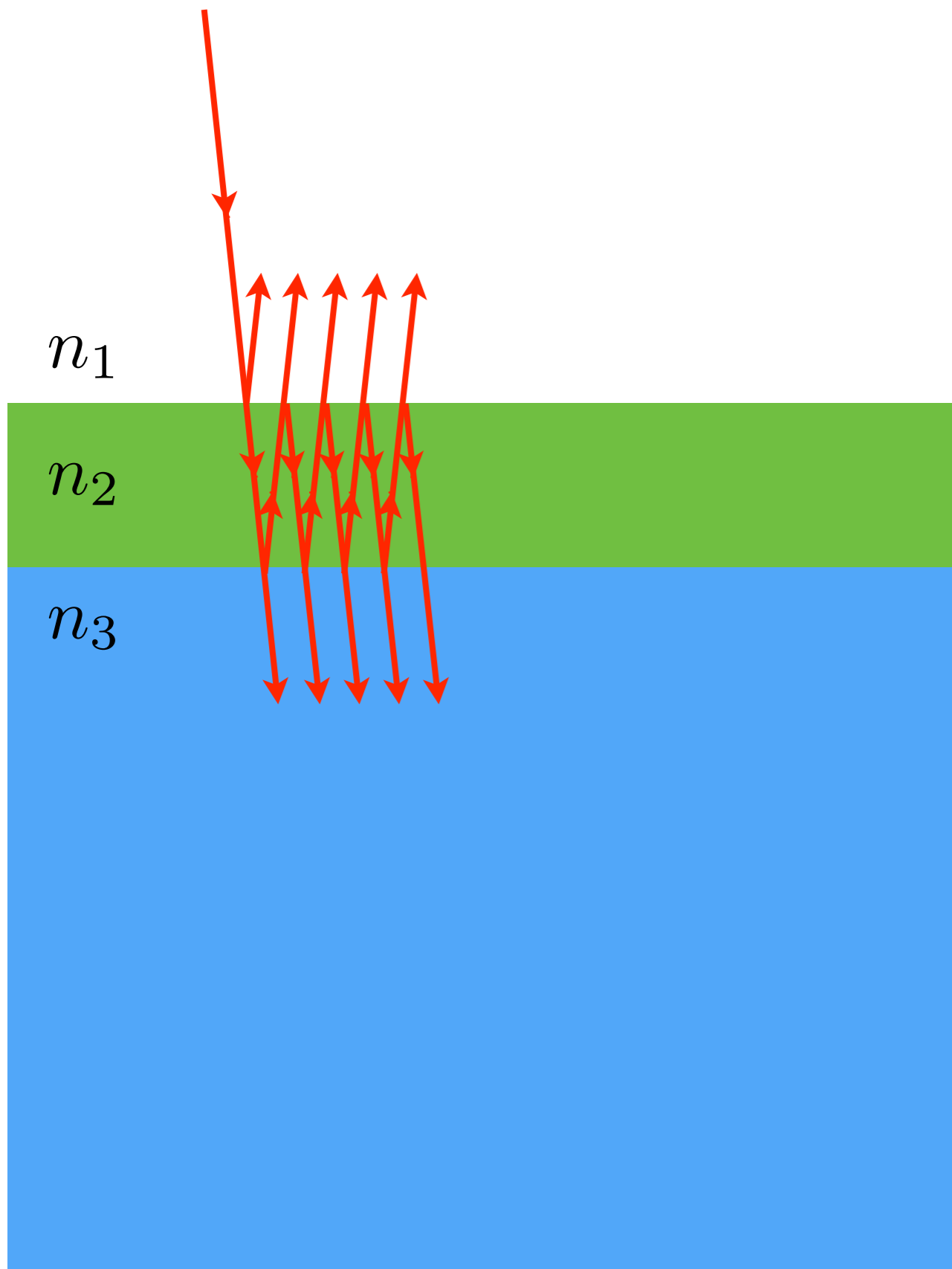
**waves offset by  $(m + 1/2)\lambda$ ,**

$$m = 0, \pm 1, \pm 2, \dots$$

$$e^{ik(m+1/2)\lambda} = e^{i(2\pi m + \pi)} = -1$$

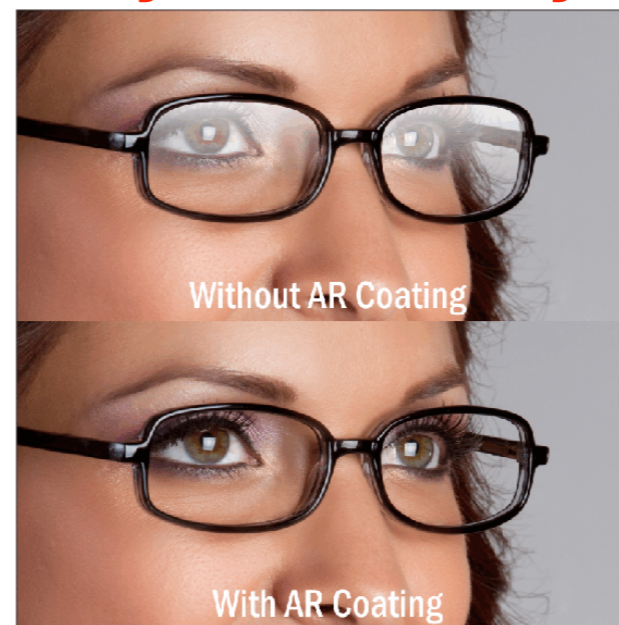
# Interference on thin films

**Constructive interference of reflected rays results in strongly reflected rays with very little transmission.**



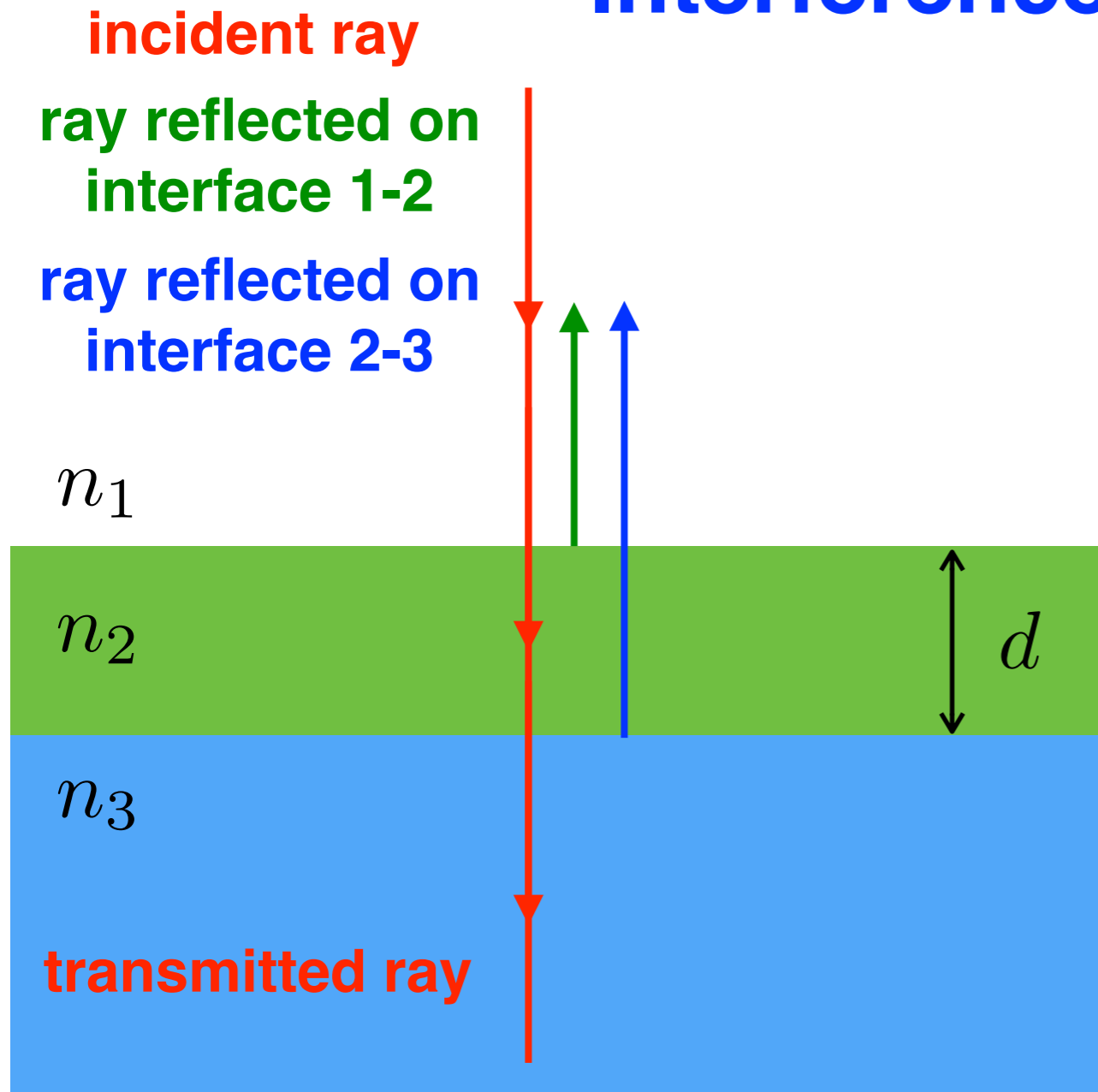
**mirrors**

**Deconstructive interference of reflected rays results in almost perfectly transmitted rays with very little reflection.**



**antireflective coatings**

# Interference on thin films



difference between optical path lengths of the two reflected rays

$$OPD = 2n_2d$$

$$n_1 < n_2 < n_3 \quad n_1 > n_2 > n_3$$

**no additional phase difference due to reflections**

**constructive interference of reflected rays**

$$OPD = m\lambda$$

**destructive interference of reflected rays**

$$OPD = \left(m + \frac{1}{2}\right) \lambda$$

$$m = 0, \pm 1, \pm 2, \dots$$

$$n_1 > n_2 < n_3 \quad n_1 < n_2 > n_3$$

**additional  $\pi$  phase difference due to reflections**

**constructive interference of reflected rays**

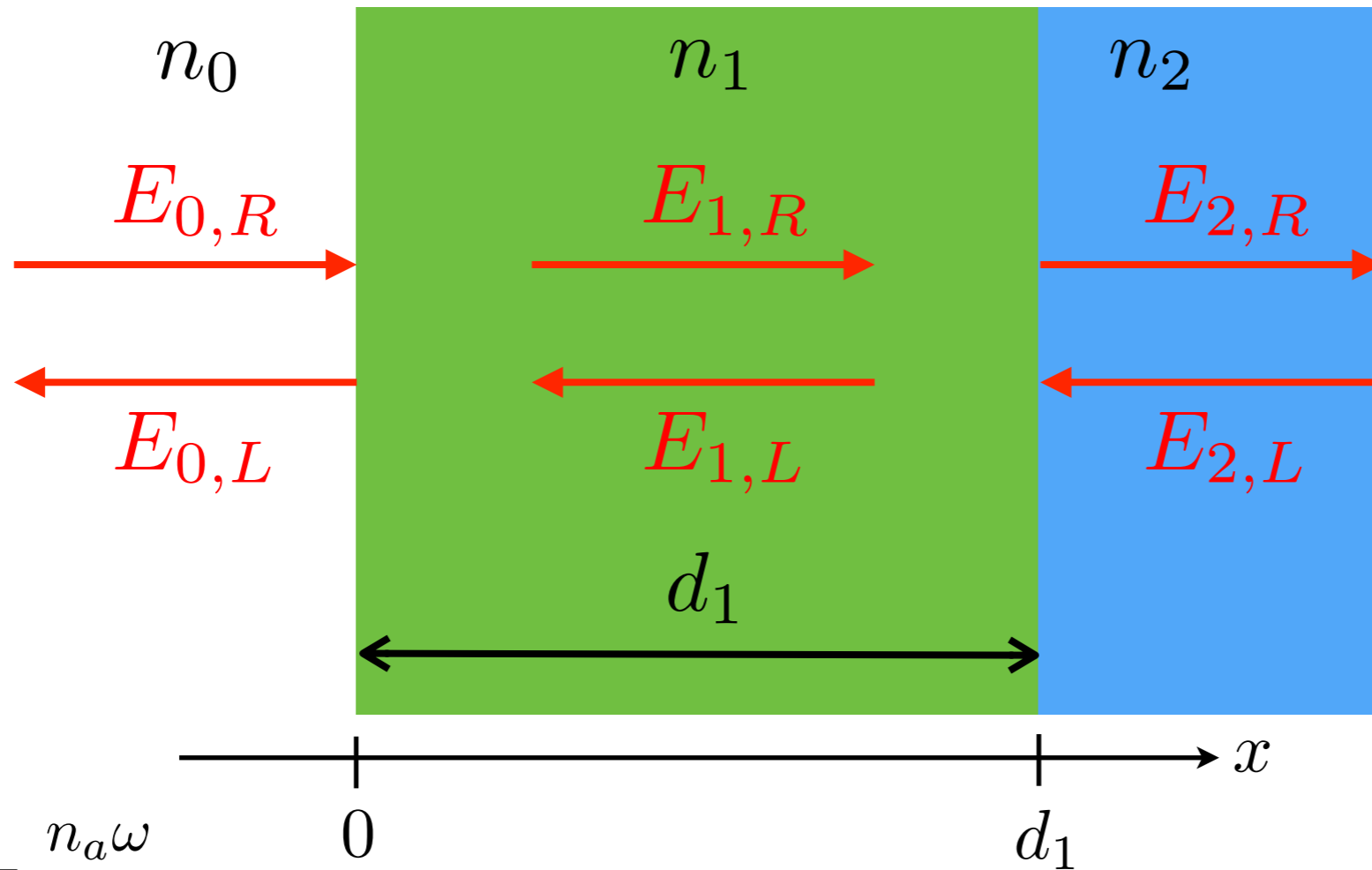
$$OPD = \left(m + \frac{1}{2}\right) \lambda$$

**destructive interference of reflected rays**

$$OPD = m\lambda$$

**What happens for other wavelengths?**

# Transfer matrices



$$k_a = \frac{2\pi n_a}{\lambda} = \frac{n_a \omega}{c_0}$$

**Electromagnetic waves in different regions:**

$$E_0(x, t) = E_{0,R} e^{i(k_0 x - \omega t)} + E_{0,L} e^{i(-k_0 x - \omega t)}$$

$$E_1(x, t) = E_{1,R} e^{i(k_1 x - \omega t)} + E_{1,L} e^{i(-k_1 x - \omega t)}$$

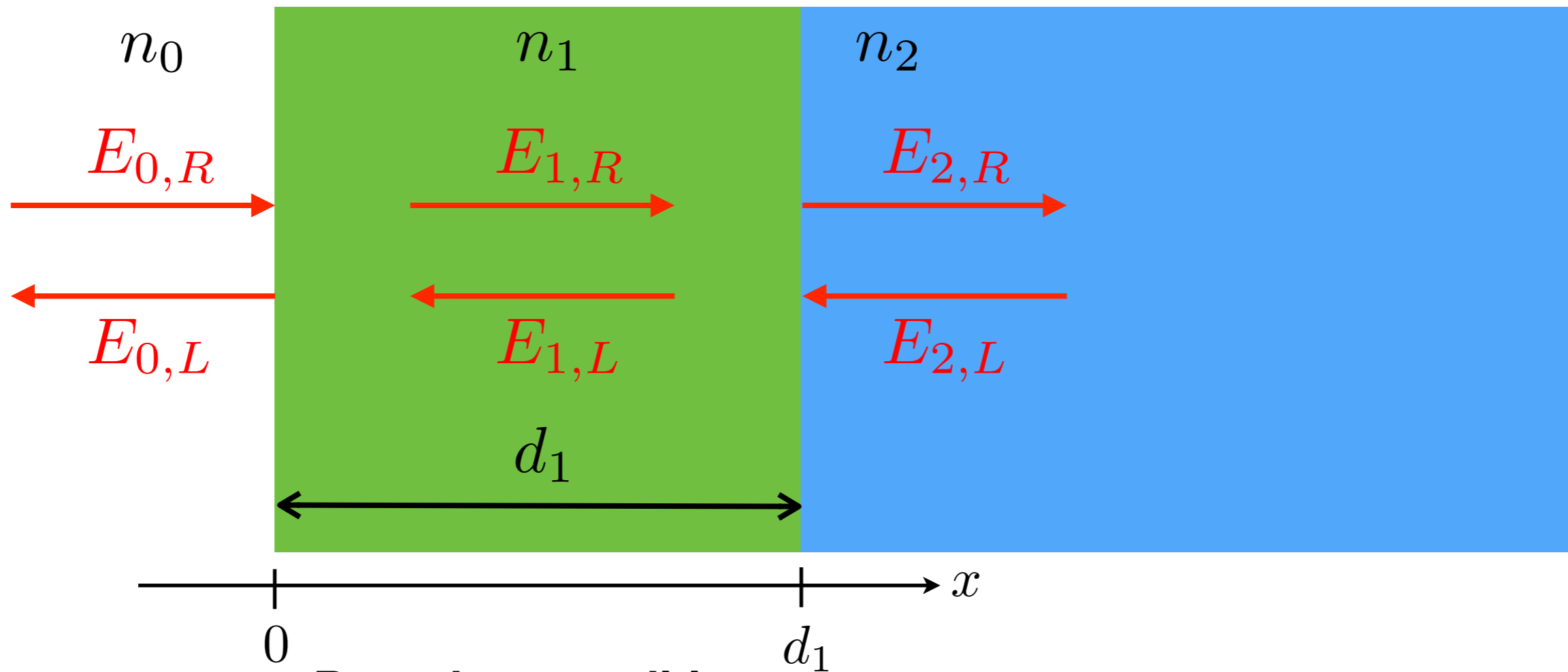
$$E_2(x, t) = E_{2,R} e^{i(k_2 x - \omega t)} + E_{2,L} e^{i(-k_2 x - \omega t)}$$

**Boundary conditions:**

$$E_0(0, t) = E_1(0, t) \qquad E_1(d_1, t) = E_2(d_1, t)$$

$$\frac{\partial E_0}{\partial x}(0, t) = \frac{\partial E_1}{\partial x}(0, t) \qquad \frac{\partial E_1}{\partial x}(d_1, t) = \frac{\partial E_2}{\partial x}(d_1, t)$$

# Transfer matrices



**Boundary conditions:**

$$E_0(0, t) = E_1(0, t) \quad E_1(d_1, t) = E_2(d_1, t)$$

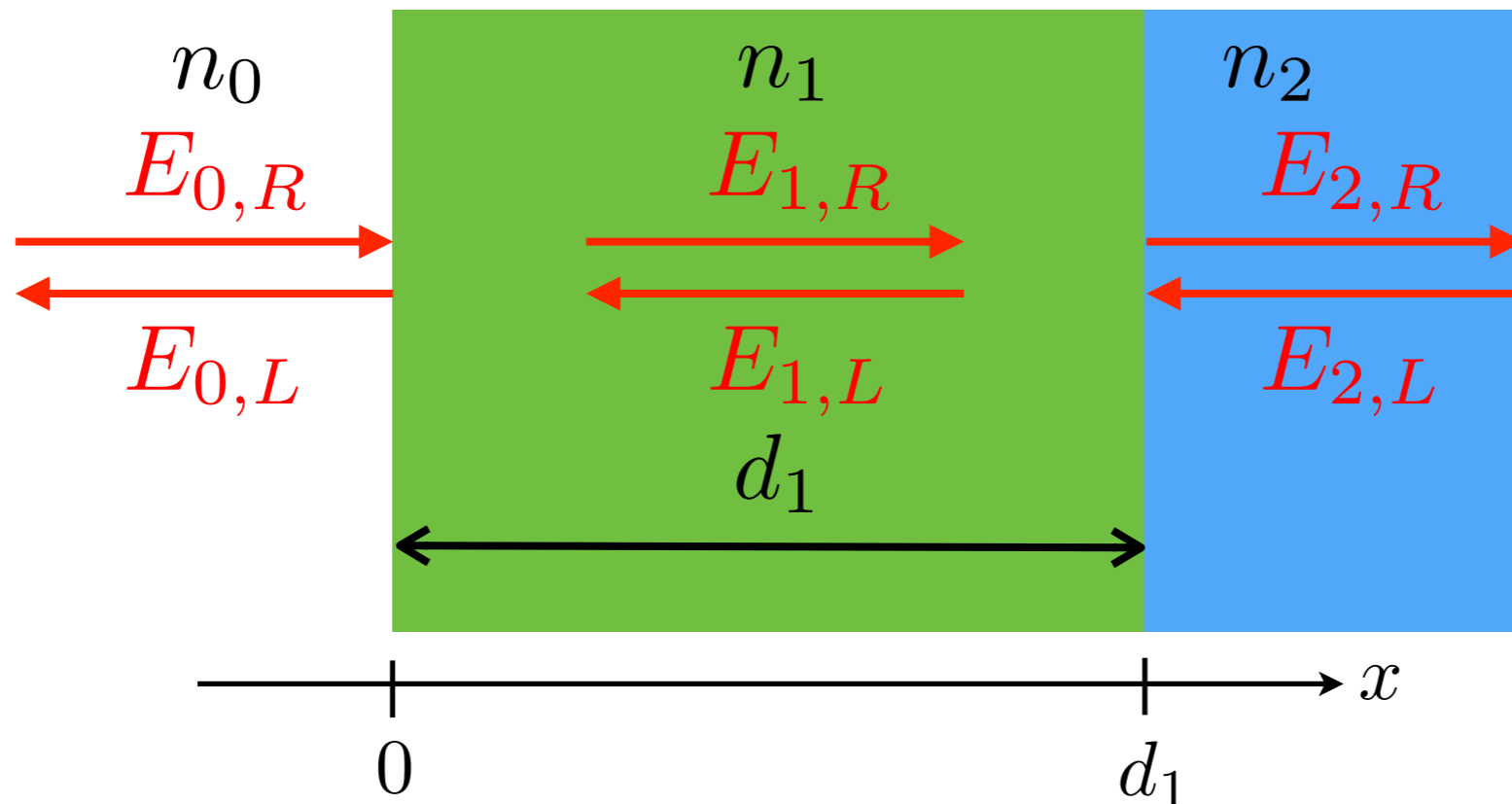
$$\frac{\partial E_0}{\partial x}(0, t) = \frac{\partial E_1}{\partial x}(0, t) \quad \frac{\partial E_1}{\partial x}(d_1, t) = \frac{\partial E_2}{\partial x}(d_1, t)$$

