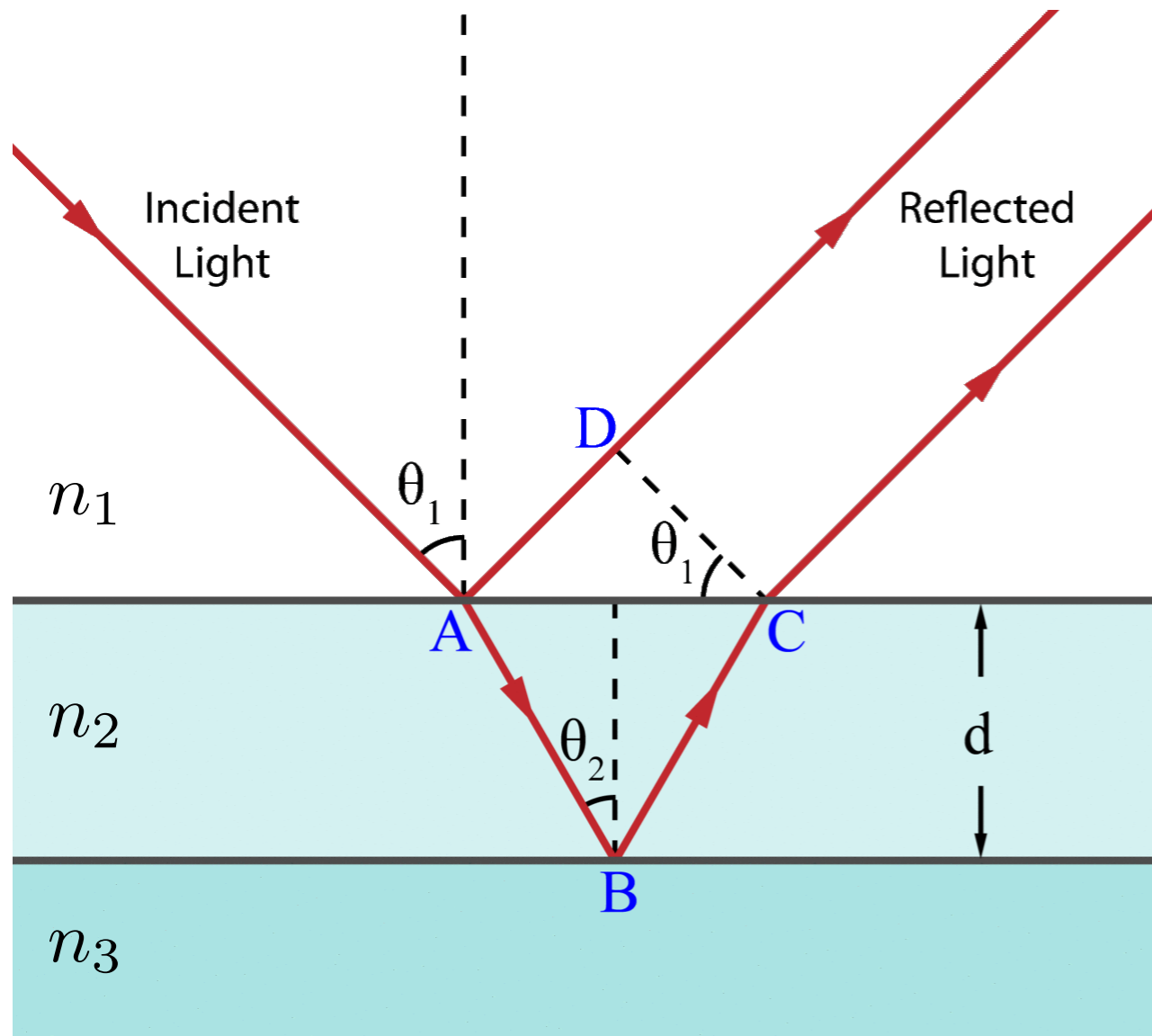


Structural Color and Wrinkled Surfaces



Interference on thin films



difference between optical path lengths of the two reflected rays

$$OPD = n_2 (\overline{AB} + \overline{BC}) - n_1 \overline{AD}$$

$$OPD = 2n_2 d \cos(\theta_2)$$

$$n_1 < n_2 < n_3 \quad n_1 > n_2 > n_3$$

no additional phase

difference due to reflections

constructive interference of reflected rays
destructive interference of reflected rays

$$OPD = m\lambda$$

$$OPD = \left(m + \frac{1}{2}\right) \lambda$$

$$m = 0, \pm 1, \pm 2, \dots$$

$$n_1 > n_2 < n_3 \quad n_1 < n_2 > n_3$$

additional π phase

difference due to reflections

constructive interference of reflected rays
destructive interference of reflected rays

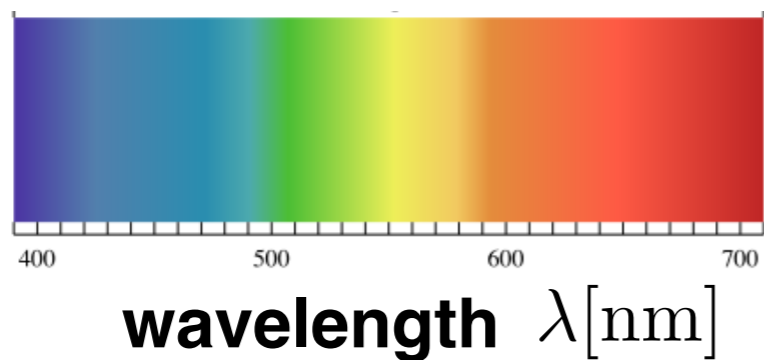
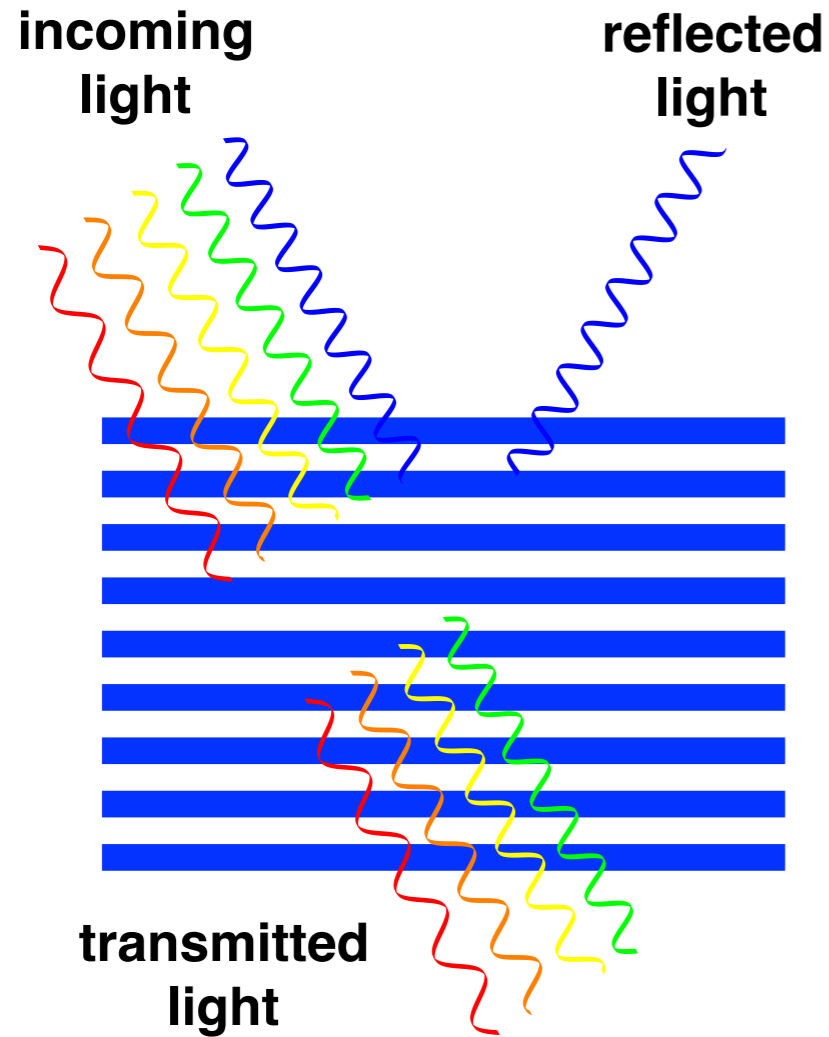
$$OPD = \left(m + \frac{1}{2}\right) \lambda$$

constructive interference of reflected rays
destructive interference of reflected rays

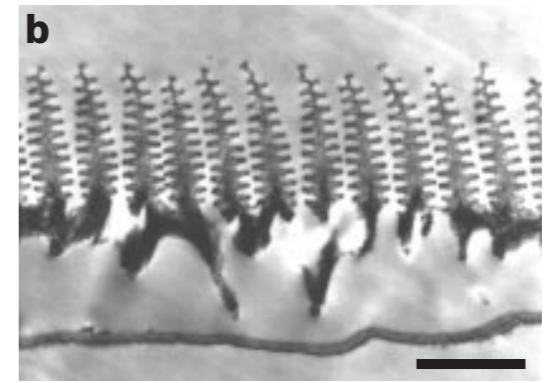
$$OPD = m\lambda$$

Structural colors on periodic structures

Single reflected color on structures with uniform spacing

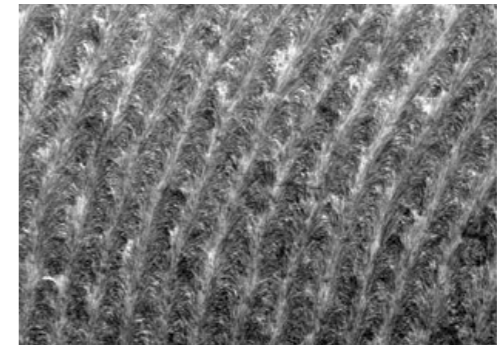


Morpho butterfly



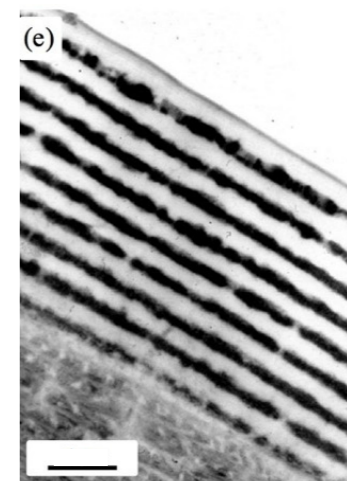
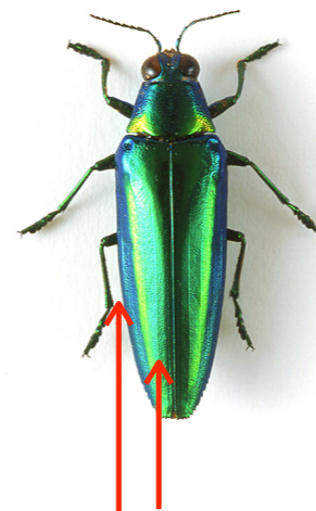
1.7 μm

Marble berry



250nm

Chrysochroa raja beetle

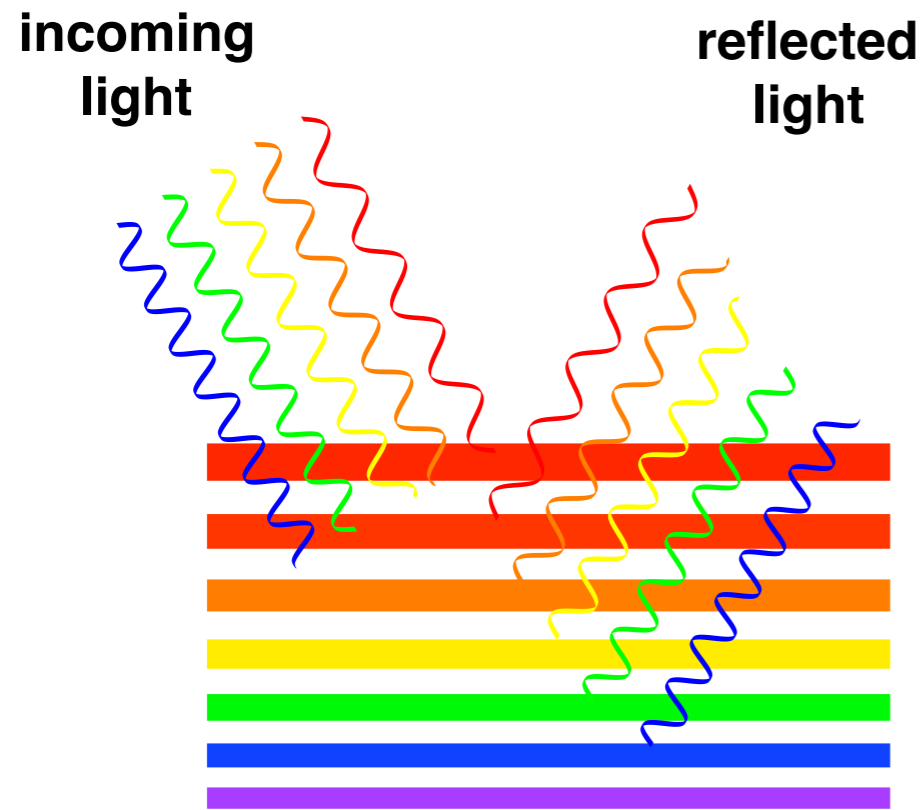


1 μm

reflected color depends on the viewing angle!

Silver and gold structural colors

Many colors reflected on structures with varying spacing

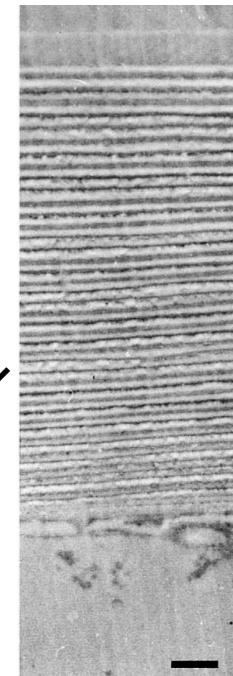


chirped structure

Chrysina limbata beetle



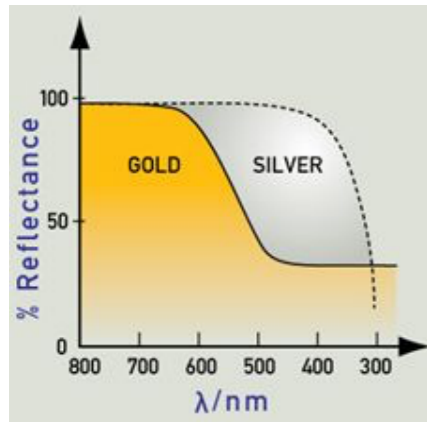
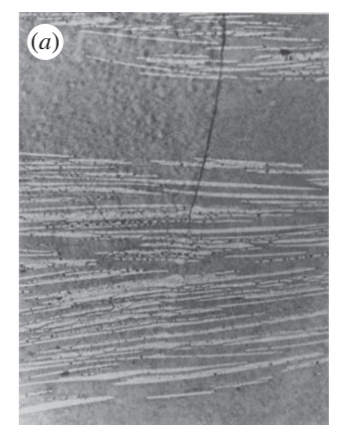
Chrysina aurigans beetle