**We would like to relate boundary conditions at two different interfaces via a transfer matrix  $M_1$ :**

$$\begin{pmatrix} E_2(d_1, t) \\ \frac{\partial E_2}{\partial x}(d_1, t) \end{pmatrix} = M_1 \begin{pmatrix} E_0(0, t) \\ \frac{\partial E_0}{\partial x}(0, t) \end{pmatrix}$$



# Transfer matrices



**Electromagnetic waves in regions 1:**

$$E_1(x, t) = E_{1,R}e^{i(k_1x - \omega t)} + E_{1,L}e^{i(-k_1x - \omega t)}$$

**Relation between boundary conditions:**

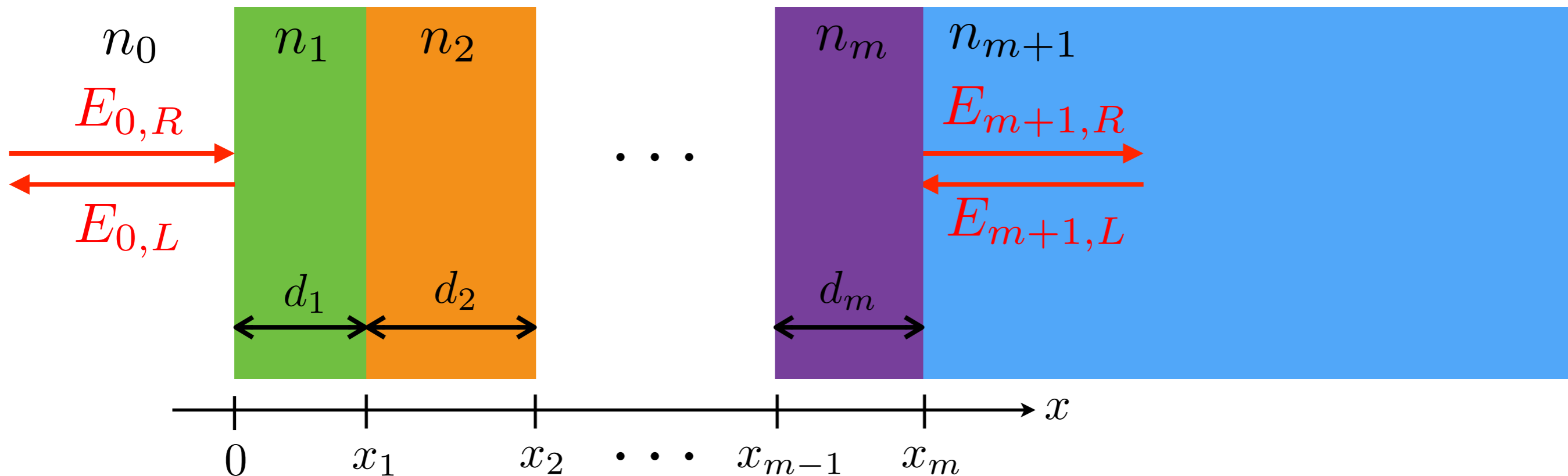
$$\begin{pmatrix} E_1(d_1, t) \\ \frac{\partial E_1}{\partial x}(d_1, t) \end{pmatrix} = \begin{pmatrix} E_2(d_1, t) \\ \frac{\partial E_2}{\partial x}(d_1, t) \end{pmatrix} = M_1 \begin{pmatrix} E_0(0, t) \\ \frac{\partial E_0}{\partial x}(0, t) \end{pmatrix} = M_1 \begin{pmatrix} E_1(0, t) \\ \frac{\partial E_1}{\partial x}(0, t) \end{pmatrix}$$

$$\begin{pmatrix} E_{1,R}e^{ik_1d_1} + E_{1,L}e^{-ik_1d_1} \\ ik_1E_{1,R}e^{ik_1d_1} - ik_1E_{1,L}e^{-ik_1d_1} \end{pmatrix} = M_1 \begin{pmatrix} E_{1,R} + E_{1,L} \\ ik_1E_{1,R} - ik_1E_{1,L} \end{pmatrix}$$

**Transfer matrix  $M_1$  can be obtained by solving equations above:**

$$M_1 = \begin{pmatrix} \cos(k_1d_1), & \frac{\sin(k_1d_1)}{k_1} \\ -k_1 \sin(k_1d_1), & \cos(k_1d_1) \end{pmatrix}$$

# Transfer matrices



**Transfer matrix for  $m$  layers:**

$$\begin{pmatrix} E_{m+1}(x_m, t) \\ \frac{\partial E_{m+1}}{\partial x}(x_m, t) \end{pmatrix} = M_m \begin{pmatrix} E_m(x_{m-1}, t) \\ \frac{\partial E_m}{\partial x}(x_{m-1}, t) \end{pmatrix} = M_m M_{m-1} \begin{pmatrix} E_{m-1}(x_{m-2}, t) \\ \frac{\partial E_{m-1}}{\partial x}(x_{m-2}, t) \end{pmatrix} = \dots$$

$$\begin{pmatrix} E_{m+1}(x_m, t) \\ \frac{\partial E_{m+1}}{\partial x}(x_m, t) \end{pmatrix} = M \begin{pmatrix} E_0(0, t) \\ \frac{\partial E_0}{\partial x}(0, t) \end{pmatrix}$$

$$M = M_m \cdot \dots \cdot M_2 \cdot M_1$$

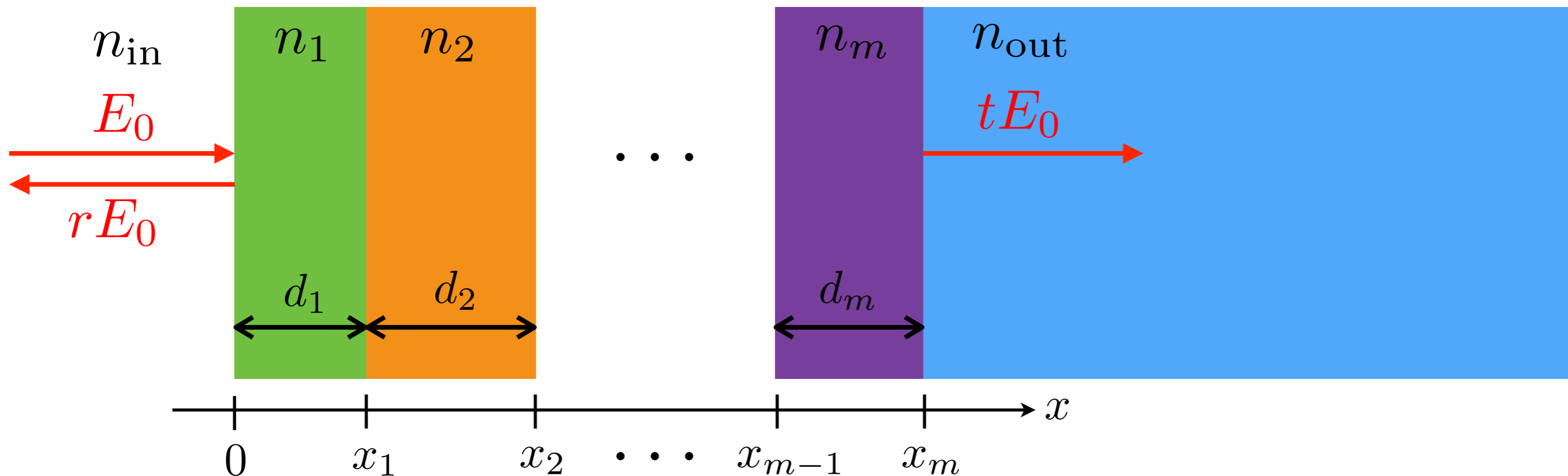
**Note:**

$$M_a = \begin{pmatrix} \cos(k_a d_a), & \frac{\sin(k_a d_a)}{k_a} \\ -k_a \sin(k_a d_a), & \cos(k_a d_a) \end{pmatrix}$$

$$\det(M) = \det(M_a) = 1$$

$$k_a = \frac{2\pi n_a}{\lambda} = \frac{n_a \omega}{c_0}$$

# Transfer matrices



**Incoming and outgoing electromagnetic waves:**

$$E_{\text{in}}(x, t) = E_0 e^{i(k_{\text{in}}x - \omega t)} + rE_0 e^{i(-k_{\text{in}}x - \omega t)}$$

$$E_{\text{out}}(x, t) = tE_0 e^{i(k_{\text{out}}x - \omega t)}$$

$$\begin{pmatrix} E_{\text{out}}(x_m, t) \\ \frac{\partial E_{\text{out}}}{\partial x}(x_m, t) \end{pmatrix} = \begin{pmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{pmatrix} \begin{pmatrix} E_{\text{in}}(0, t) \\ \frac{\partial E_{\text{in}}}{\partial x}(0, t) \end{pmatrix}$$

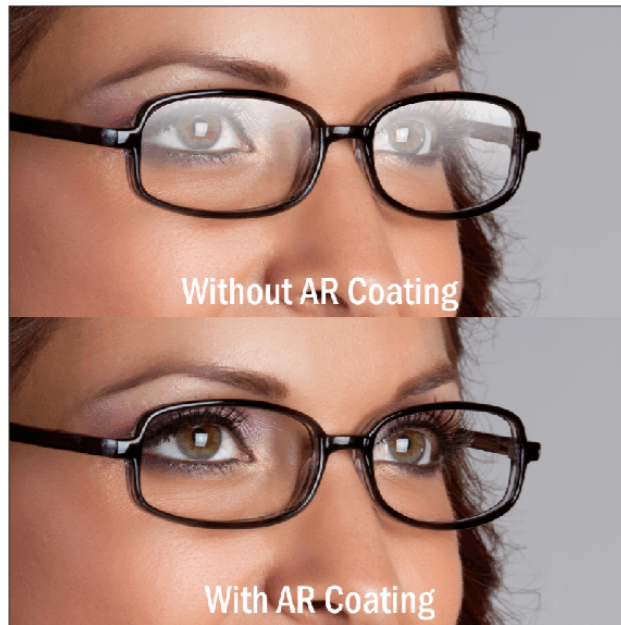
**Amplitudes of reflected and transmitted waves:**

$$r = \frac{(M_{21} + k_{\text{in}}k_{\text{out}}M_{12}) + i(k_{\text{in}}M_{22} - k_{\text{out}}M_{11})}{(-M_{21} + k_{\text{in}}k_{\text{out}}M_{12}) + i(k_{\text{out}}M_{11} + k_{\text{in}}M_{22})}$$

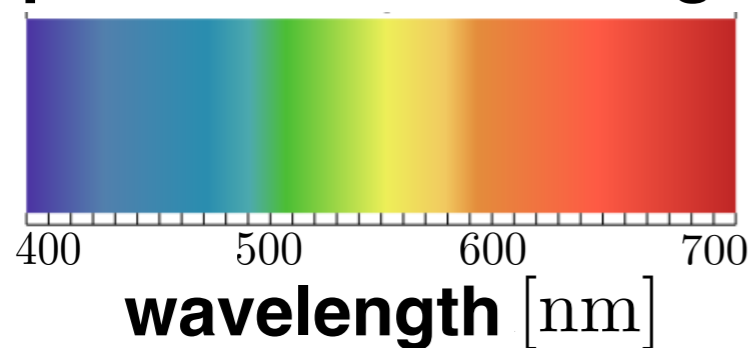
$$t = \frac{2ik_{\text{in}}e^{-ix_mk_{\text{out}}}}{(-M_{21} + k_{\text{in}}k_{\text{out}}M_{12}) + i(k_{\text{out}}M_{11} + k_{\text{in}}M_{22})}$$

# Example: antireflective coating

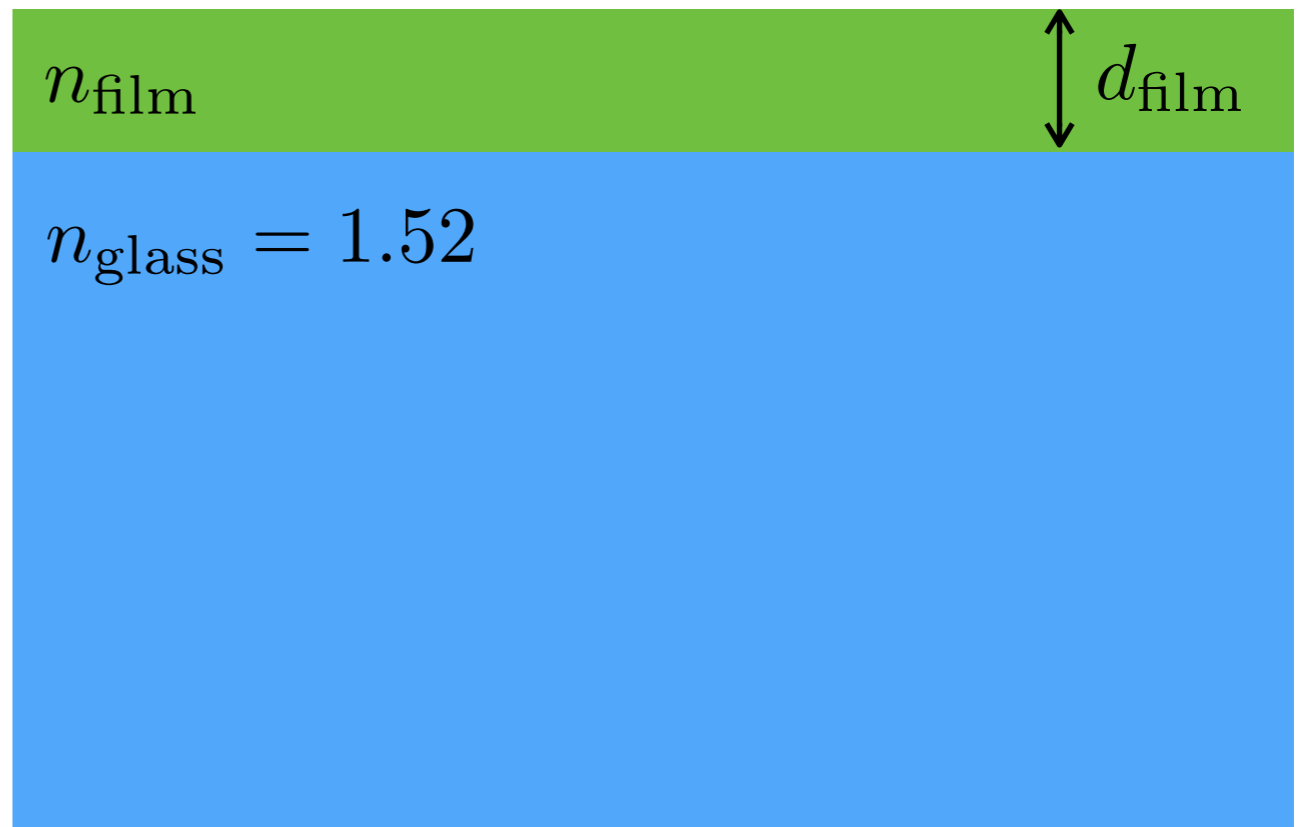
We would like to design a thin film coating for glasses that minimizes reflection of visible light.



spectrum of visible light



$$n_{\text{air}} \approx 1$$



Assume that thin film is made of  $\text{MgF}_2$  that can be easily applied with physical vapor deposition:

$$n_{\text{film}} = 1.38$$

Note: the condition for destructive interference of reflected rays can be satisfied only for discrete set of wavelengths  $\lambda_0$  :

$$2d_{\text{film}}n_{\text{film}} = \left(m + \frac{1}{2}\right)\lambda_0$$
$$m = 0, 1, 2, \dots$$

# Example: antireflective coating

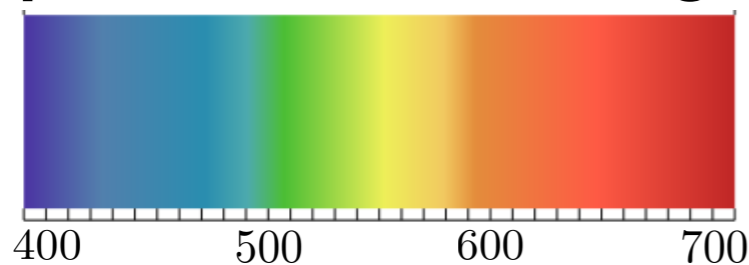
$$n_{\text{air}} \approx 1$$

$$n_{\text{film}} = 1.38$$

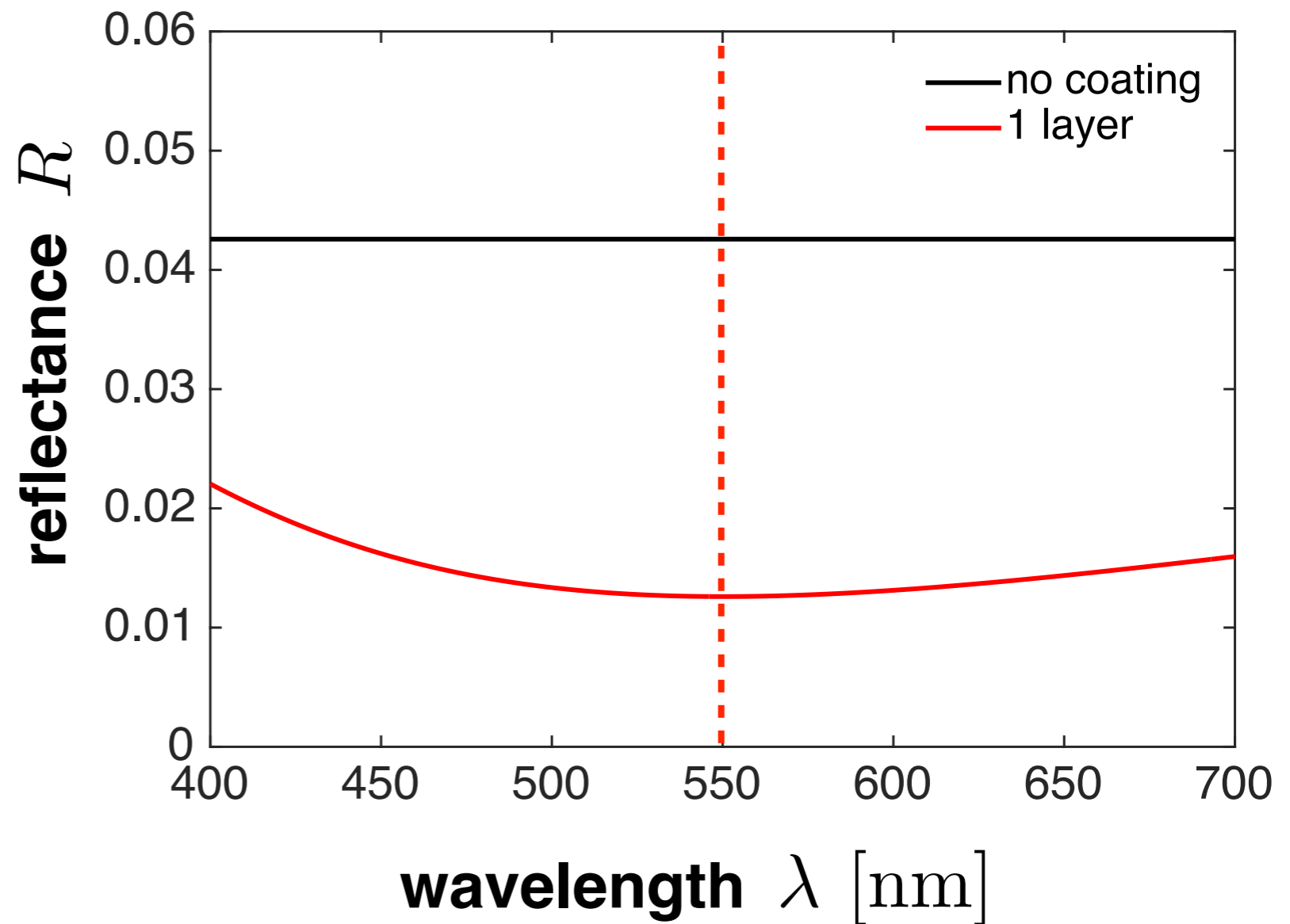
 $d_{\text{film}}$ 

$$n_{\text{glass}} = 1.52$$

spectrum of visible light



wavelength [nm]