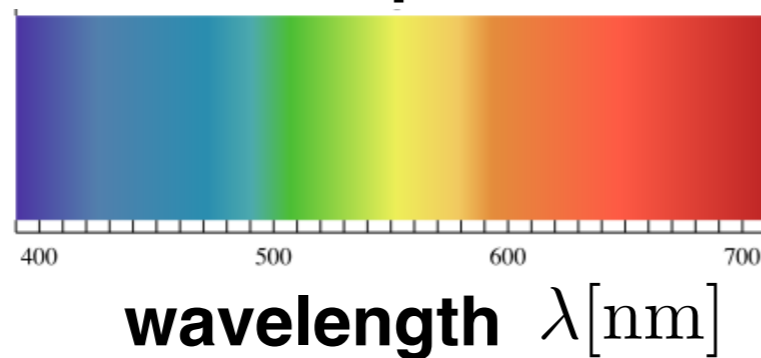
thicker
↓
thinner

disordered layer spacing

bleak fish

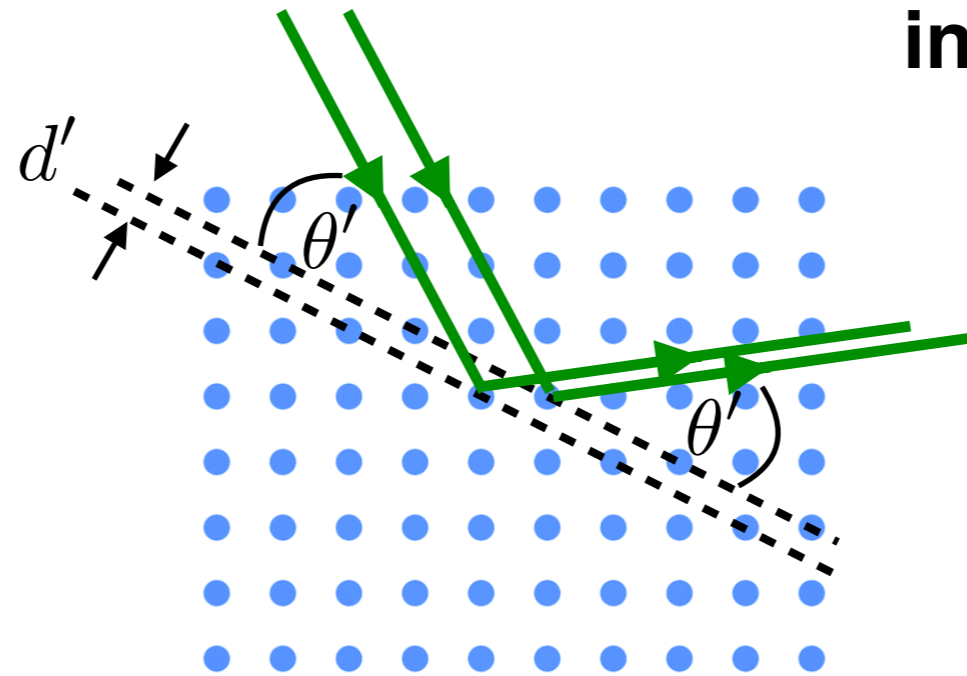
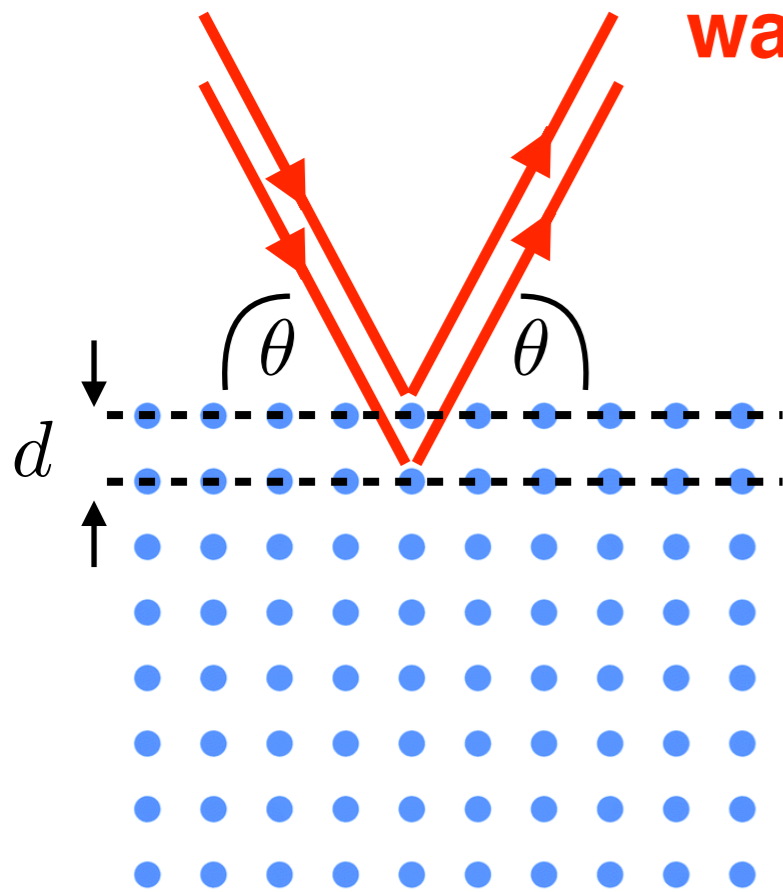


visible spectrum



Bragg scattering on crystal layers

Constructive interference for waves with different wavelengths occurs in different crystal planes!



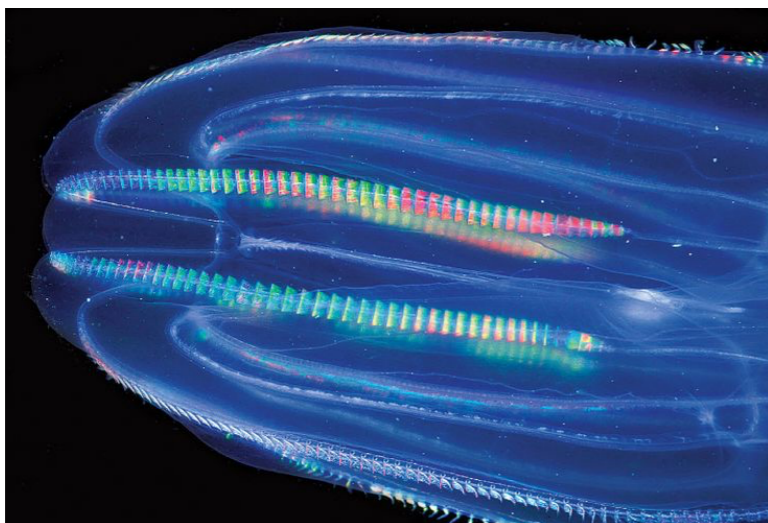
**constructive
interference condition**

$$2d \sin \theta = m\lambda$$

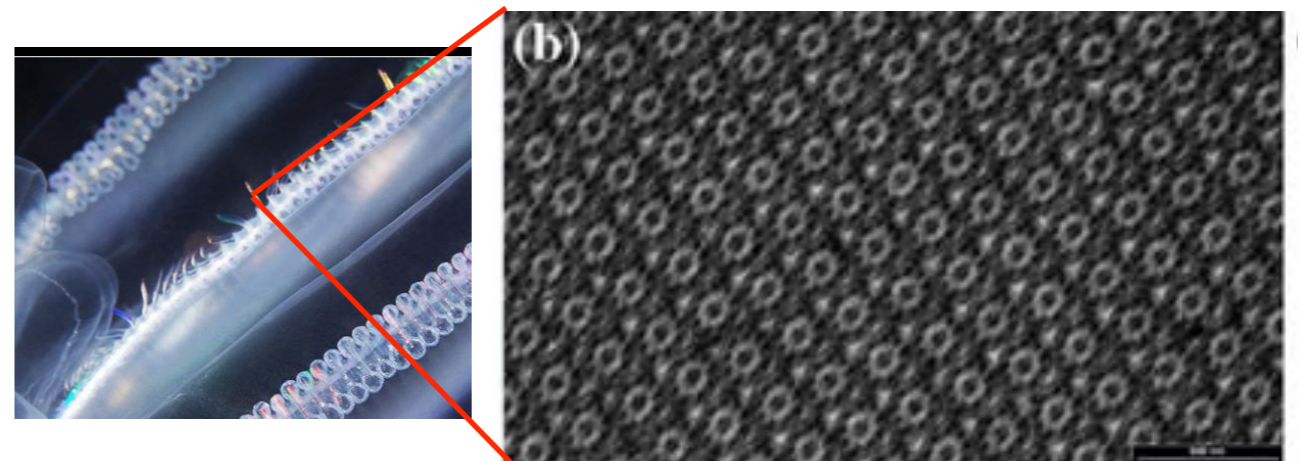
$$2d' \sin \theta' = m\lambda'$$

$$m = 0, \pm 1, \pm 2, \dots$$

Comb jelly



Beating cilia are changing crystal orientation

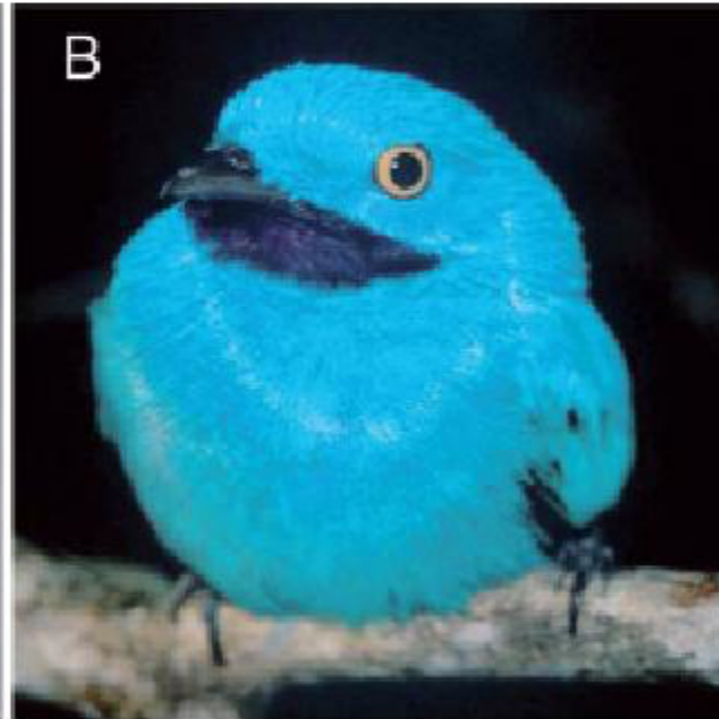


Scattering on disordered structures

Eastern
bluebird



Plum-throated
Cotinga

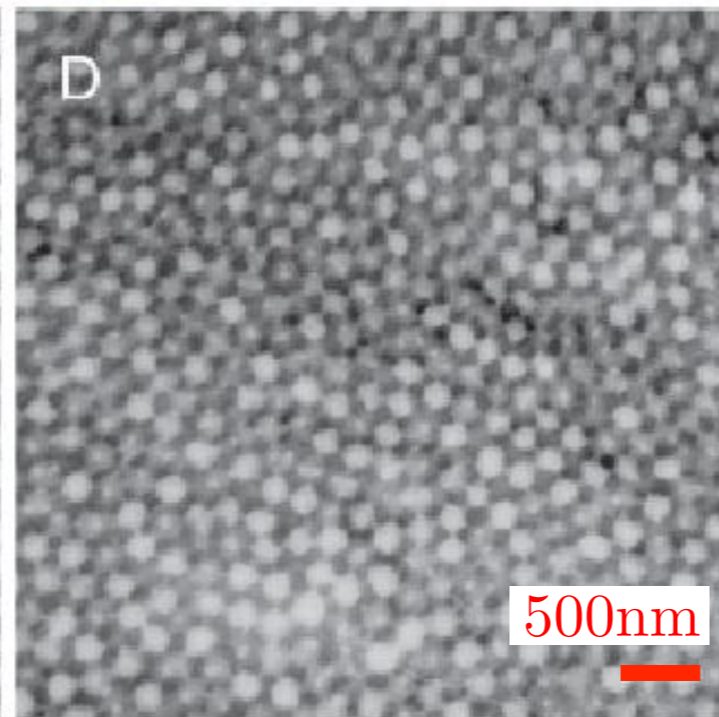
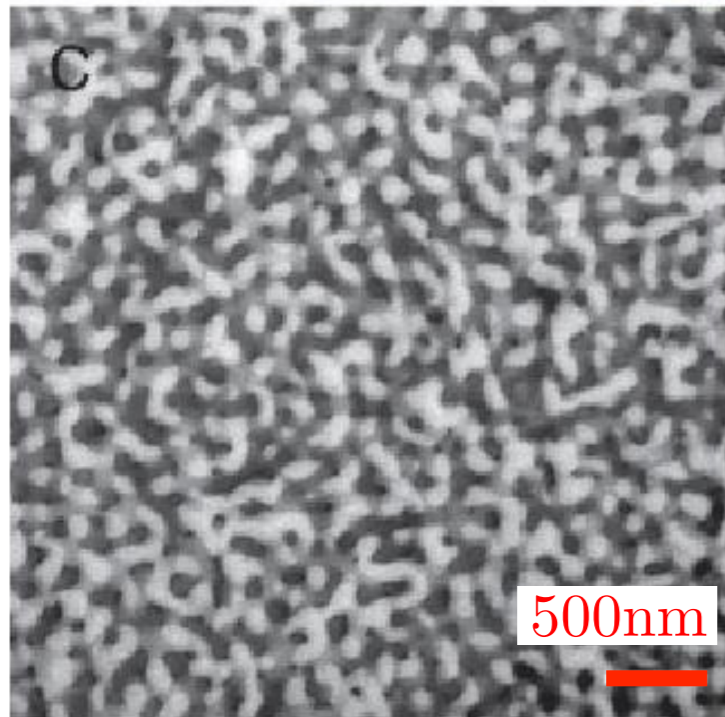


Disordered structures with a characteristic length scale.

This length scale determines what light wavelengths are preferentially scattered.

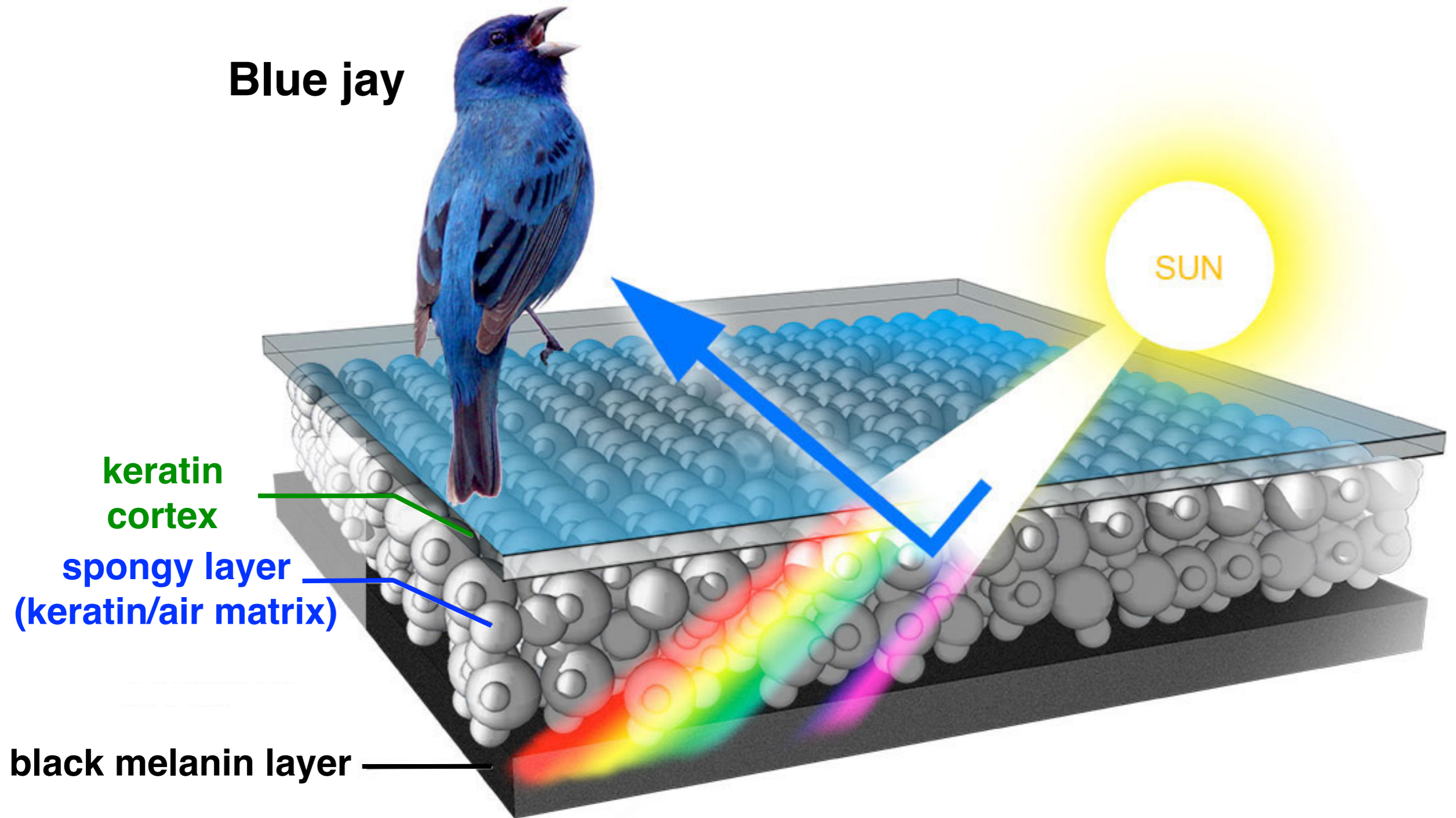
The selectively reflected wavelengths are the same in all directions!