Use film thickness that corresponds to the destructive interference for the wavelength in the middle of the visible spectrum  $\lambda_{\text{target}} = 550$  nm:

$$d_{\text{film}} = \frac{\lambda_{\text{target}}}{4n_{\text{film}}} = 100 \text{ nm}$$

# Example: antireflective coating

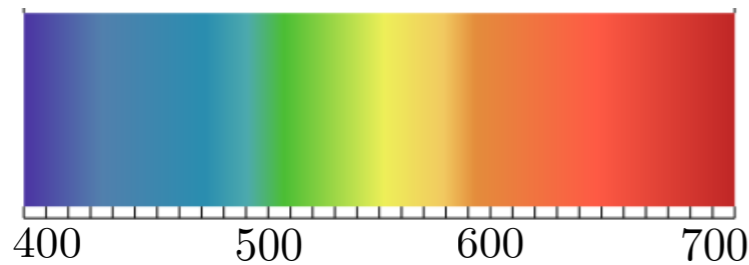
$$n_{\text{air}} \approx 1$$

$$n_{\text{film}} = 1.38$$

 $d_{\text{film}}$ 

$$n_{\text{glass}} = 1.52$$

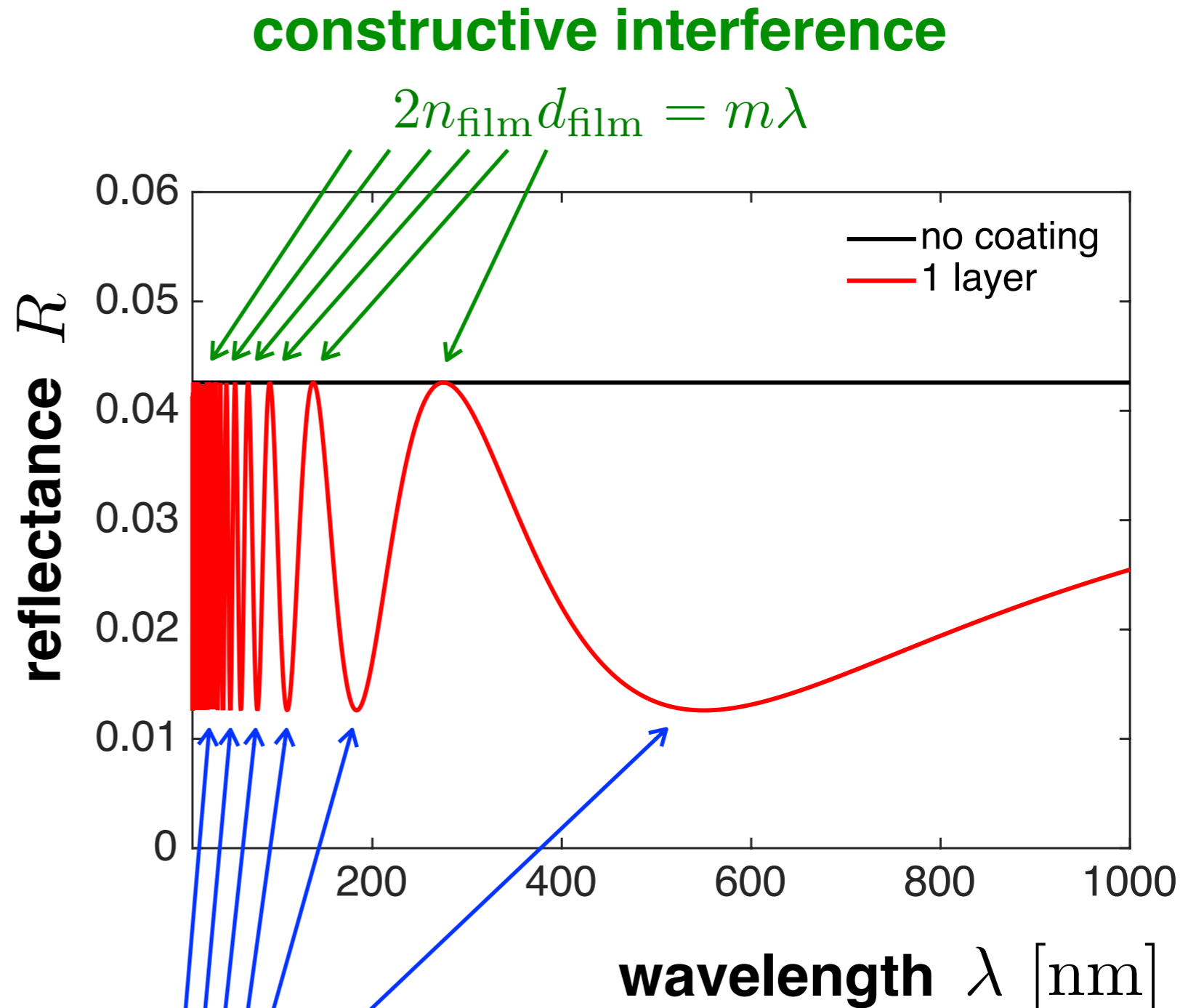
spectrum of visible light



wavelength [nm]

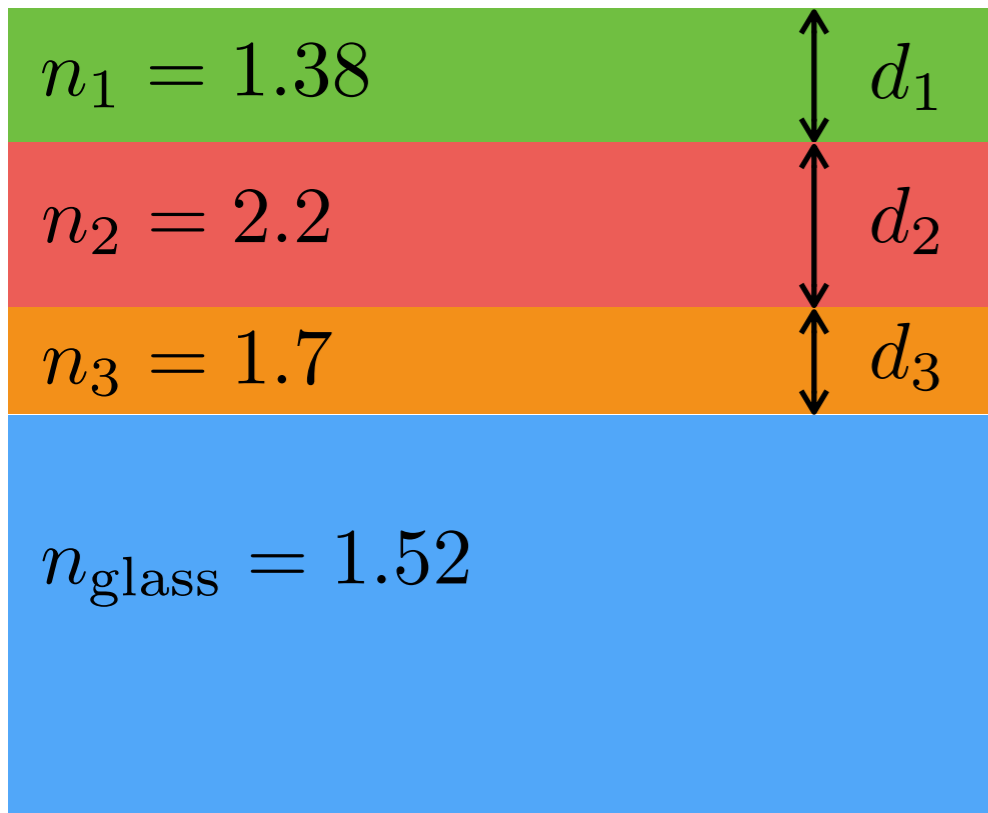
$$\lambda_{\text{target}} = 550 \text{ nm}$$

$$d_{\text{film}} = \frac{\lambda_{\text{target}}}{4n_{\text{film}}} = 100 \text{ nm}$$

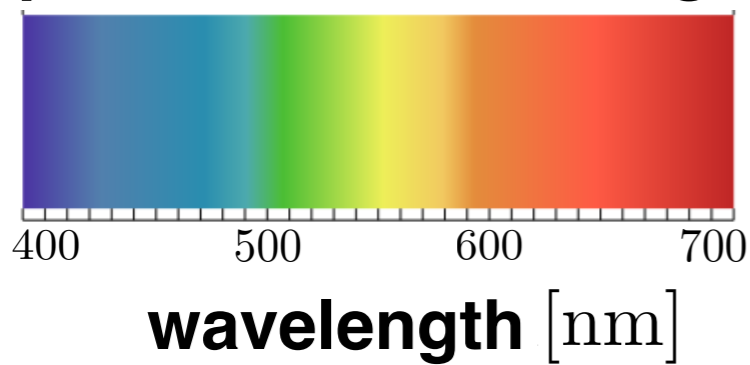


# Example: antireflective coating

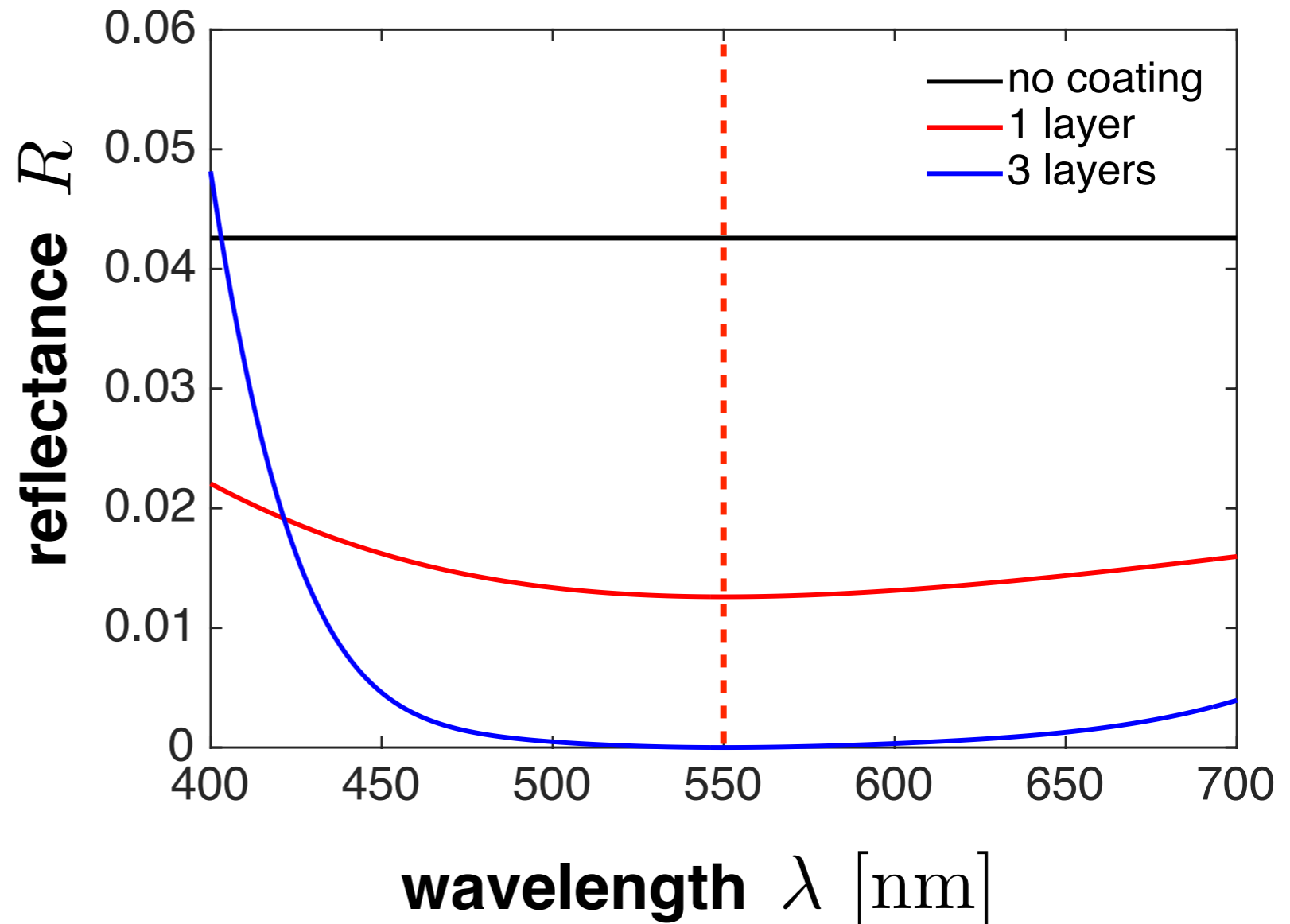
$$n_{\text{air}} \approx 1$$



spectrum of visible light



Multiple layers of coating significantly reduce the reflectance of visible spectrum!



Use film thicknesses that correspond to the destructive interference for the wavelength in the middle of the visible spectrum  $\lambda_{\text{target}} = 550 \text{ nm}$ :

$$d_1 = \lambda_{\text{target}} / (4n_1)$$

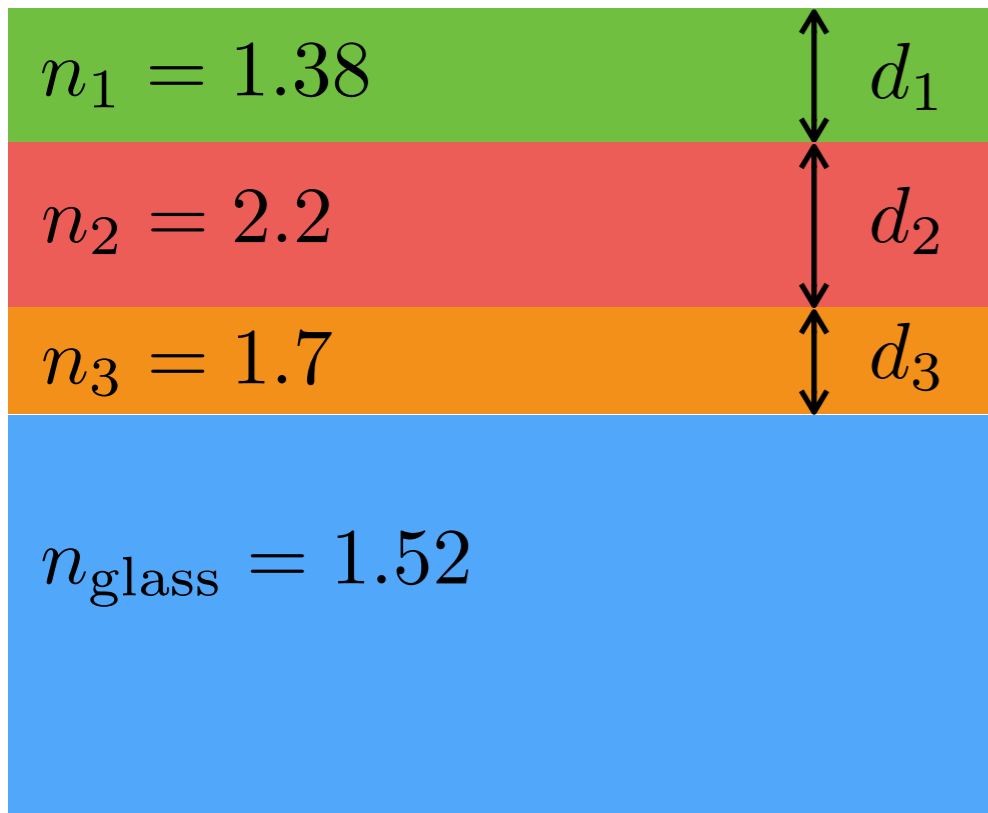
$$d_2 = \lambda_{\text{target}} / (2n_2)$$

$$d_3 = \lambda_{\text{target}} / (4n_3)$$

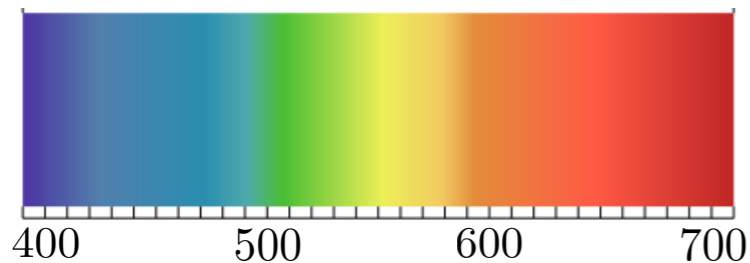
note the additional phase difference!

# Example: antireflective coating

$$n_{\text{air}} \approx 1$$



spectrum of visible light



wavelength [nm]

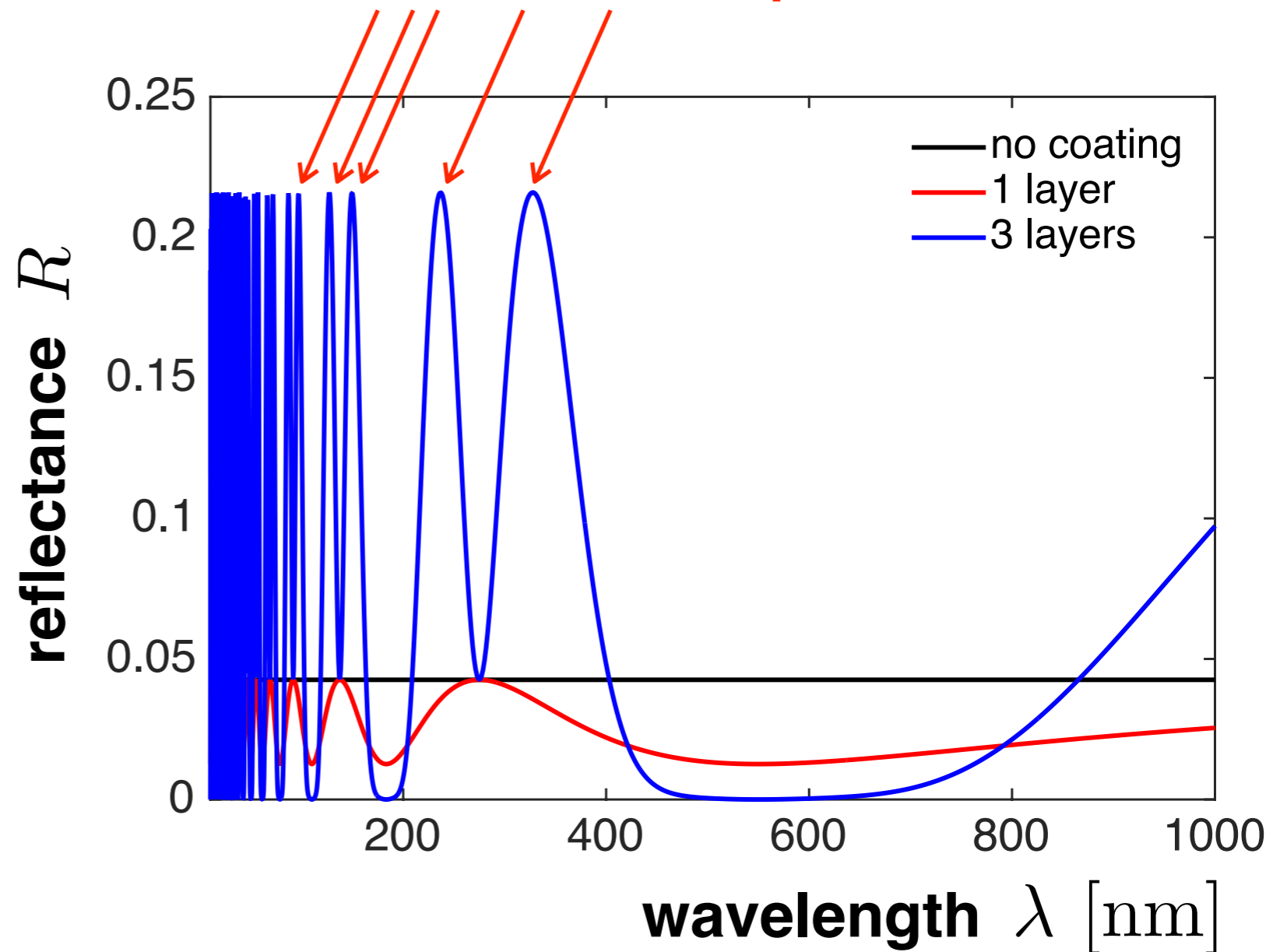
$$\lambda_{\text{target}} = 550 \text{ nm}$$

$$d_1 = \lambda_{\text{target}} / (4n_1)$$

$$d_2 = \lambda_{\text{target}} / (2n_2)$$

$$d_3 = \lambda_{\text{target}} / (4n_3)$$

Multiple layers of coating significantly enhance reflectance of certain wavelengths outside the visible spectrum!