This gives rise to blue colors in these birds.



Scattering on disordered structures

Blue jay



<https://academy.allaboutbirds.org/how-birds-make-colorful-feathers/>

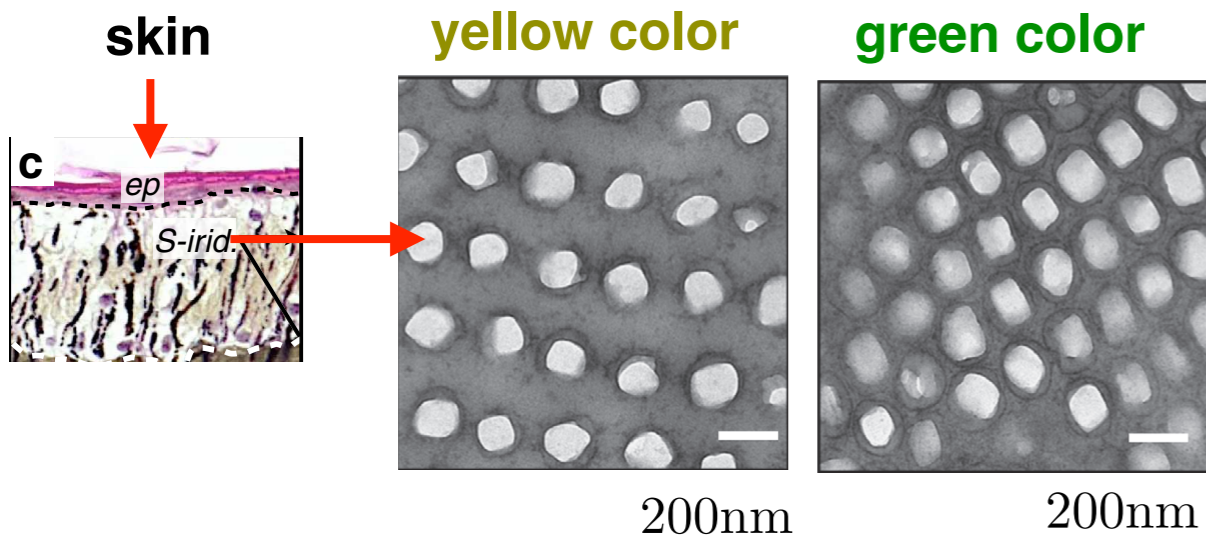
Dynamic structural colors

Chameleon (speed 8x)



J. Teyssier et al., Nat. Comm. 6, 6368 (2015)

Changes in osmotic concentration lead to the swelling of cells in excited chameleon. This changes the spacing of periodic structure from which the ambient light is reflected.

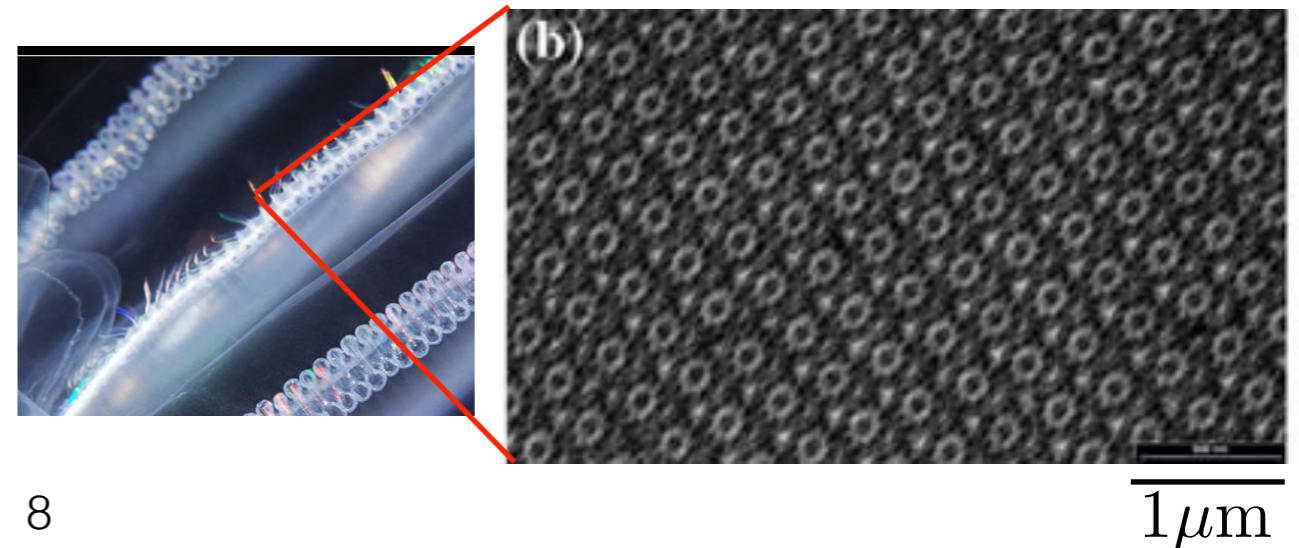


Comb Jelly (real time)



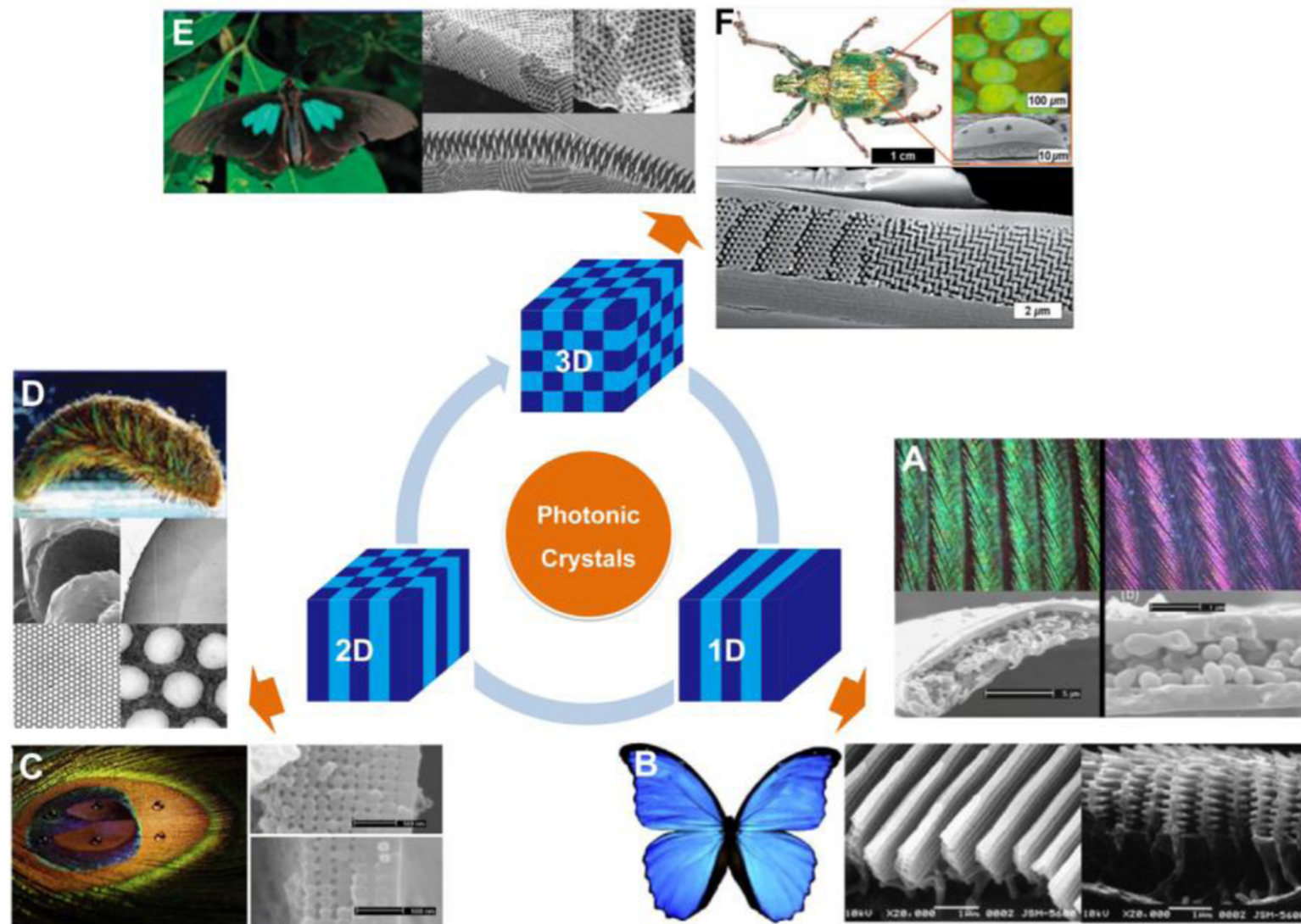
<https://www.youtube.com/watch?v=Qy90d0XvJIE>

Rainbow color waves are produced by the beating of cilia, which change the orientation of periodic structure from which the ambient light is reflected.