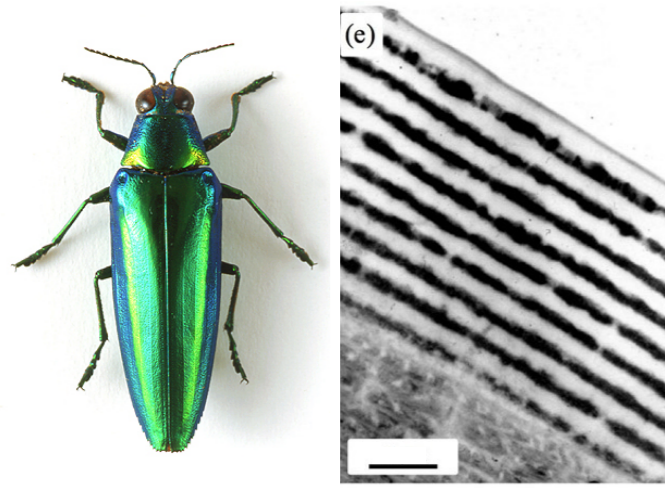
Additional peaks (minima) correspond to the constructive (deconstructive) interference for rays scattered on different combination of interfaces.



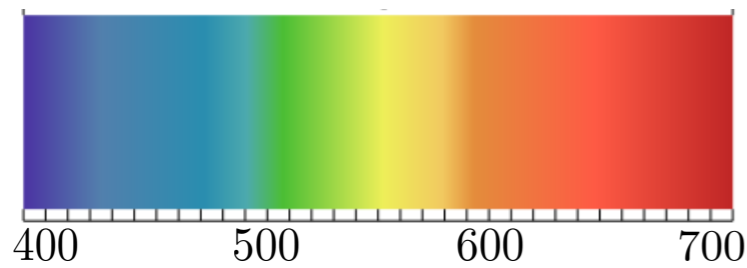
# Example: structural color

**Chrysochroa raja beetle**

We would like to design periodic structure, which preferentially reflects green color with  $\lambda_0 = 500 \text{ nm}$ .



$1 \mu\text{m}$



wavelength [nm]

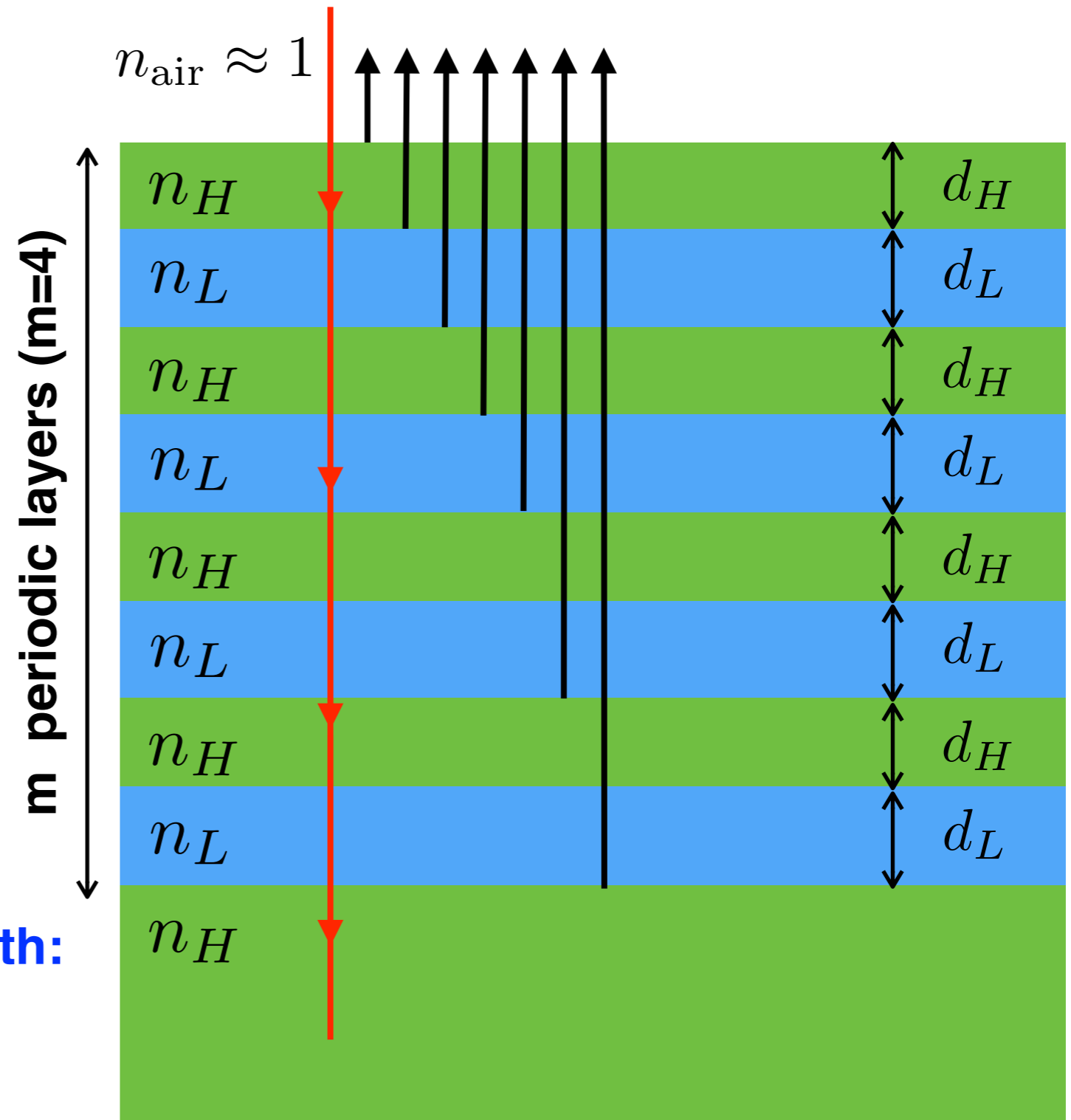
**Typical refraction indices:**

$$n_H = 1.69 \quad n_L = 1.56$$

**Constructive interference of reflected rays can be achieved with:**

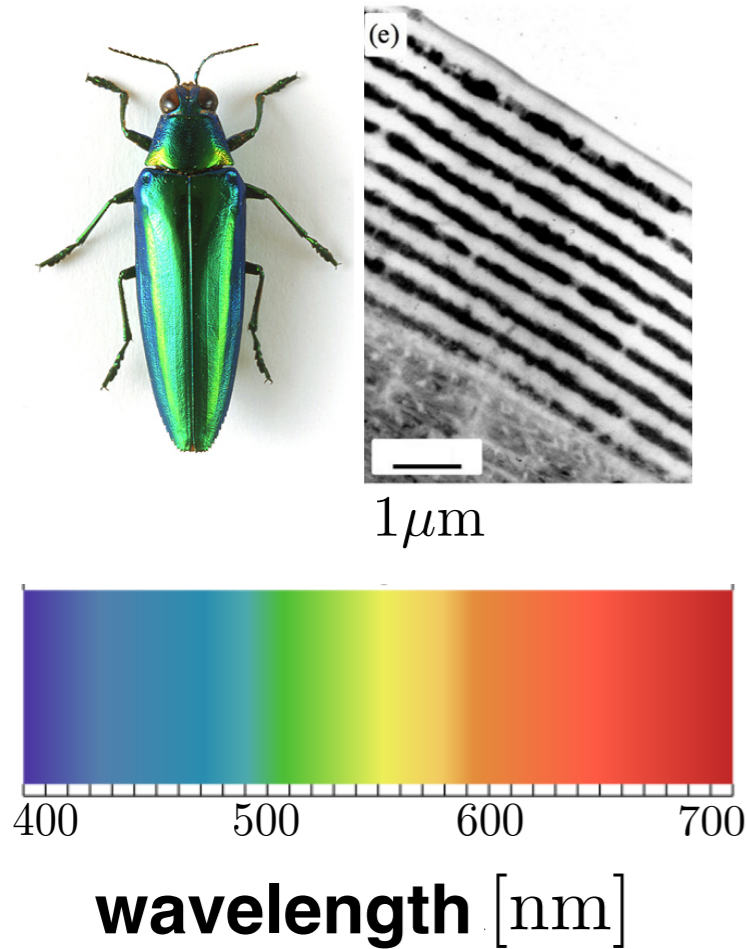
$$d_H = \frac{\lambda_0}{4n_H} = 74 \text{ nm}$$

$$d_L = \frac{\lambda_0}{4n_L} = 80 \text{ nm}$$

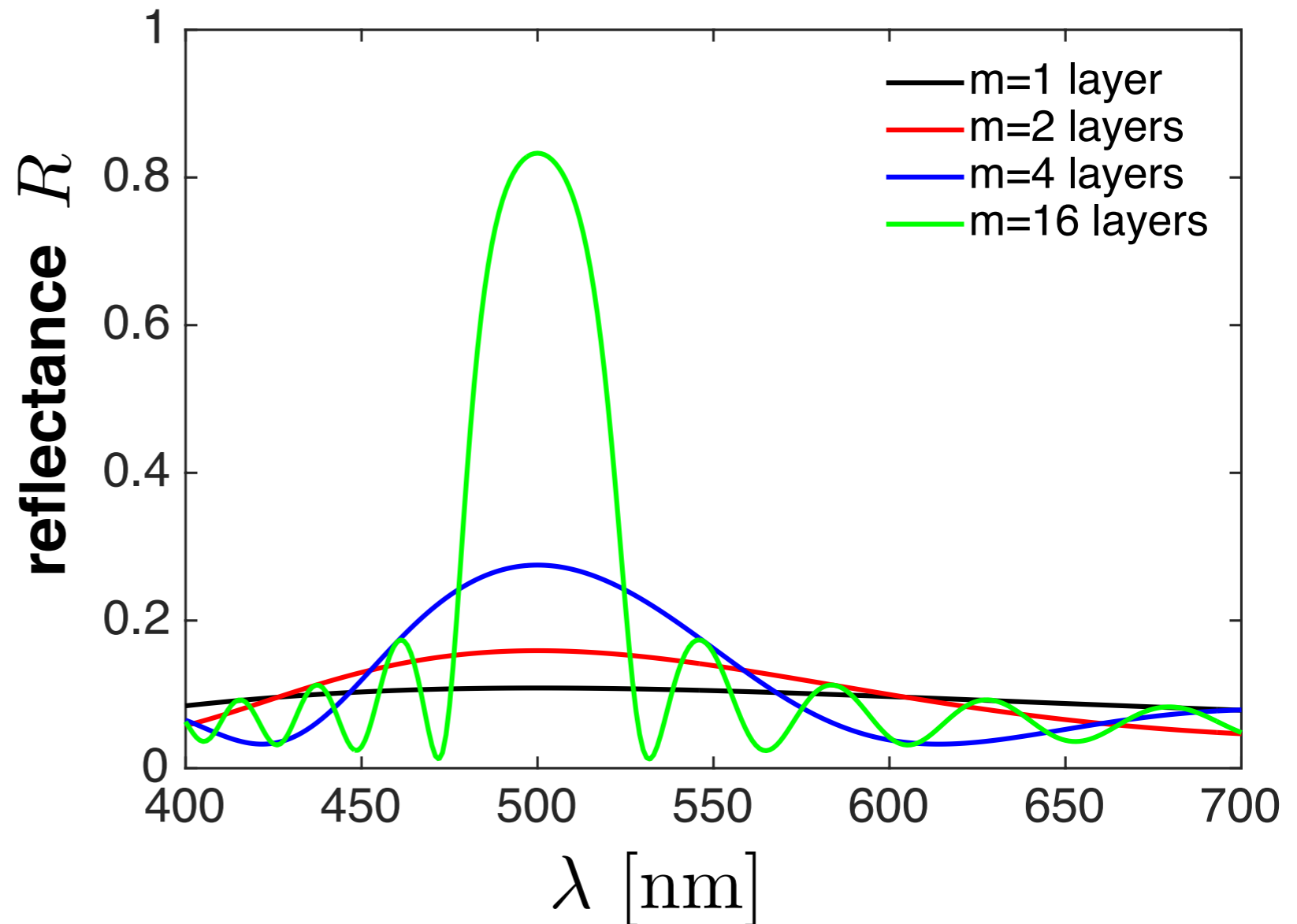


# Example: structural color

## Chrysochroa raja beetle

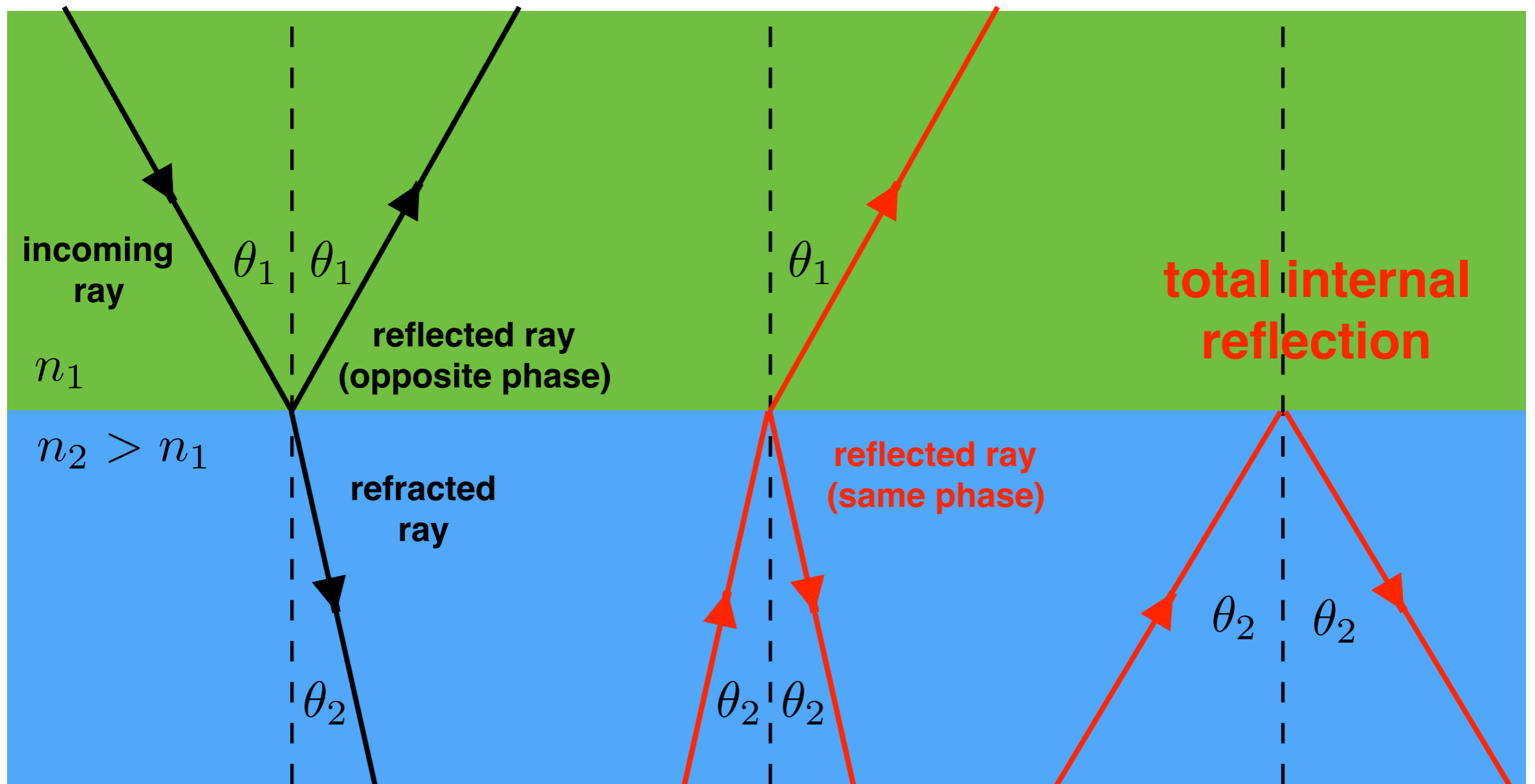


Multiple periodic layers increase the reflectance of target wavelength  $\lambda_0 = 500\text{ nm}$ !



In periodic structures high reflectance is achieved for a range of wavelengths around the target wavelength. This range is called band gap.

# Refraction of light



**Snell's law**

$$n_1 \sin \theta_1 = n_2 \sin \theta_2$$

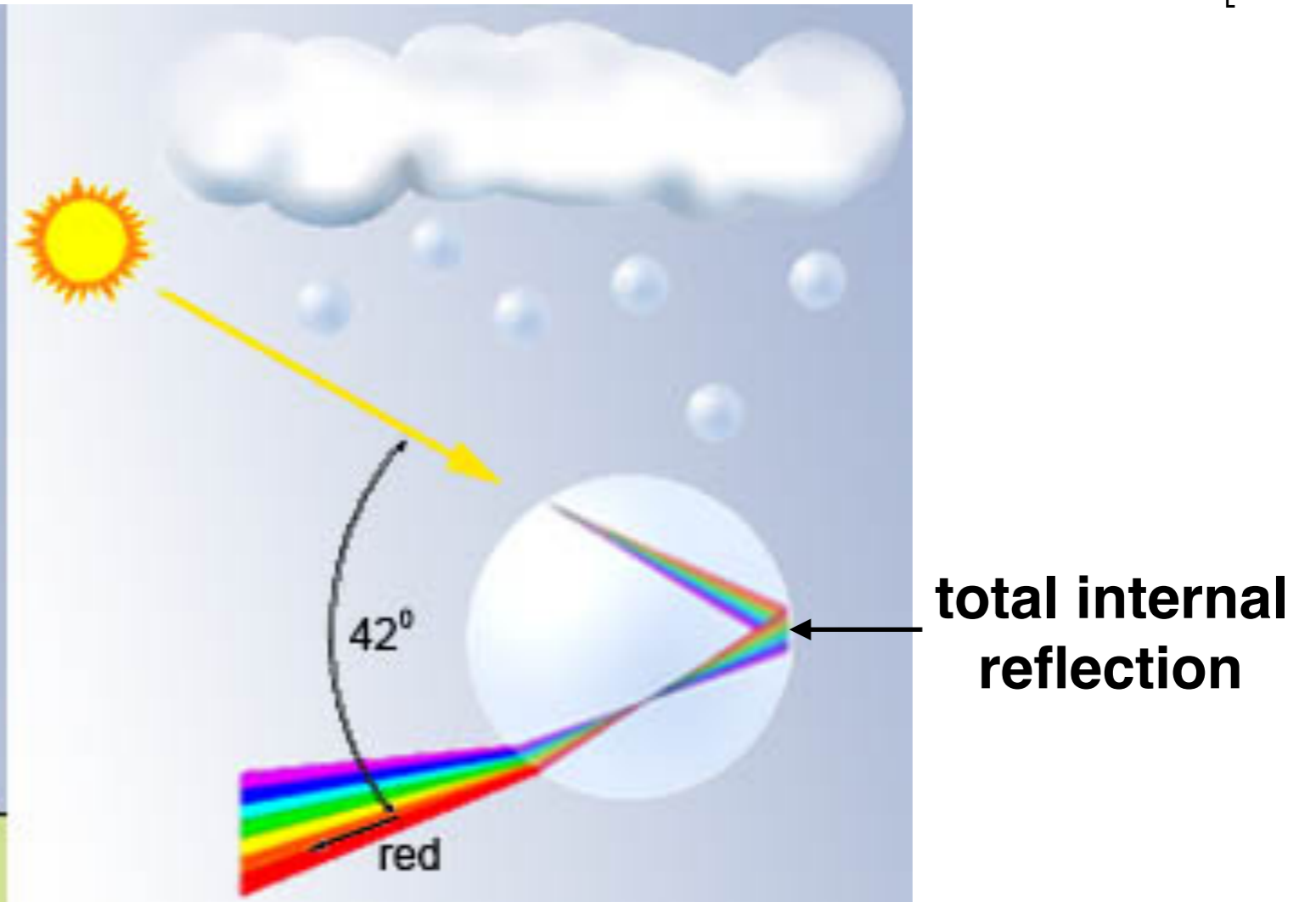
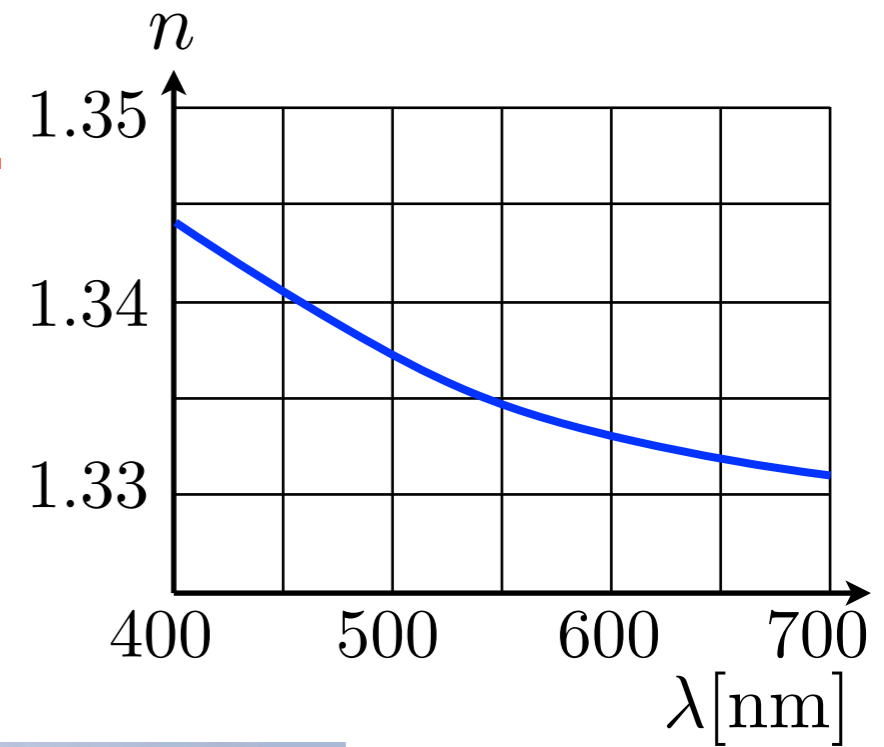
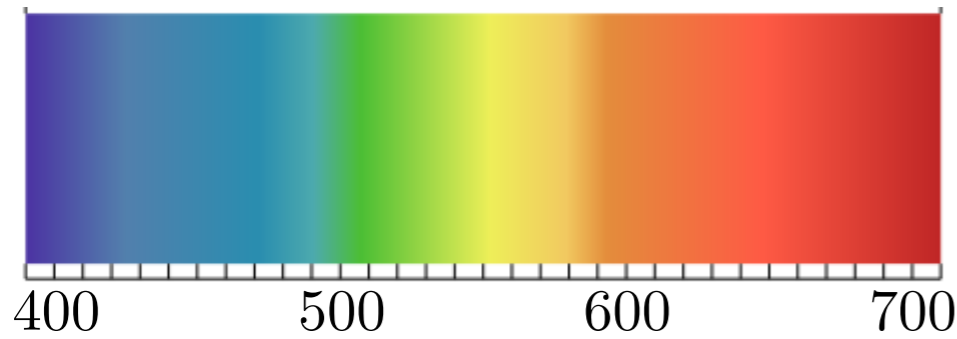
**Total internal reflection**

$$\theta_2 > \arcsin(n_1/n_2)$$

# Rainbow

Rainbow forms because refraction index  $n$  in water droplets depends on the color (wavelength) of light.