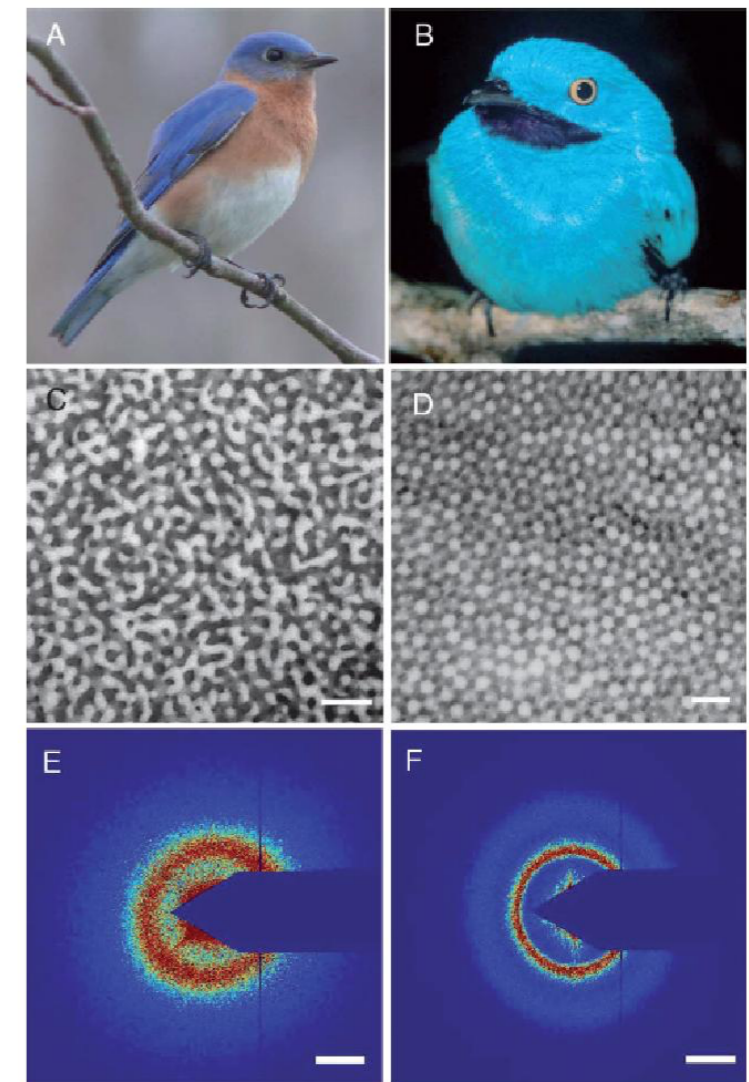


Structural colors

Structural colors of animals and plants appear due to the selective reflection of ambient light on structural features underneath the surface.



H. Wang and K-Q. Zhang,
Sensors 13, 4192 (2013)



V. Saranathan et al.,
J. R. Soc. Interface 9, 2563 (2012)

Noise barriers around the Amsterdam airport



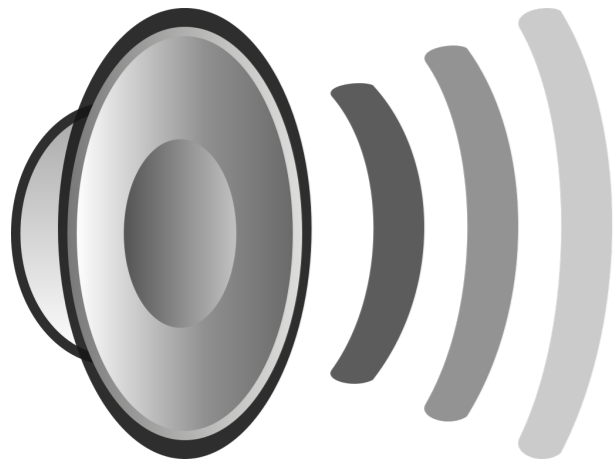
Sound from airplanes that are landing and taking off is reflected from artificial barriers into the atmosphere.

Controllable sound filters

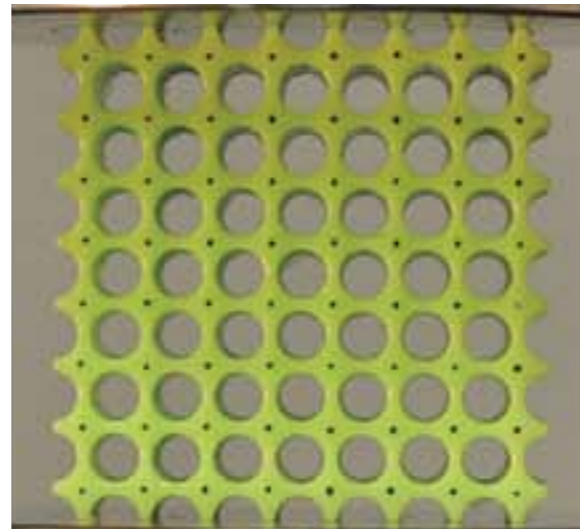
In periodic structures sound waves of certain frequencies (within a “band gap”) cannot propagate. The range of “band gap” frequencies depends on material properties, the geometry of structure and the external load.

undeformed structure

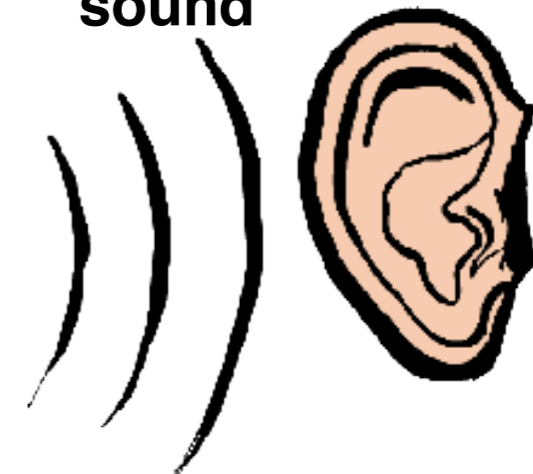
incoming sound



reflected sound

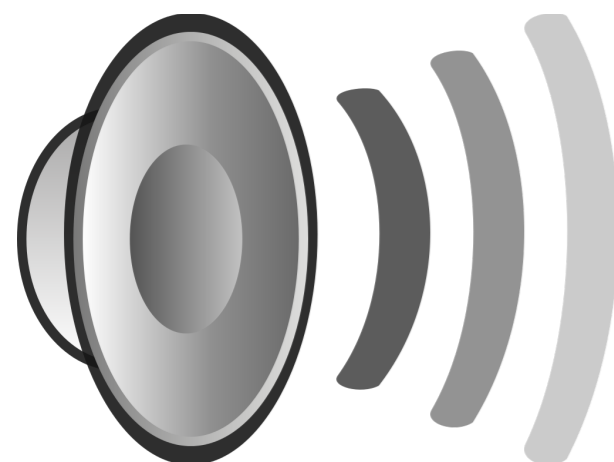


transmitted sound

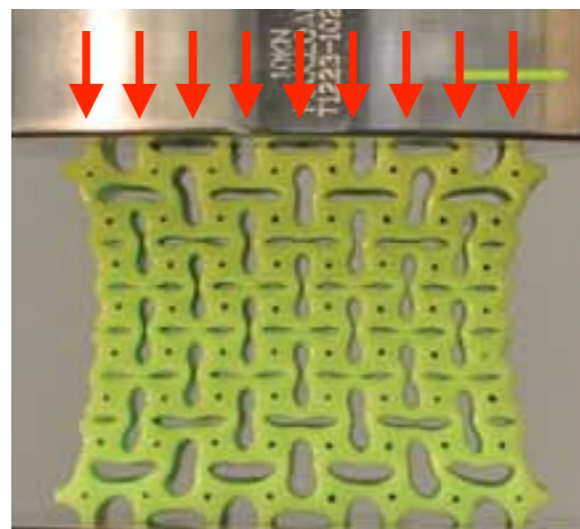


deformed structure

incoming sound

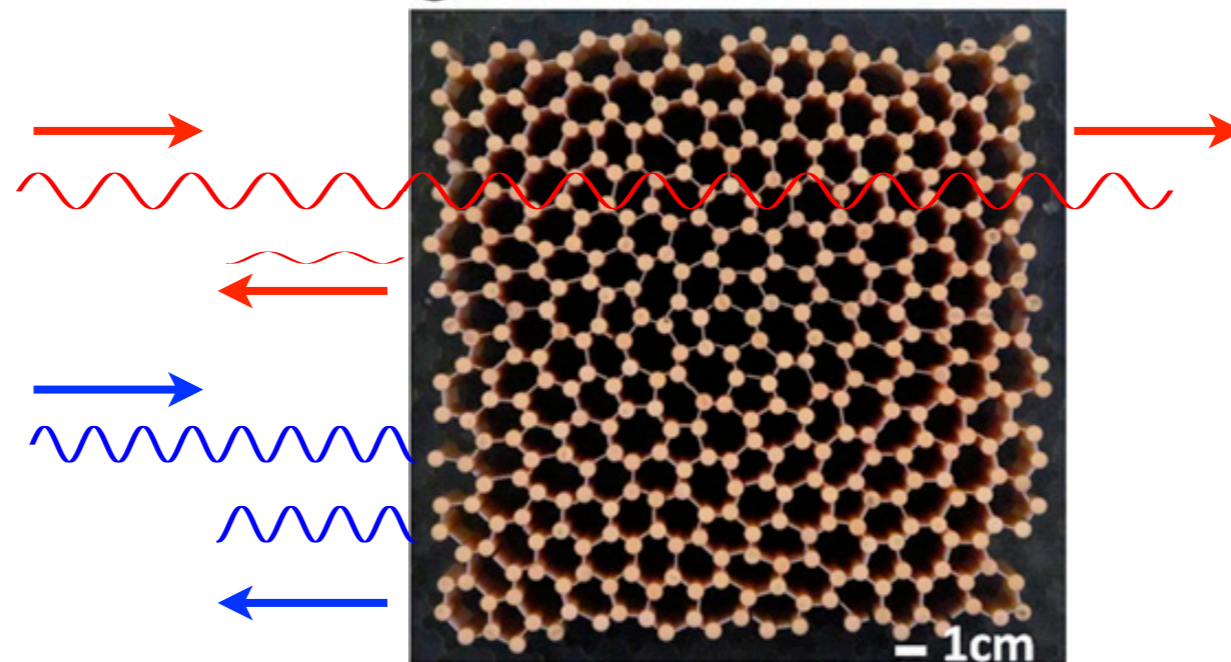


reflected sound



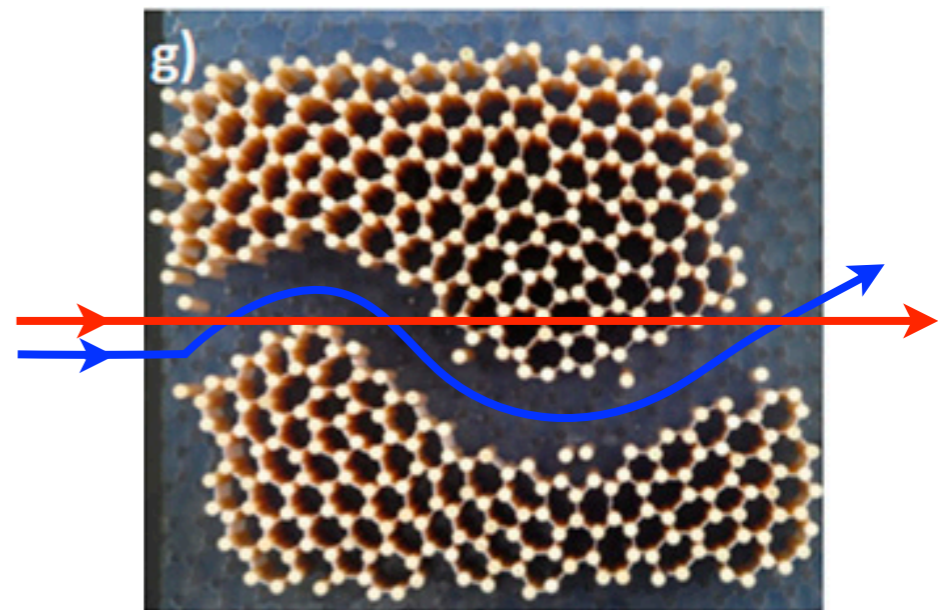
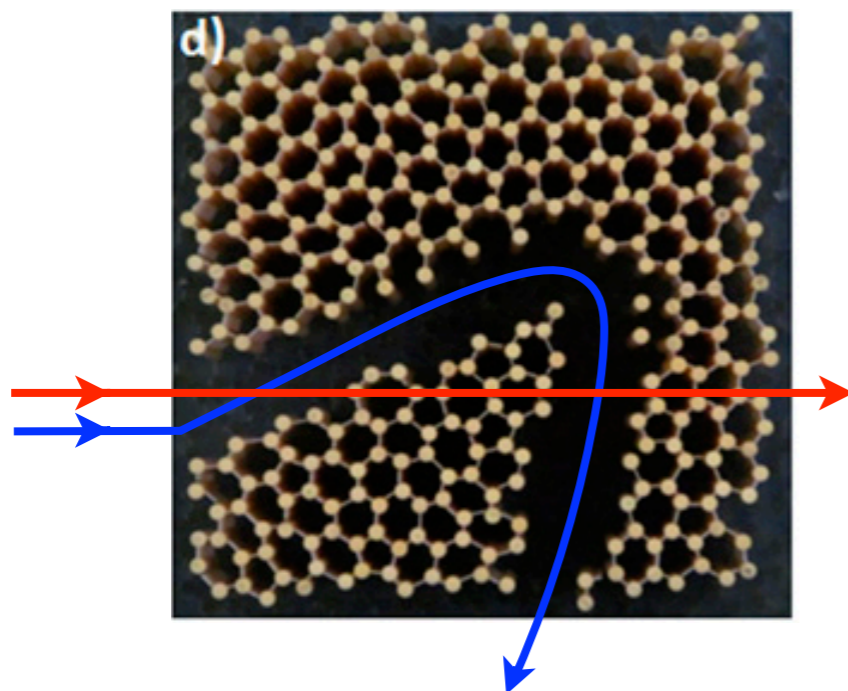
P. Wang, J. Shim and K. Bertoldi,
PRB **88**, 014304 (2013)