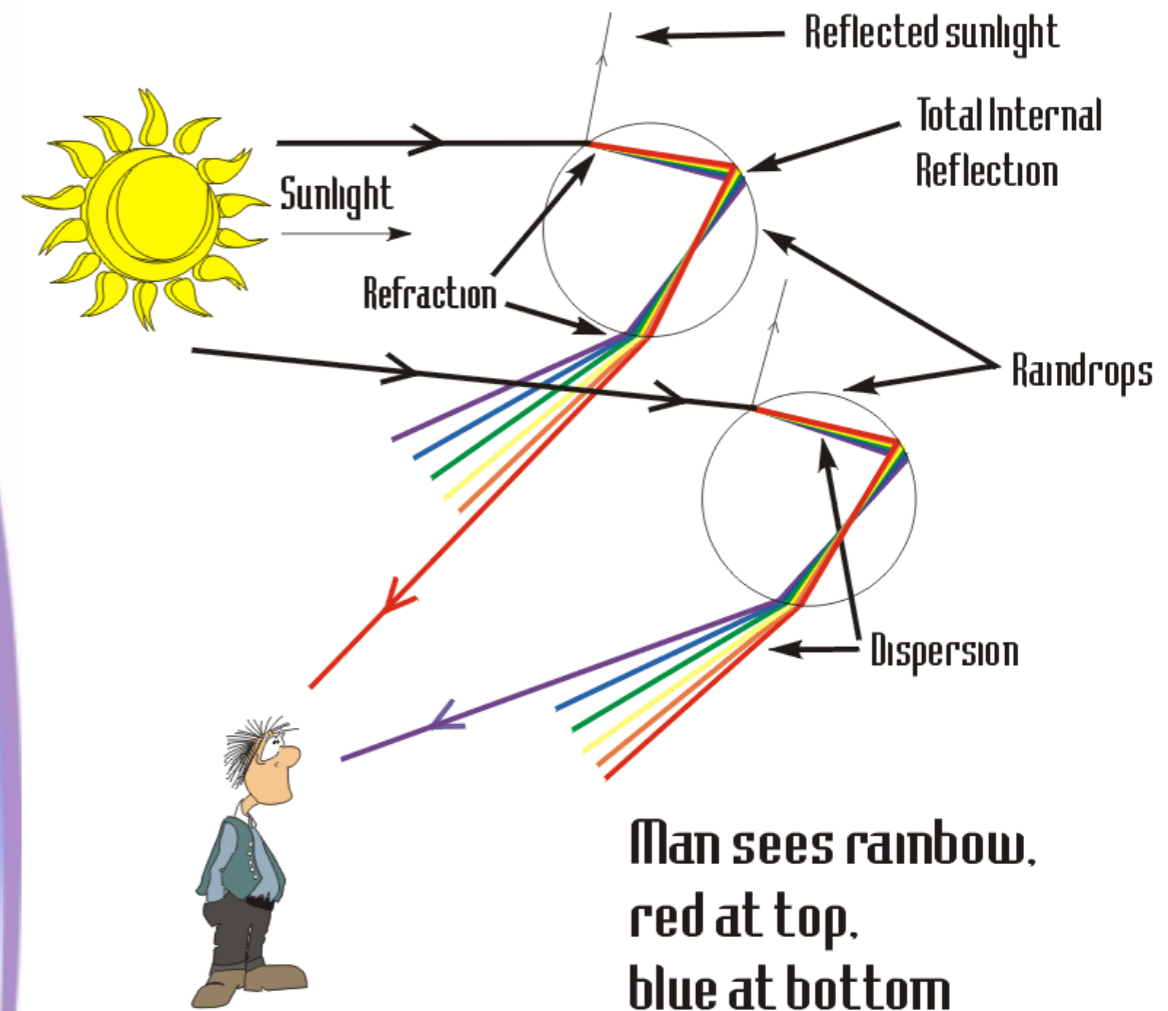
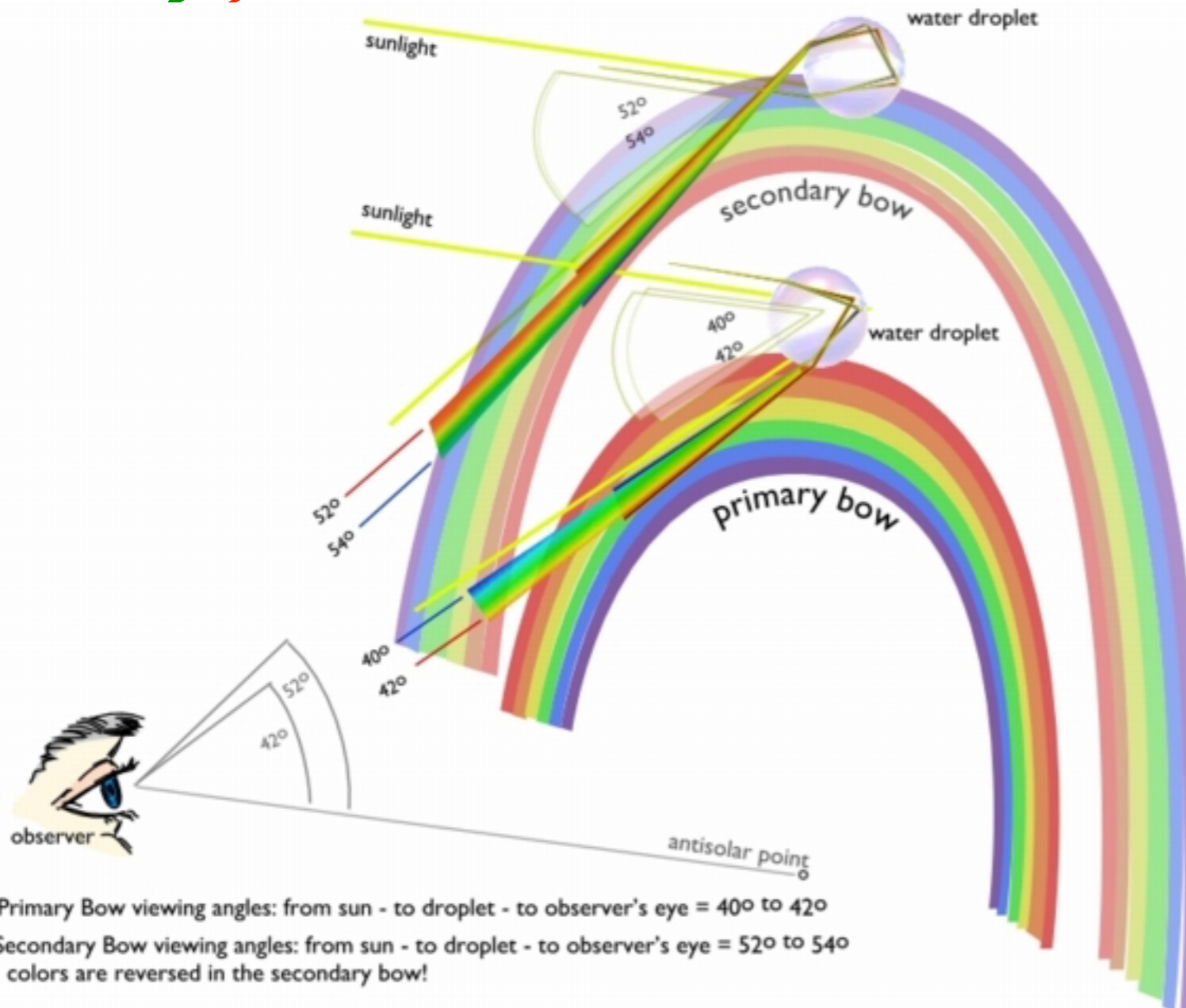
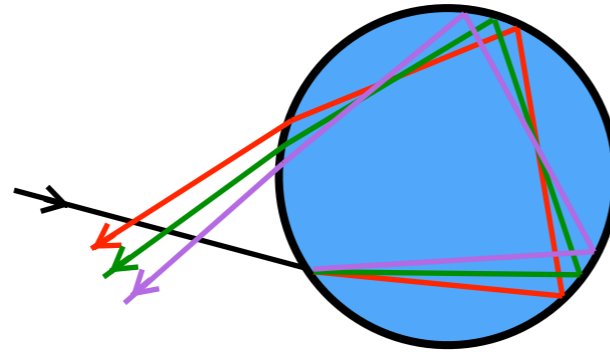
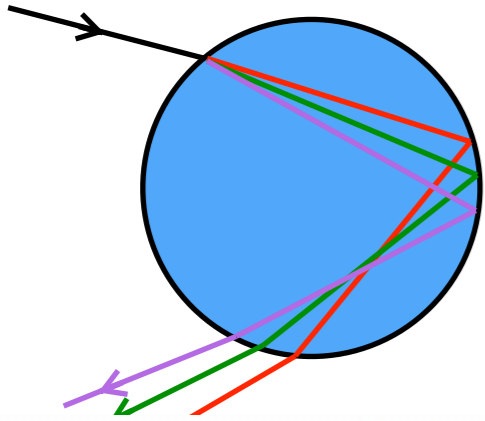
$$n_{\text{purple}} > n_{\text{blue}} > n_{\text{green}} > n_{\text{yellow}} > n_{\text{orange}} > n_{\text{red}}$$



# Double Rainbow

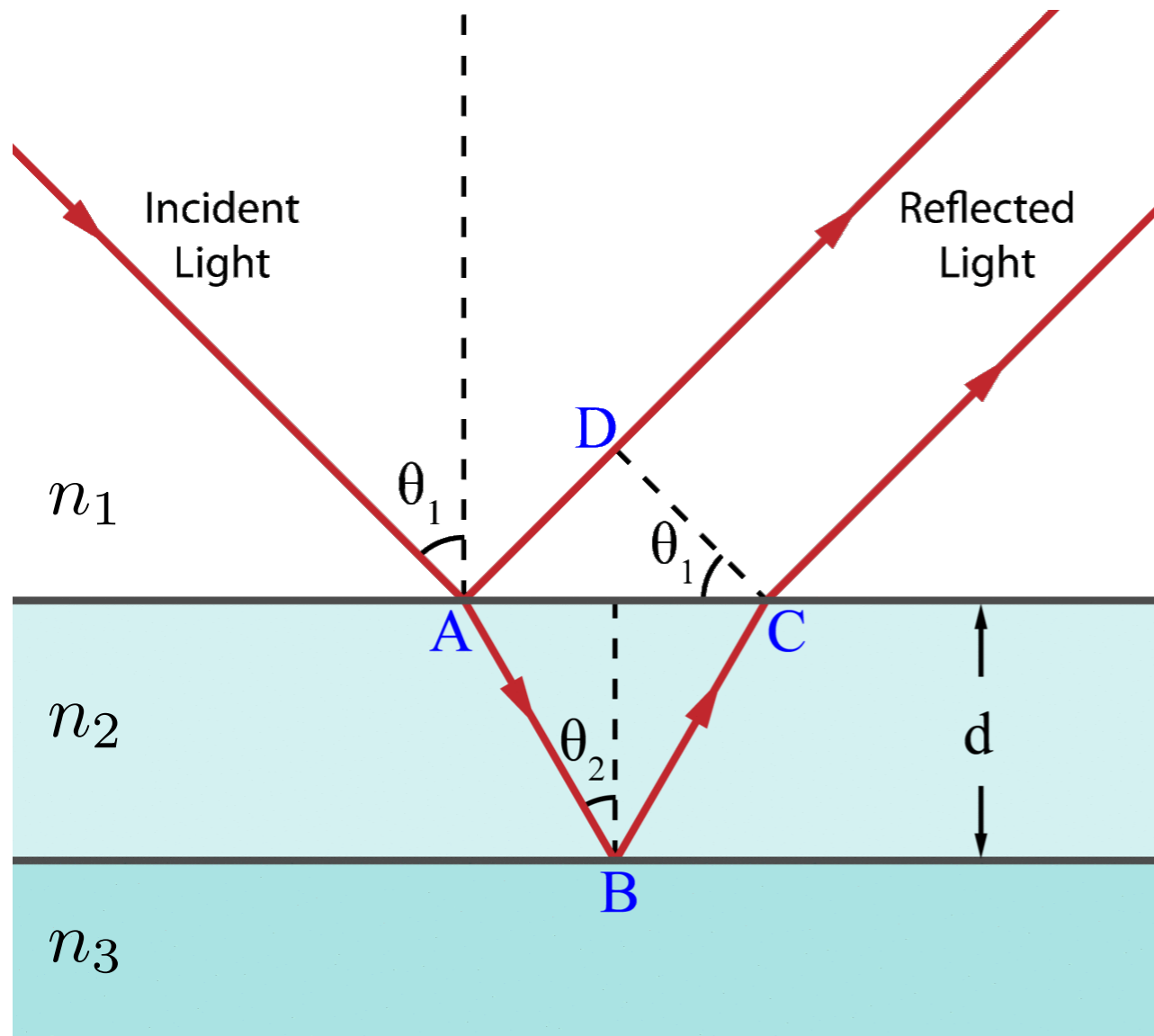
primary rainbow  
(1 internal reflection)

secondary rainbow  
(2 internal reflections)



Primary Bow viewing angles: from sun - to droplet - to observer's eye = 40° to 42°  
Secondary Bow viewing angles: from sun - to droplet - to observer's eye = 52° to 54°  
colors are reversed in the secondary bow!

# Interference on thin films



**difference between optical path lengths of the two reflected rays**

$$OPD = n_2 (\overline{AB} + \overline{BC}) - n_1 \overline{AD}$$

$$OPD = 2n_2 d \cos(\theta_2)$$

$$n_1 < n_2 < n_3 \quad n_1 > n_2 > n_3$$

**no additional phase**

**difference due to reflections**

**constructive interference of reflected rays**

$$OPD = m\lambda$$

**destructive interference of reflected rays**

$$OPD = \left(m + \frac{1}{2}\right) \lambda$$

$$m = 0, \pm 1, \pm 2, \dots$$

---


$$n_1 > n_2 < n_3 \quad n_1 < n_2 > n_3$$

**additional  $\pi$  phase**

**difference due to reflections**

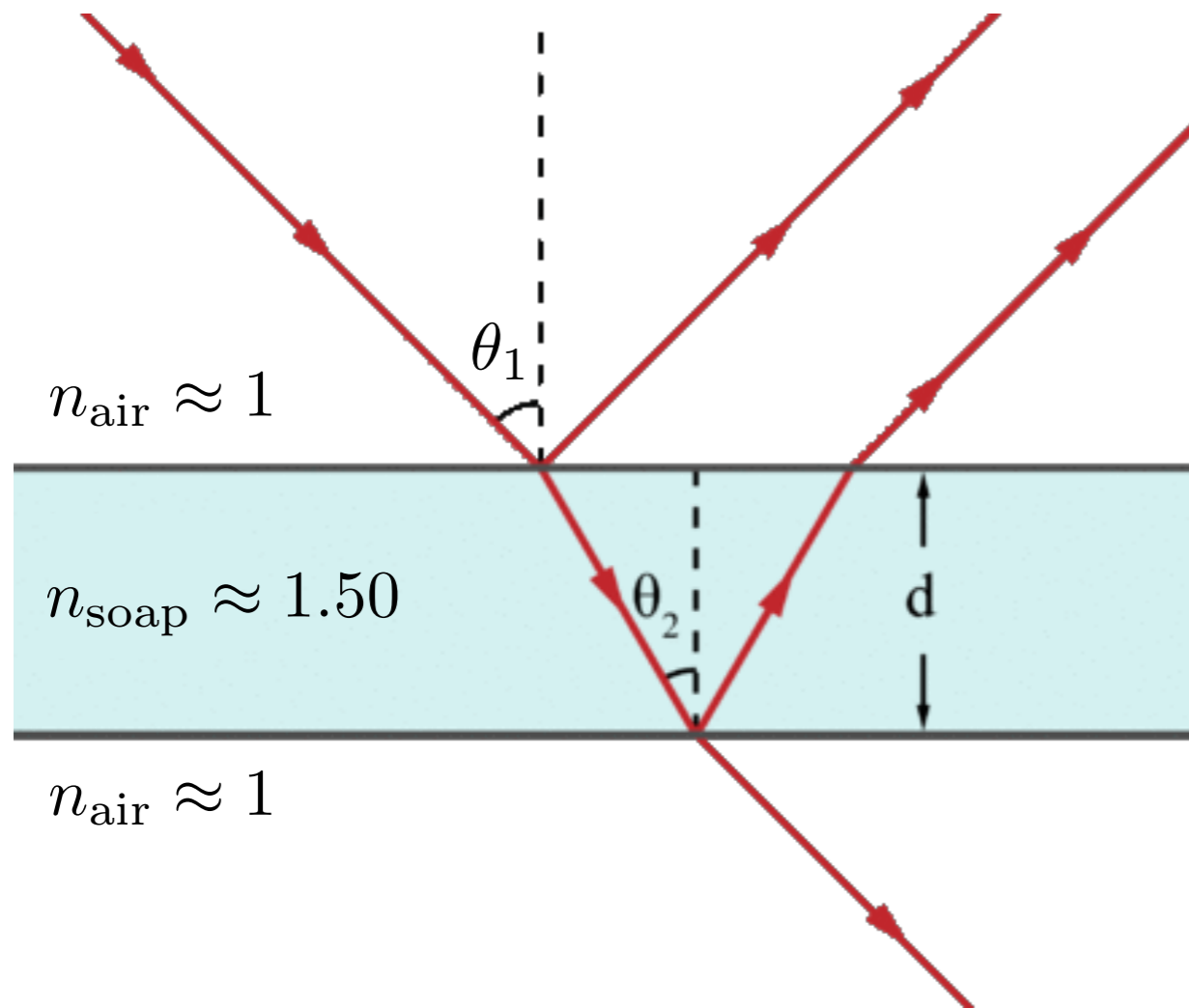
**constructive interference of reflected rays**

$$OPD = \left(m + \frac{1}{2}\right) \lambda$$

**destructive interference of reflected rays**

$$OPD = m\lambda$$

# Interference on soap bubbles



soap bubble

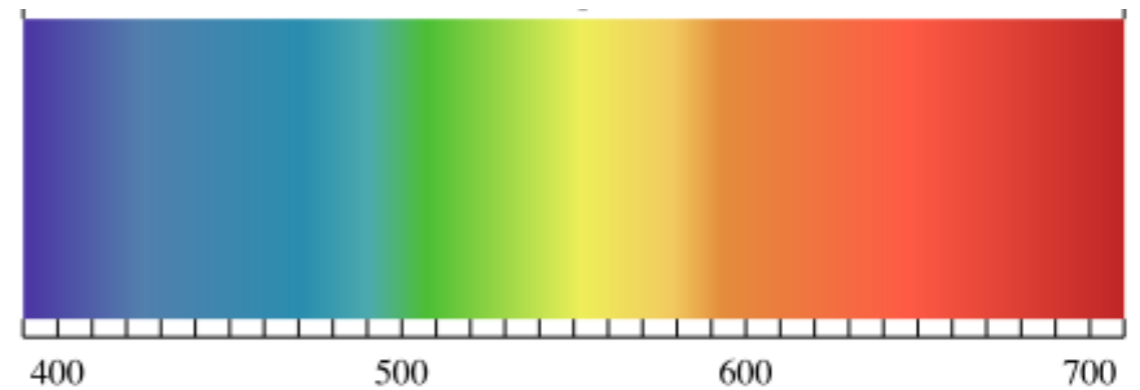


**constructive interference  
for different colors happens  
at different angles**

$$2dn_{\text{soap}} \cos(\theta_2) = (m + 1/2)\lambda$$

$$m = 0, \pm 1, \pm 2, \dots$$

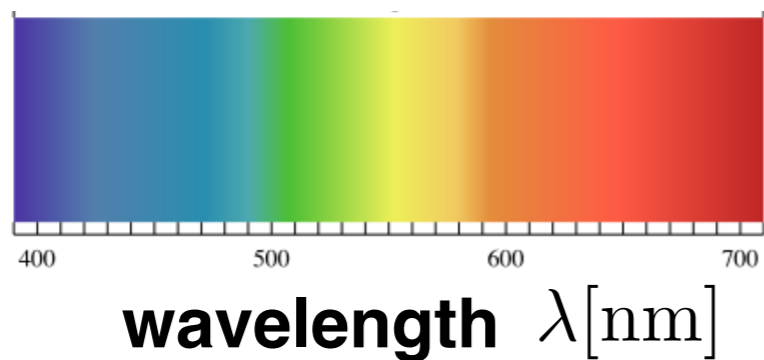
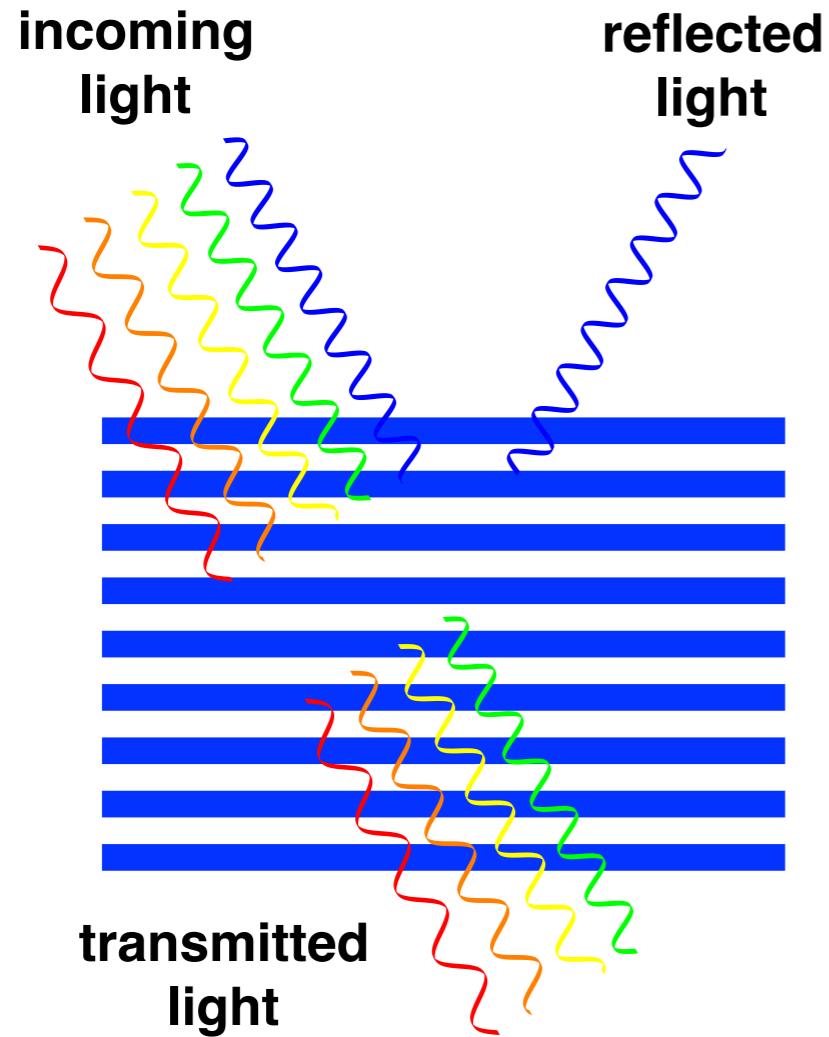
visible spectrum



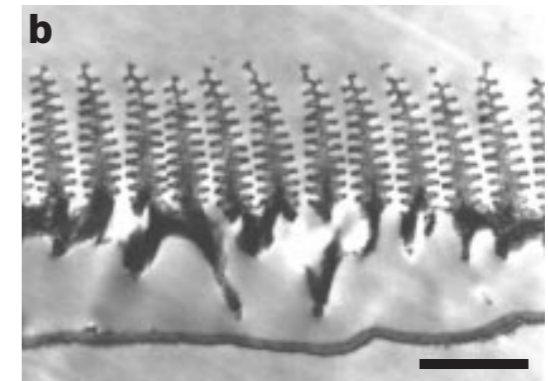
wavelength  $\lambda$ [nm]

# Structural colors on periodic structures

Single reflected color on structures with uniform spacing

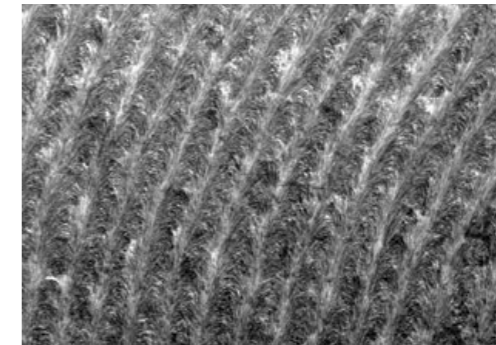


Morpho butterfly



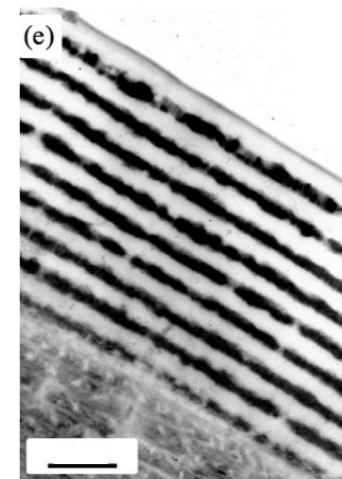
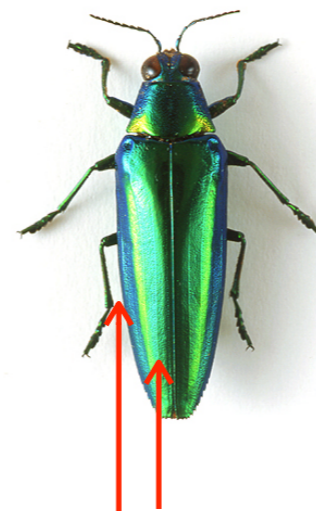
1.7  $\mu\text{m}$

Marble berry



250nm

Chrysochroa raja beetle



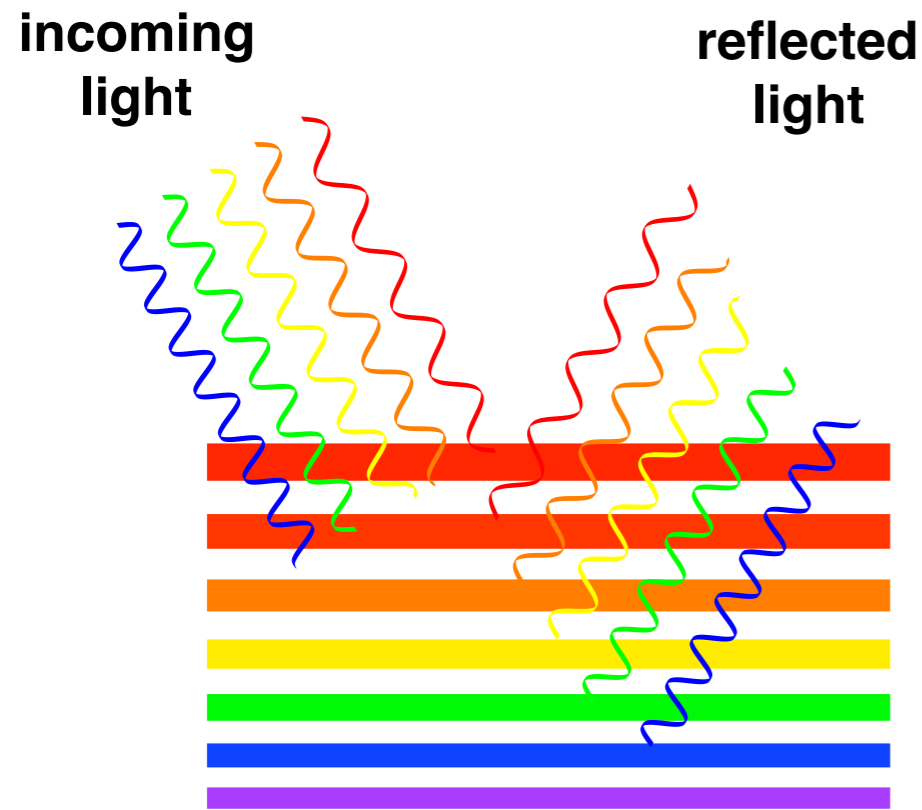
1  $\mu\text{m}$

reflected color depends on the viewing angle!



# Silver and gold structural colors

Many colors reflected on structures with varying spacing

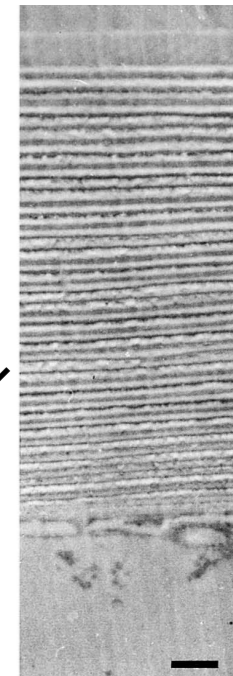


chirped structure

Chrysina limbata beetle



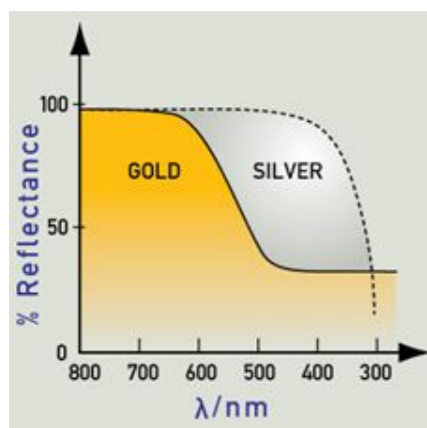
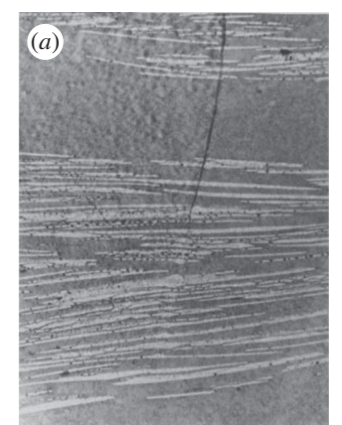
Chrysina aurigans beetle



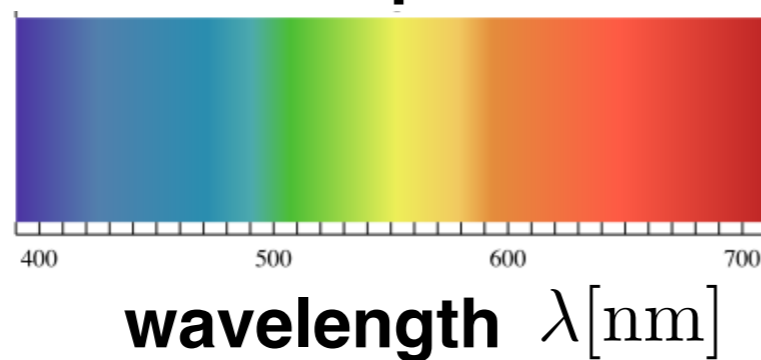
thicker  
↓  
thinner

disordered layer spacing

bleak fish

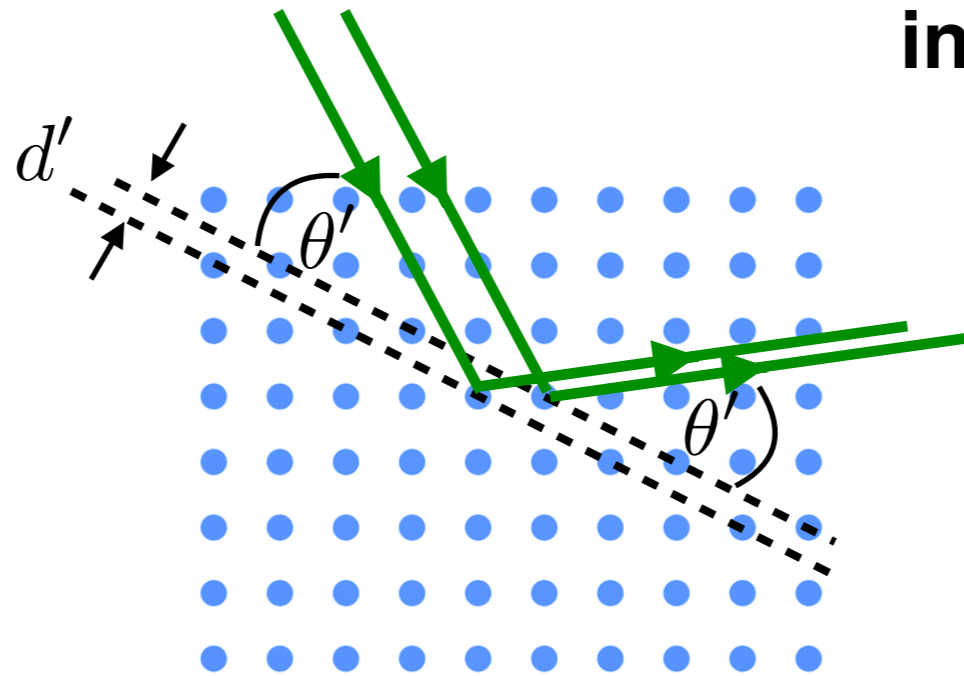
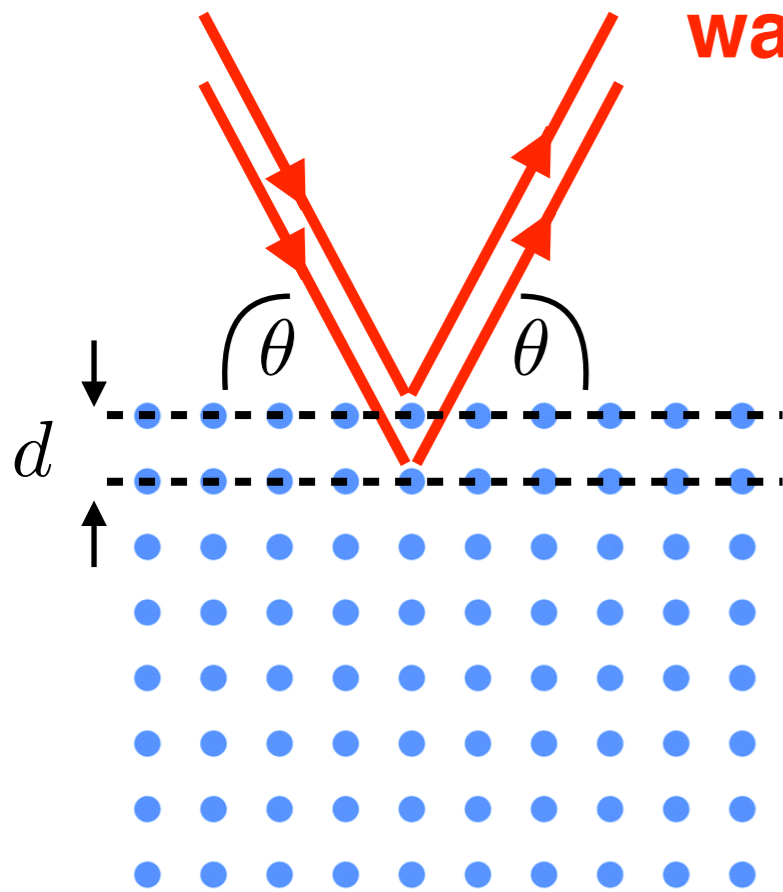


visible spectrum



# Bragg scattering on crystal layers

Constructive interference for waves with different wavelengths occurs in different crystal planes!



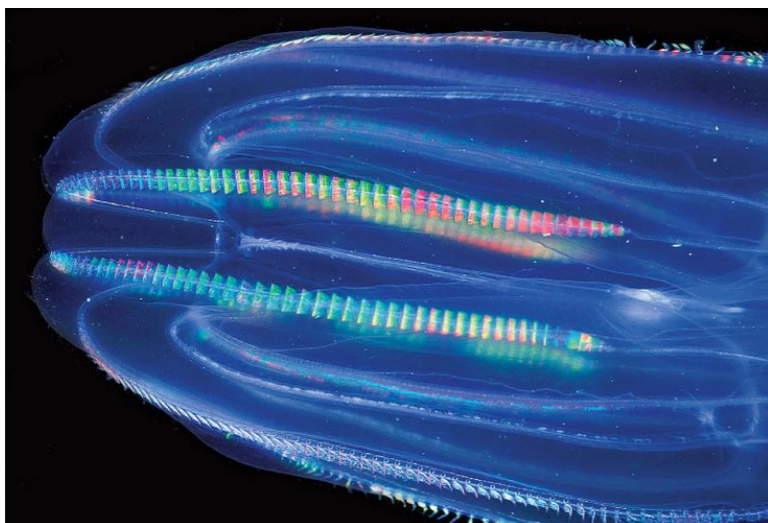
**constructive  
interference condition**

$$2d \sin \theta = m\lambda$$

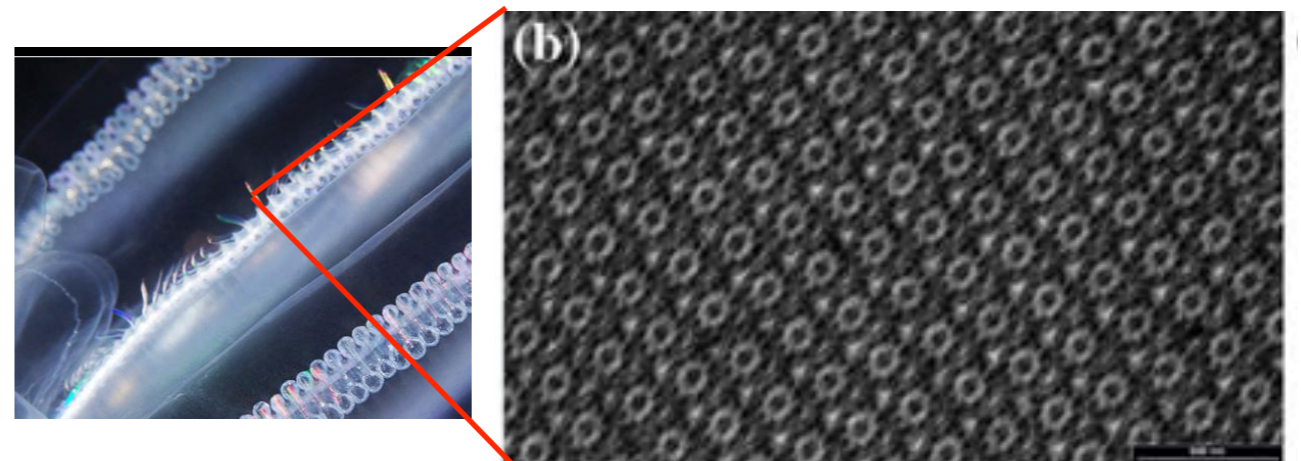
$$2d' \sin \theta' = m\lambda'$$

$$m = 0, \pm 1, \pm 2, \dots$$

**Comb jelly**



**Beating cilia are changing crystal orientation**

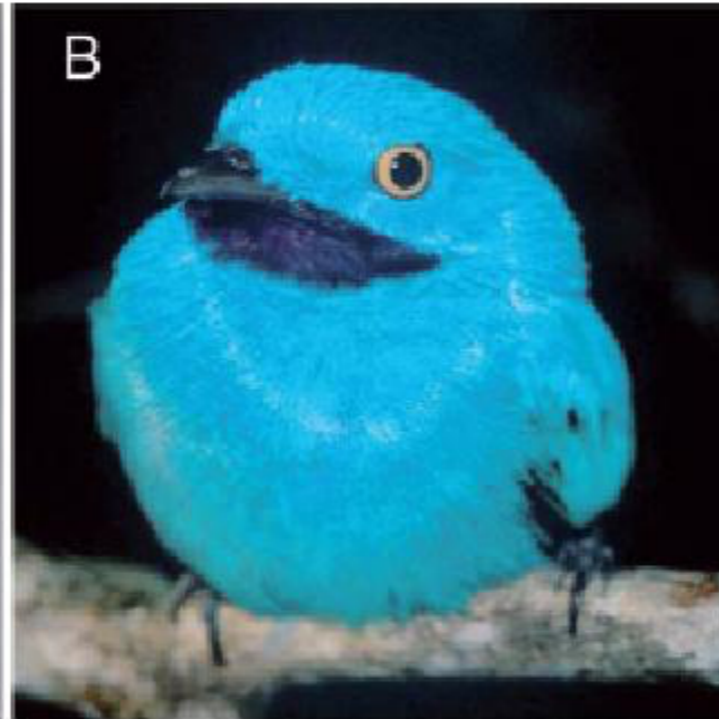


# Scattering on disordered structures

Eastern  
bluebird



Plum-throated  
Cotinga

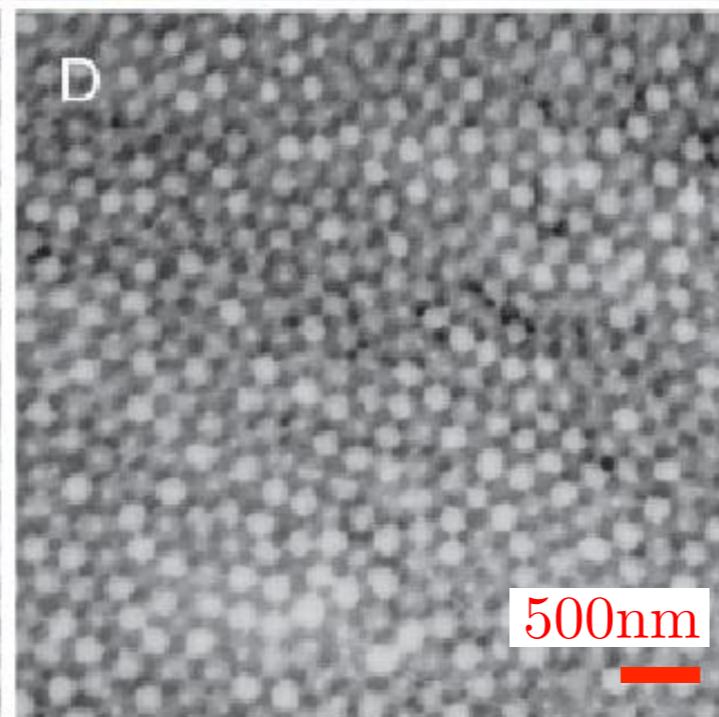
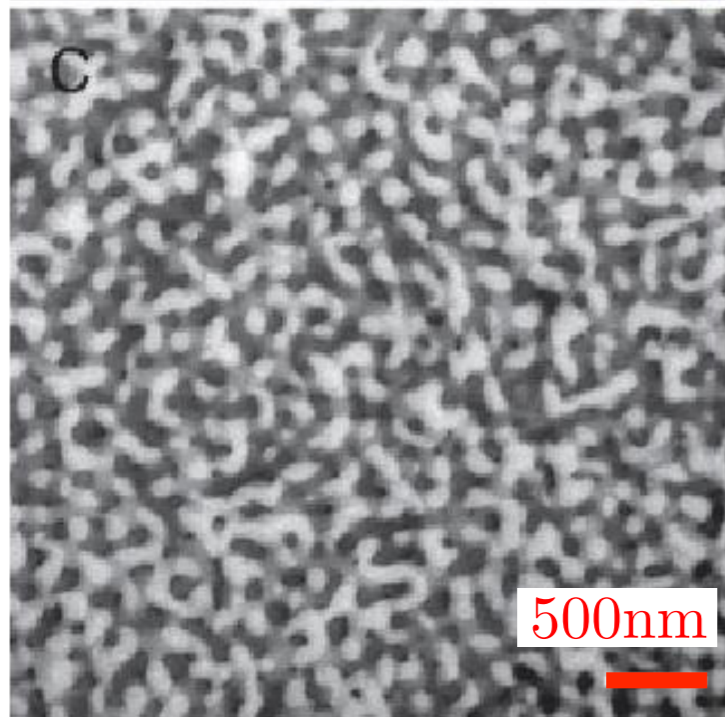


**Disordered structures with a characteristic length scale.**

**This length scale determines what light wavelengths are preferentially scattered.**

**The selectively reflected wavelengths are the same in all directions!**

**This gives rise to blue colors in these birds.**



V. Saranathan et al.,

J. R. Soc. Interface 9, 2563 (2012)

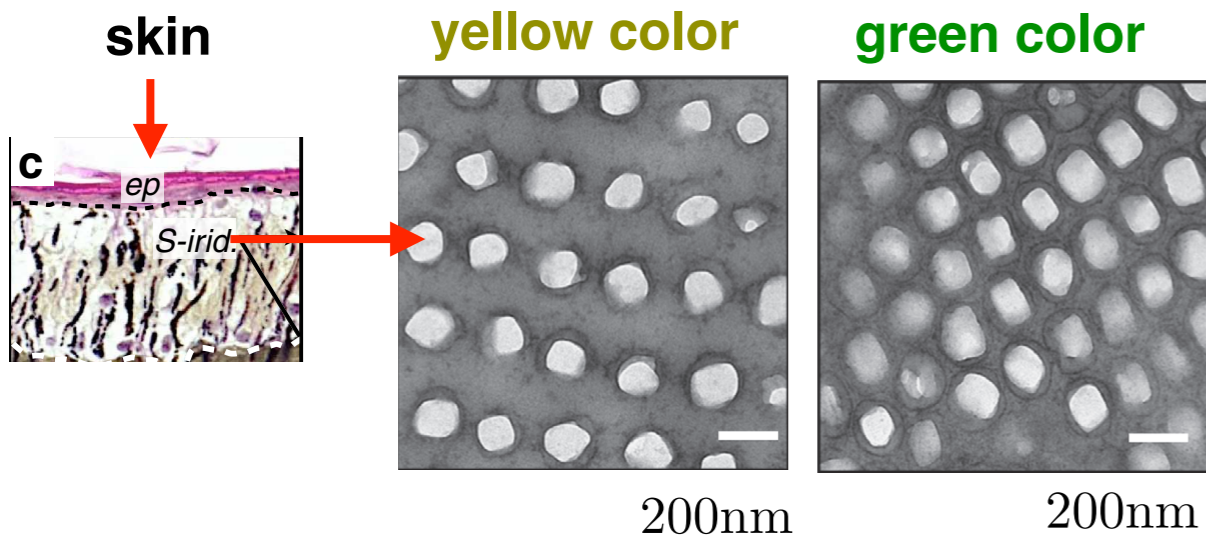
# Dynamic structural colors

## Chameleon (speed 8x)



J. Teyssier et al., Nat. Comm. 6, 6368 (2015)

**Changes in osmotic concentration lead to the swelling of cells in excited chameleon. This changes the spacing of periodic structure from which the ambient light is reflected.**

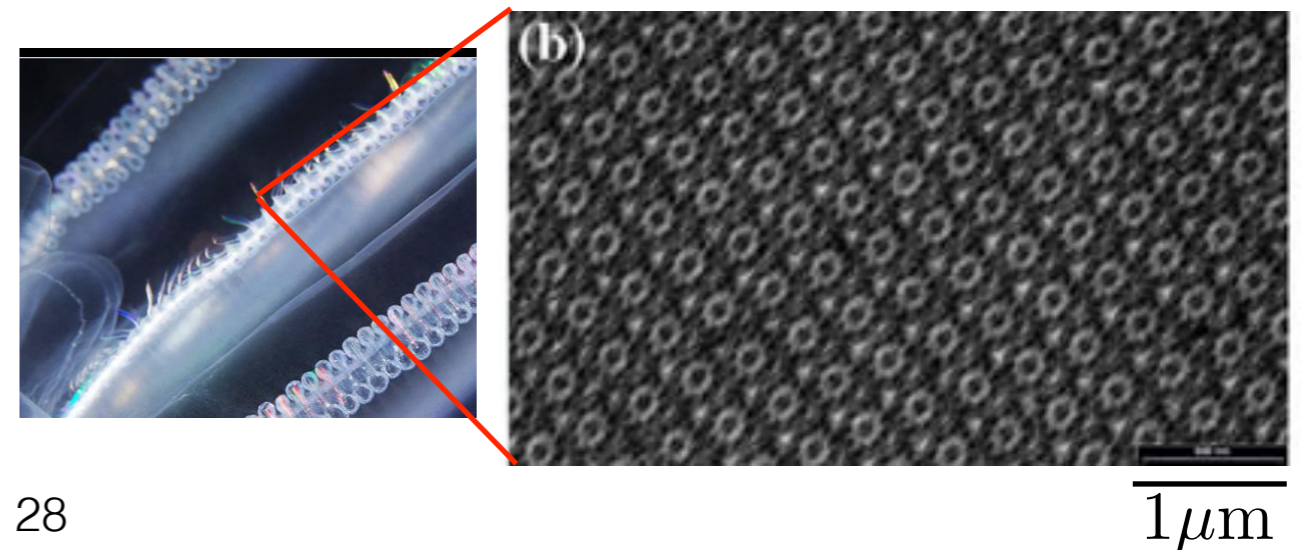


## Comb Jelly (real time)



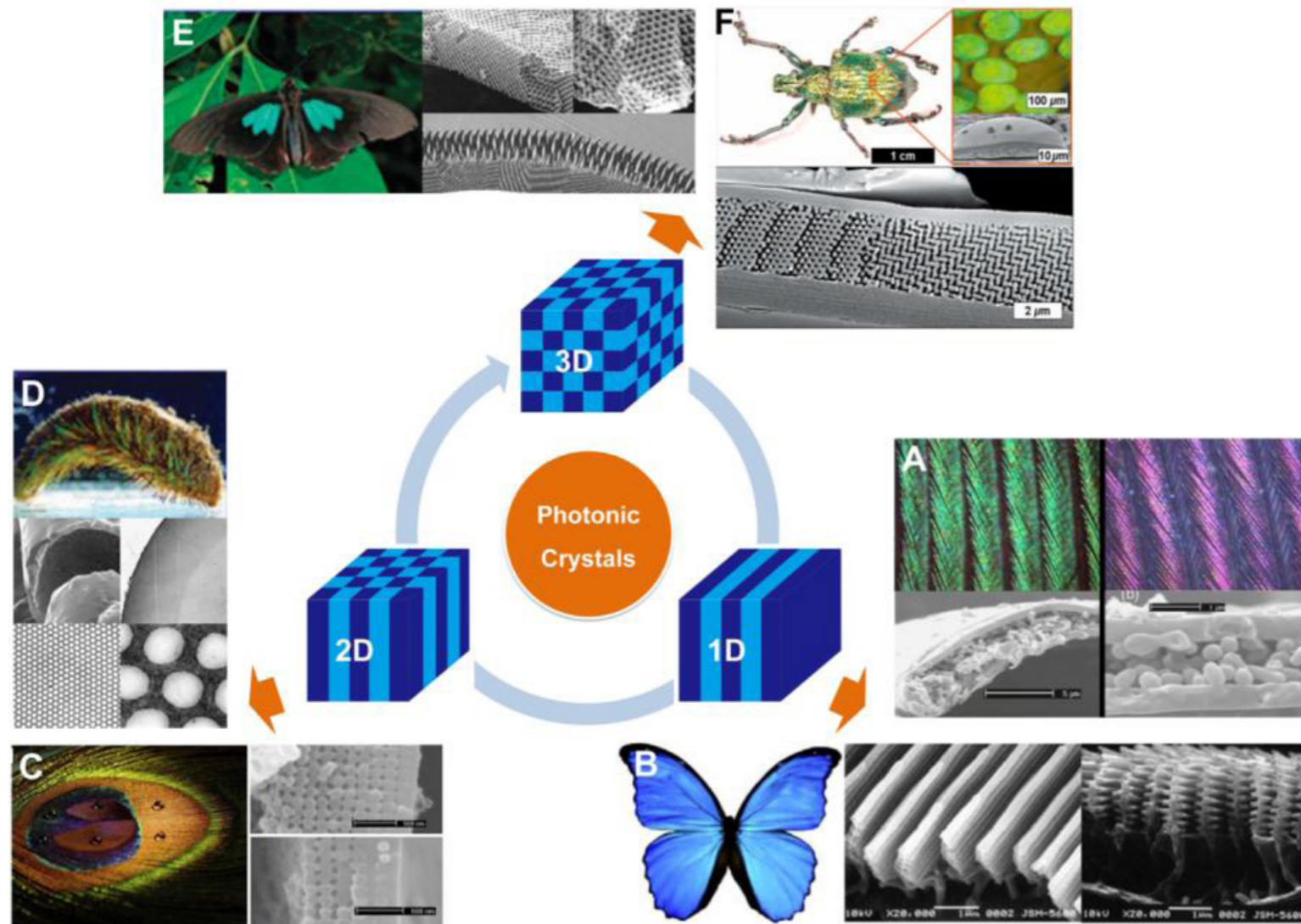
<https://www.youtube.com/watch?v=Qy90d0XvJIE>

**Rainbow color waves are produced by the beating of cilia, which change the orientation of periodic structure from which the ambient light is reflected.**

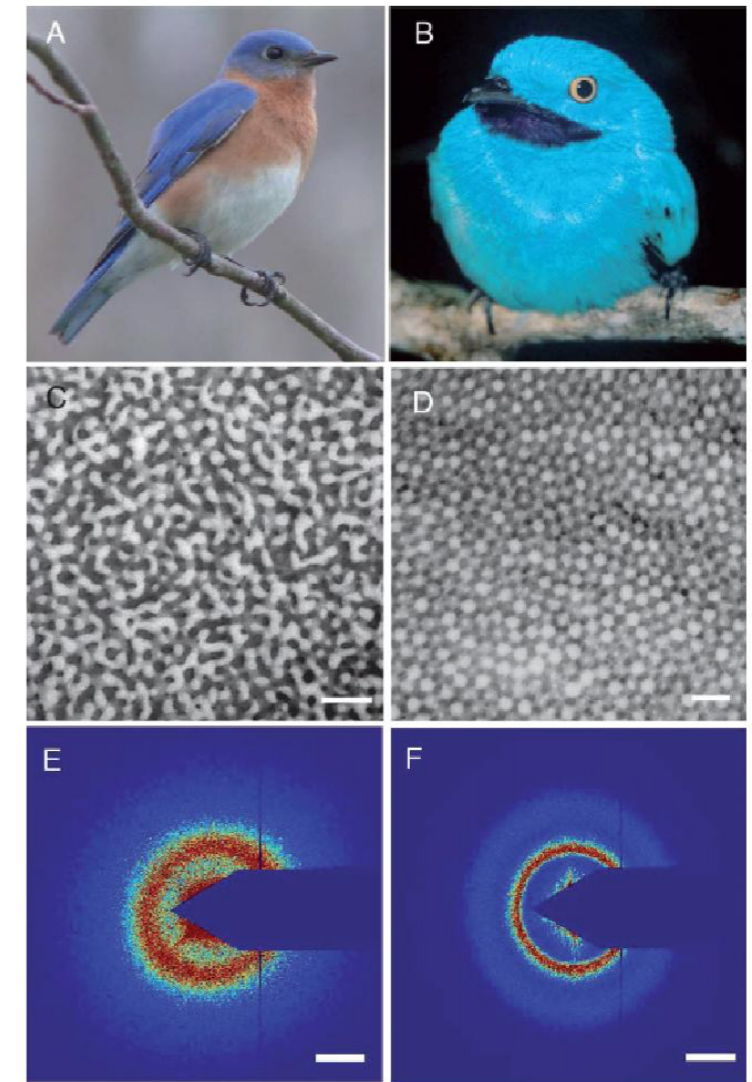


# Structural colors

Structural colors of animals and plants appear due to the selective reflection of ambient light on structural features underneath the surface.



H. Wang and K-Q. Zhang,  
Sensors 13, 4192 (2013)



V. Saranathan et al.,  
J. R. Soc. Interface 9, 2563 (2012)

# Noise barriers around the Amsterdam airport



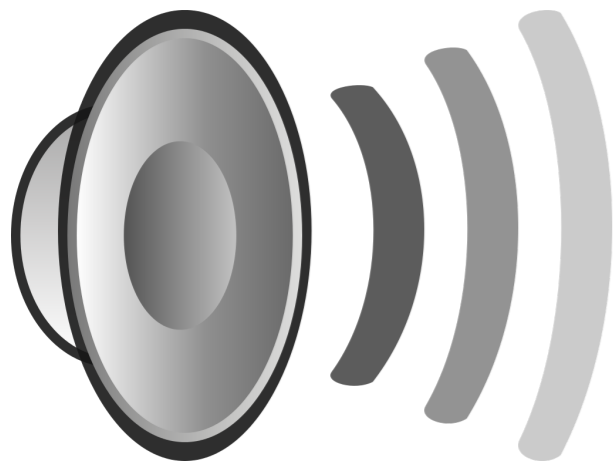
**Sound from airplanes that are landing and taking off is reflected from artificial barriers into the atmosphere.**

# Controllable sound filters

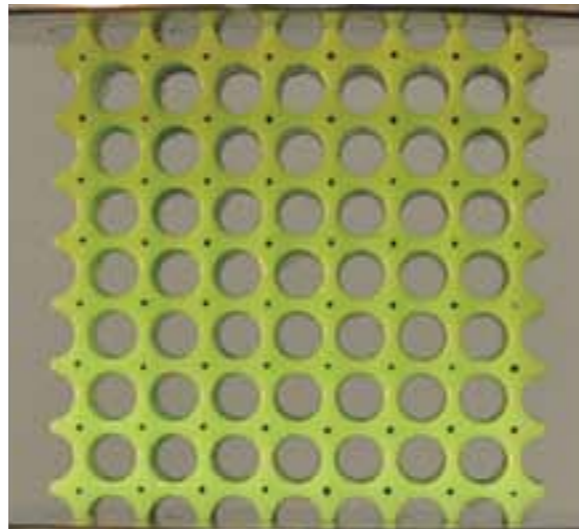
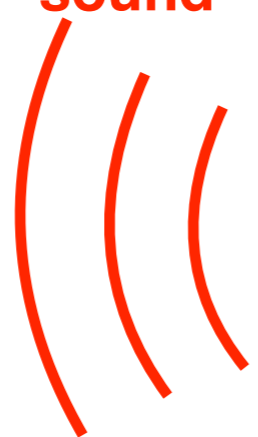
In periodic structures sound waves of certain frequencies (within a “band gap”) cannot propagate. The range of “band gap” frequencies depends on material properties, the geometry of structure and the external load.

## undeformed structure

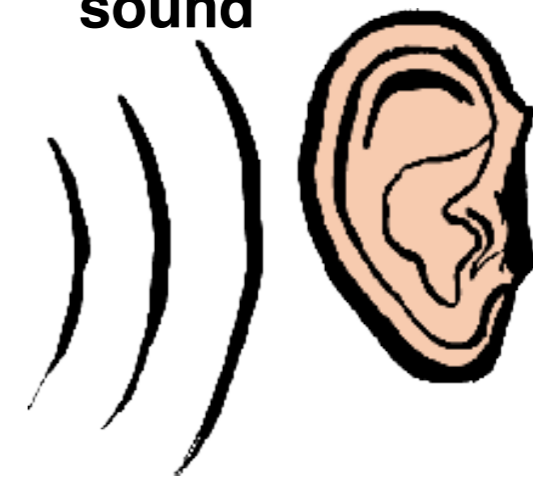
incoming sound



reflected sound

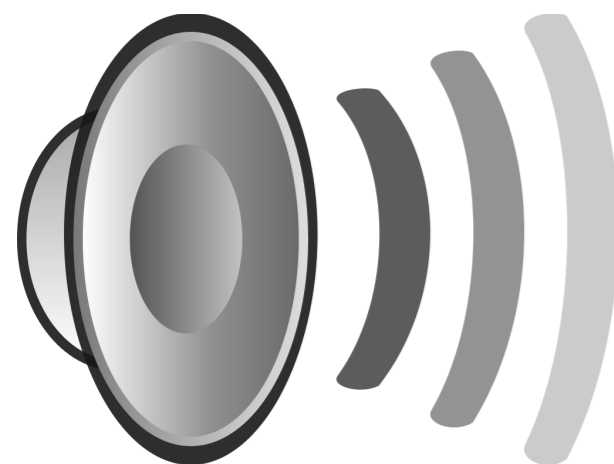


transmitted sound

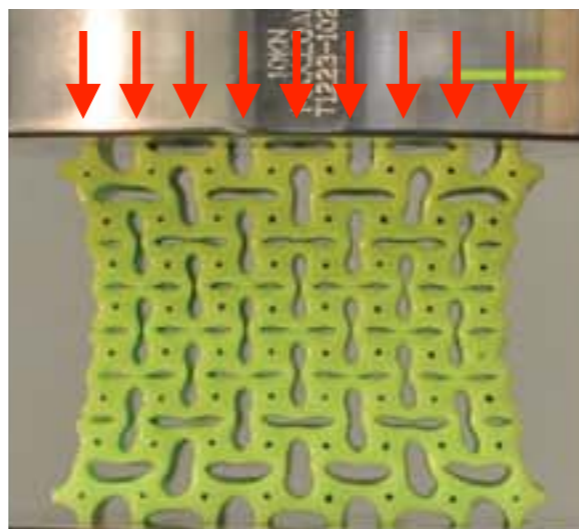


## deformed structure

incoming sound

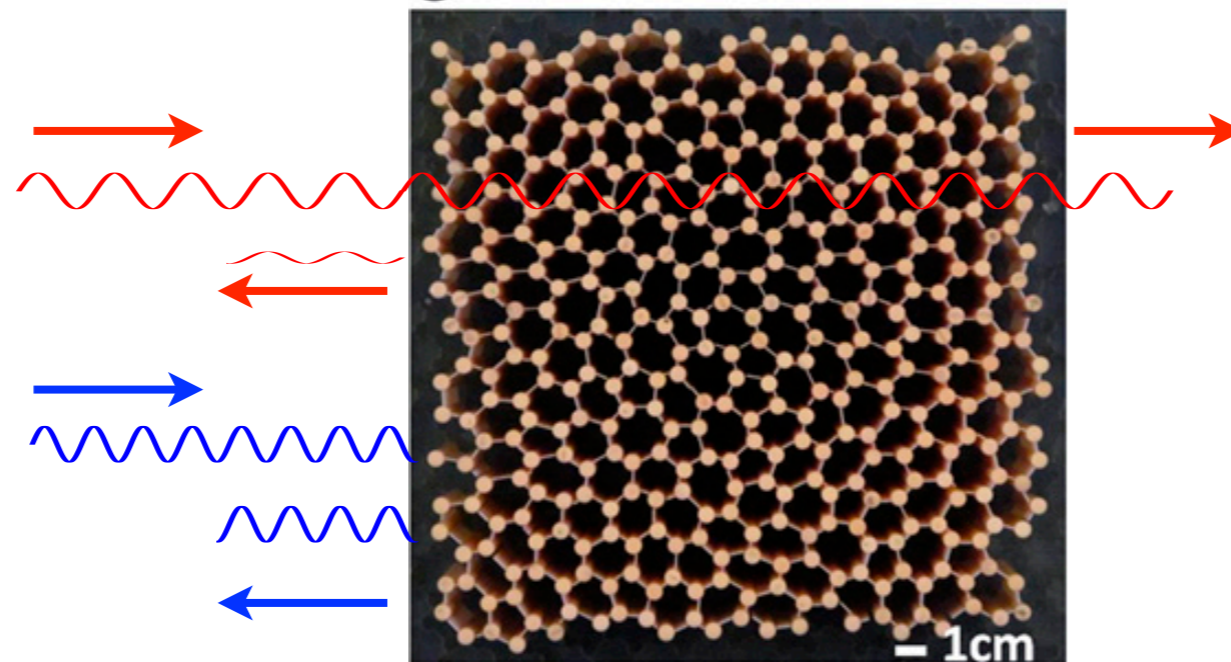


reflected sound



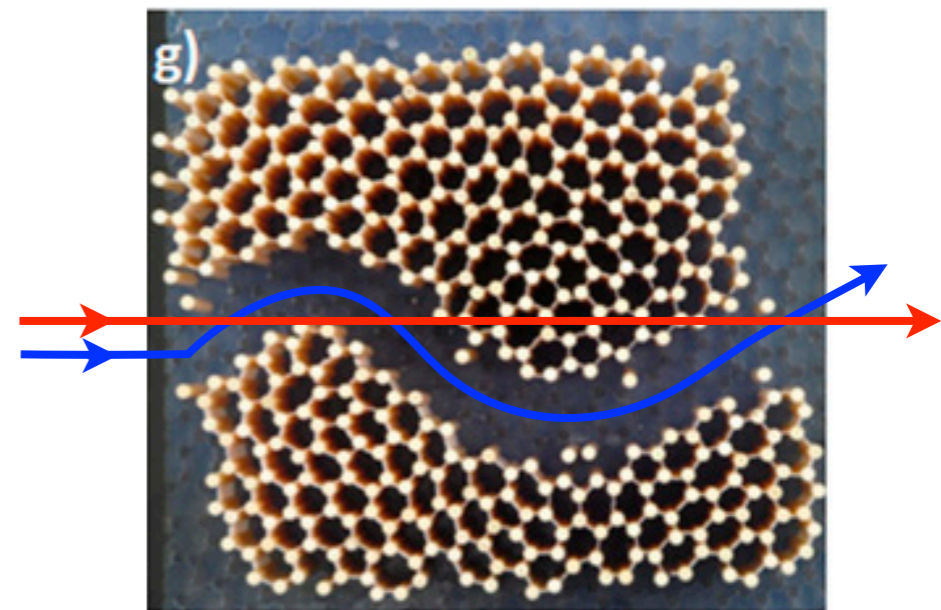
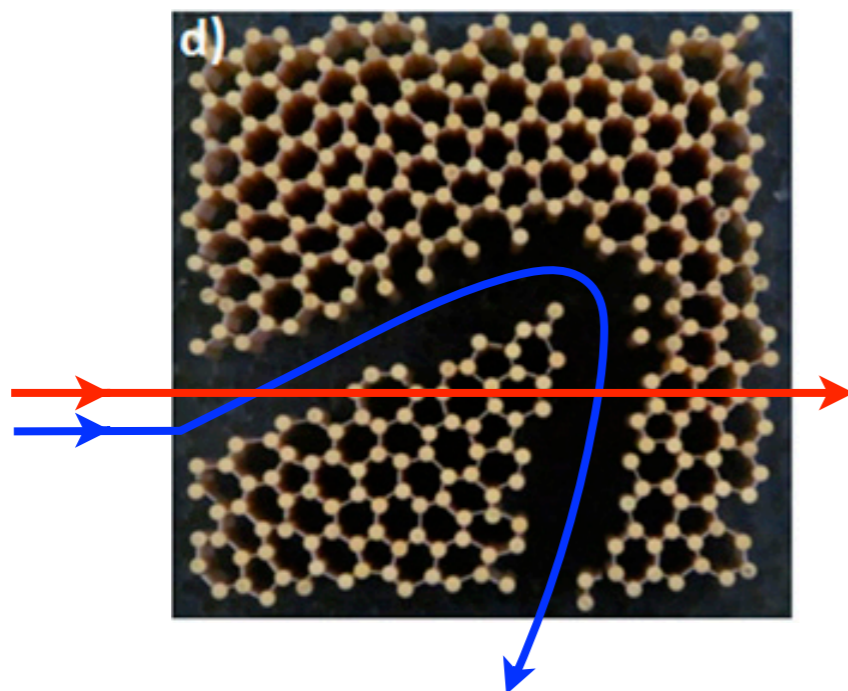
P. Wang, J. Shim and K. Bertoldi,  
PRB **88**, 014304 (2013)

# Waveguides in disordered structures



**Channels inside structures can be used as guides for waves with wavelengths that are totally reflected from a complete structure!**

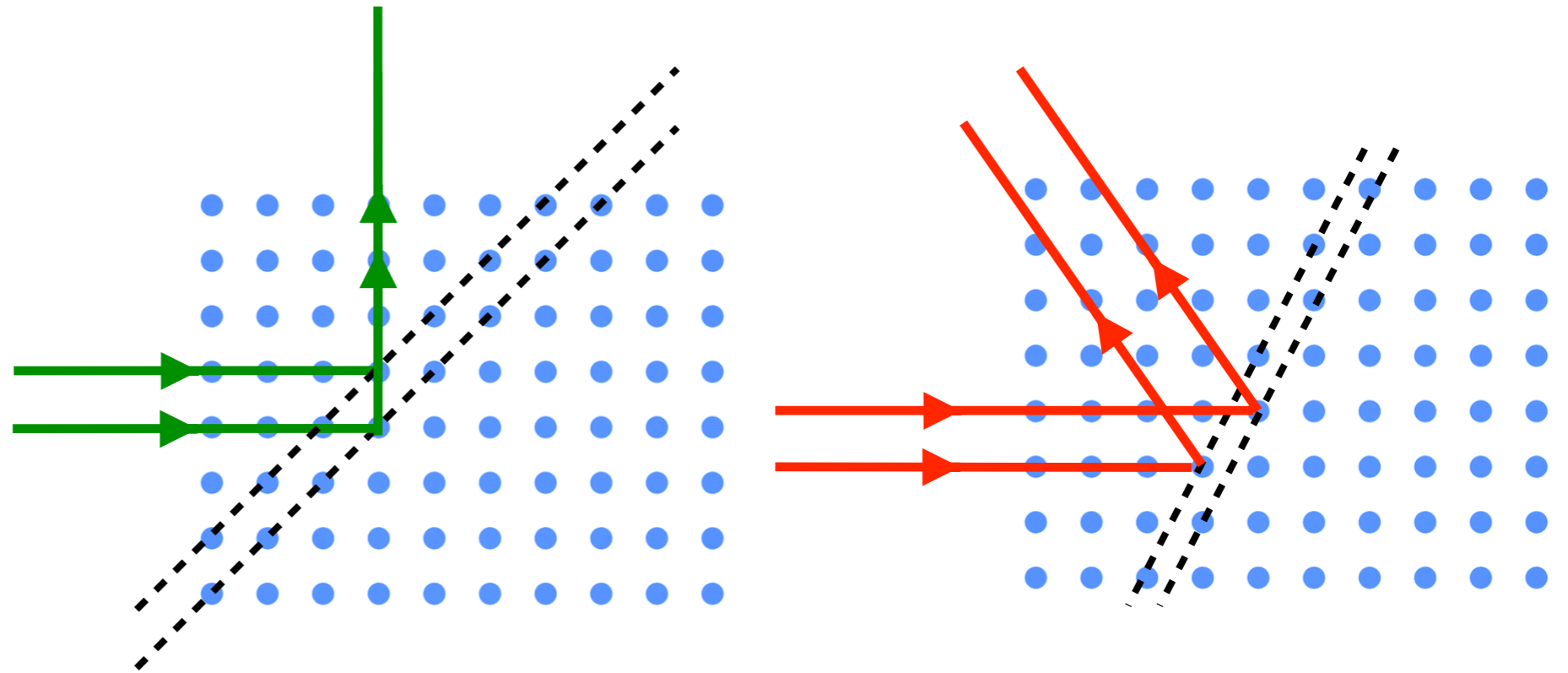
**Note: channels can have arbitrary bends!**



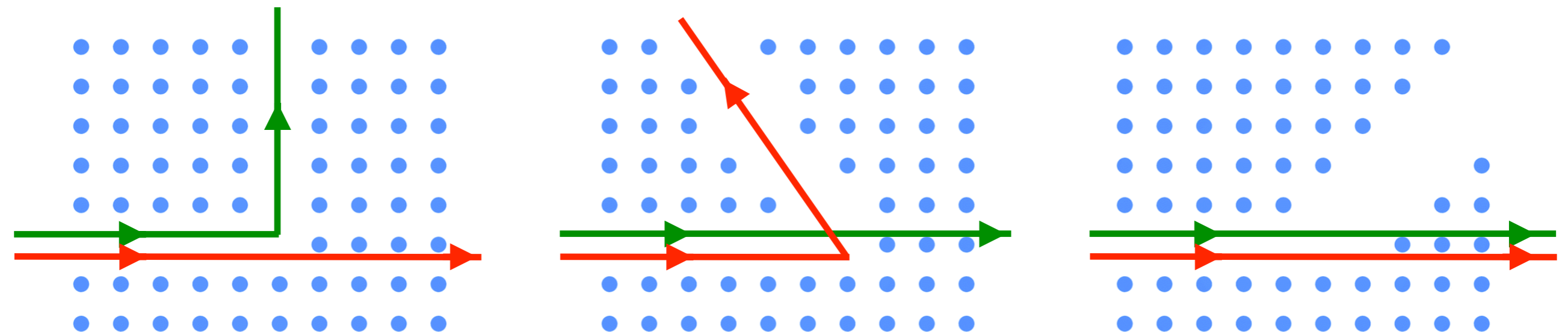


# Waveguides in periodic structures

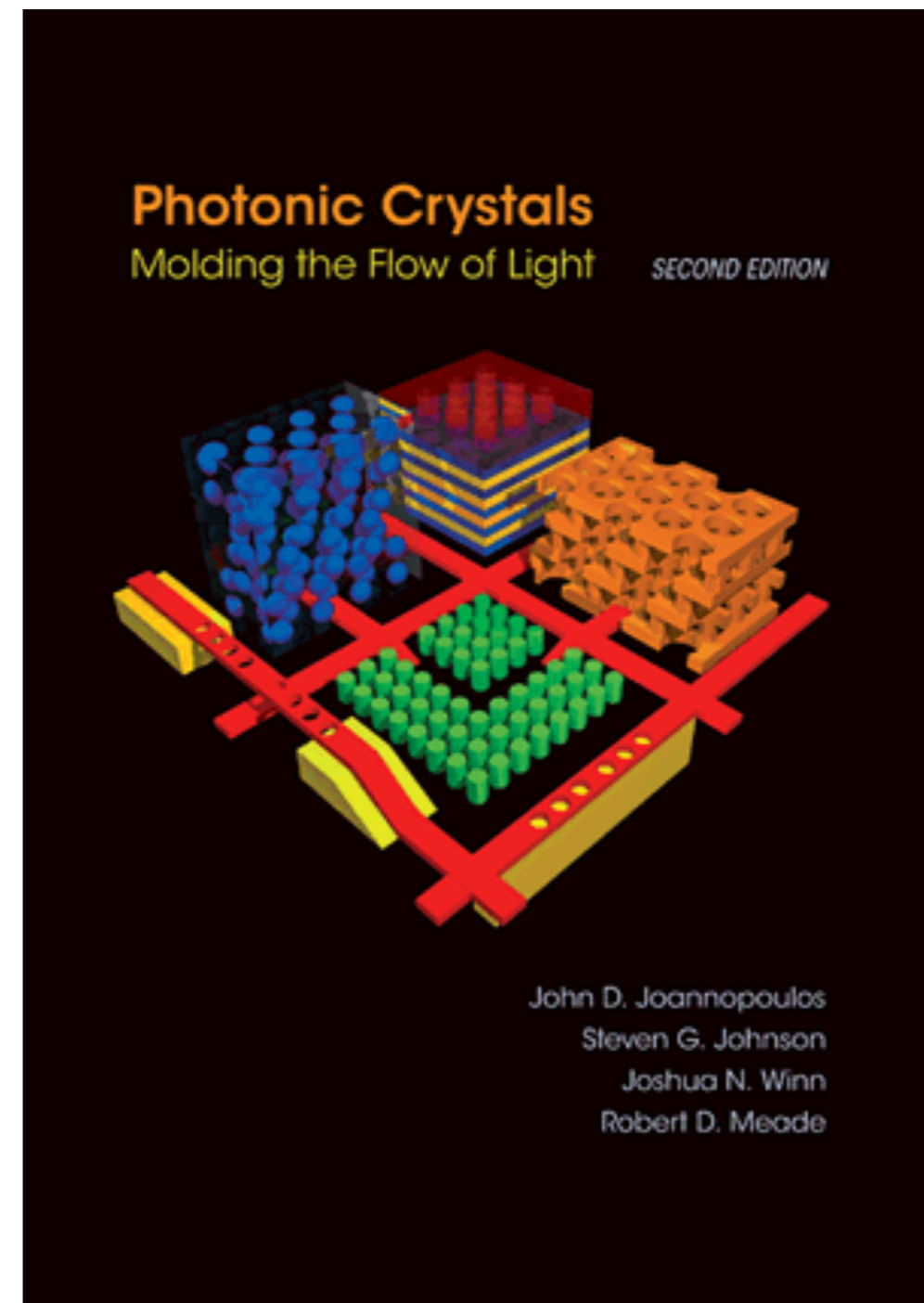
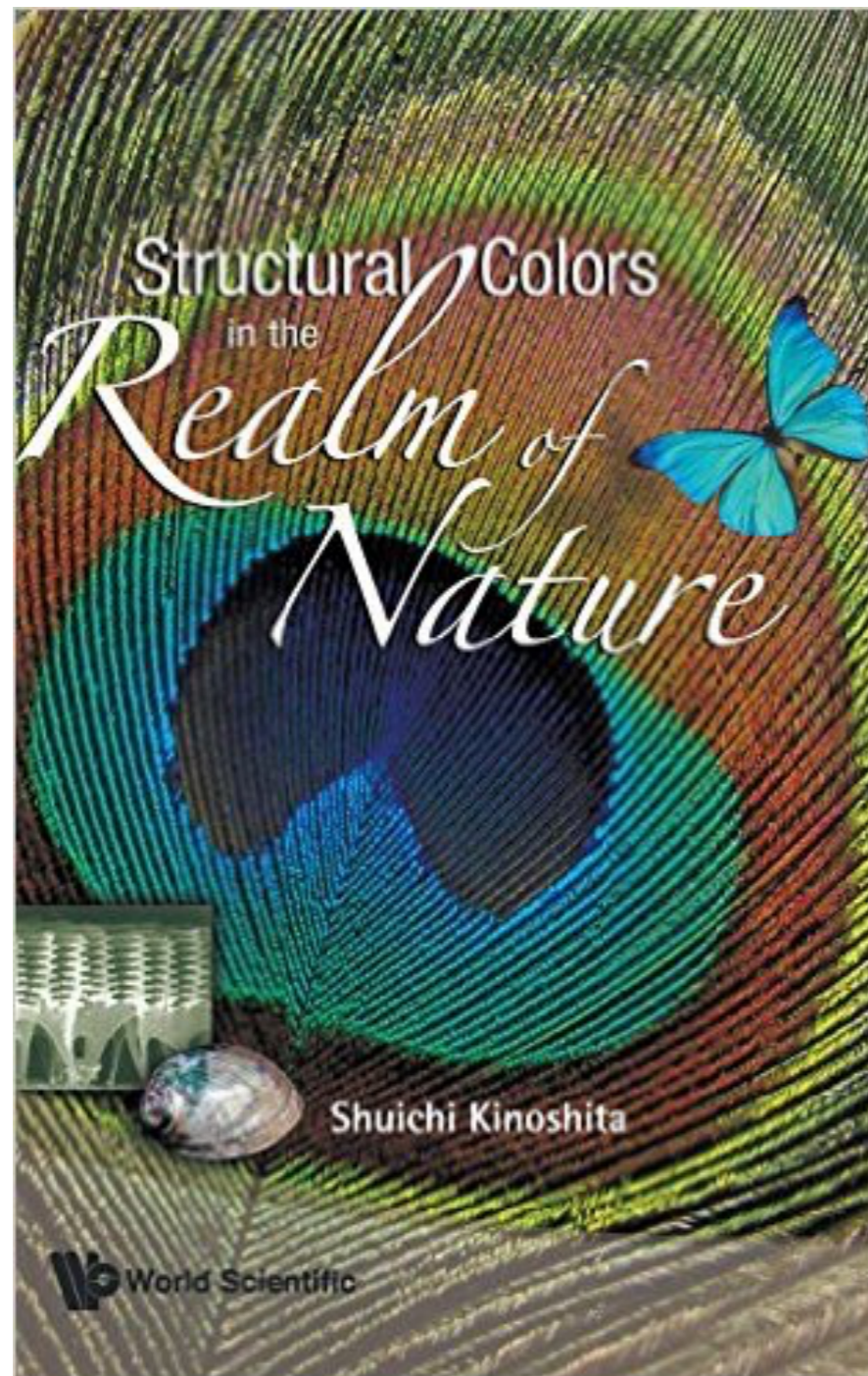
In periodic structures waves are completely reflected only at certain angles.



**Note: channels with certain bends act as waveguides only for those waves that are completely reflected at these angles!**



# Further reading about structural colors and photonic crystals



<http://ab-initio.mit.edu/book/>