Waveguides in disordered structures



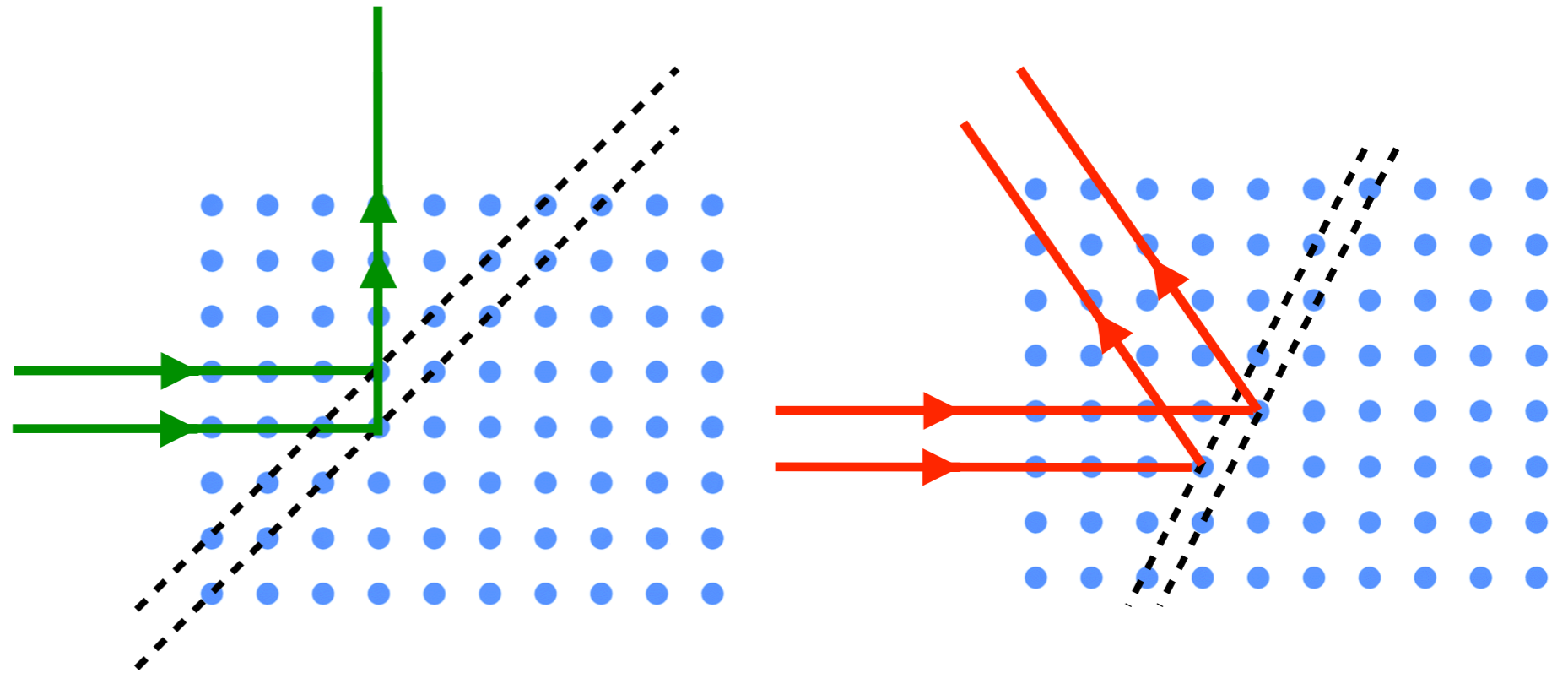
Channels inside structures can be used as guides for waves with wavelengths that are totally reflected from a complete structure!

Note: channels can have arbitrary bends!

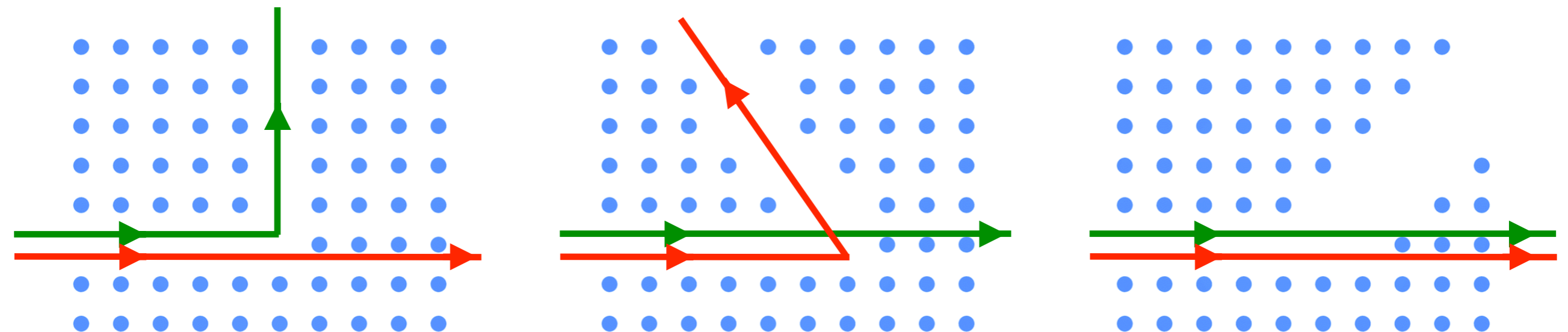


Waveguides in periodic structures

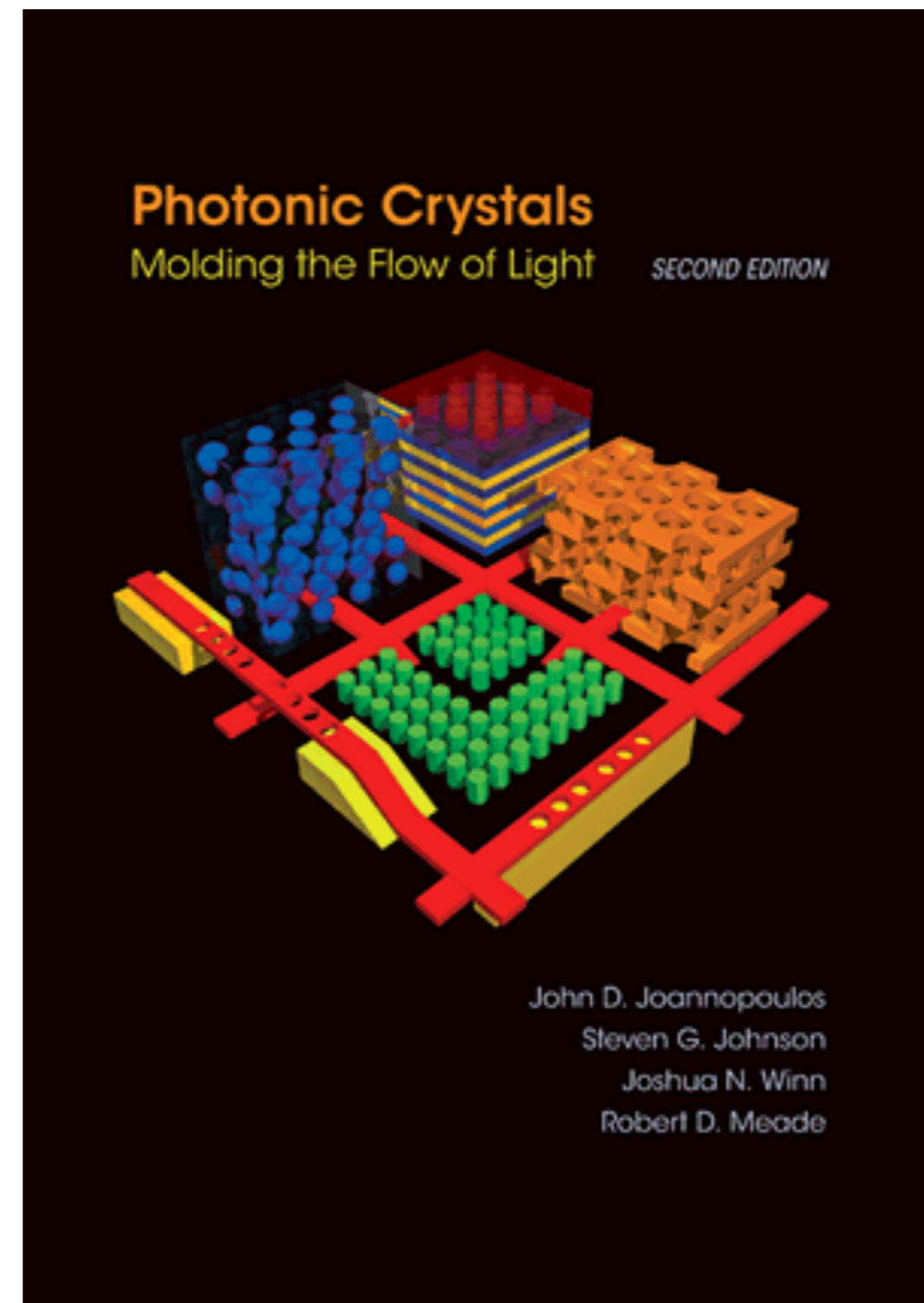
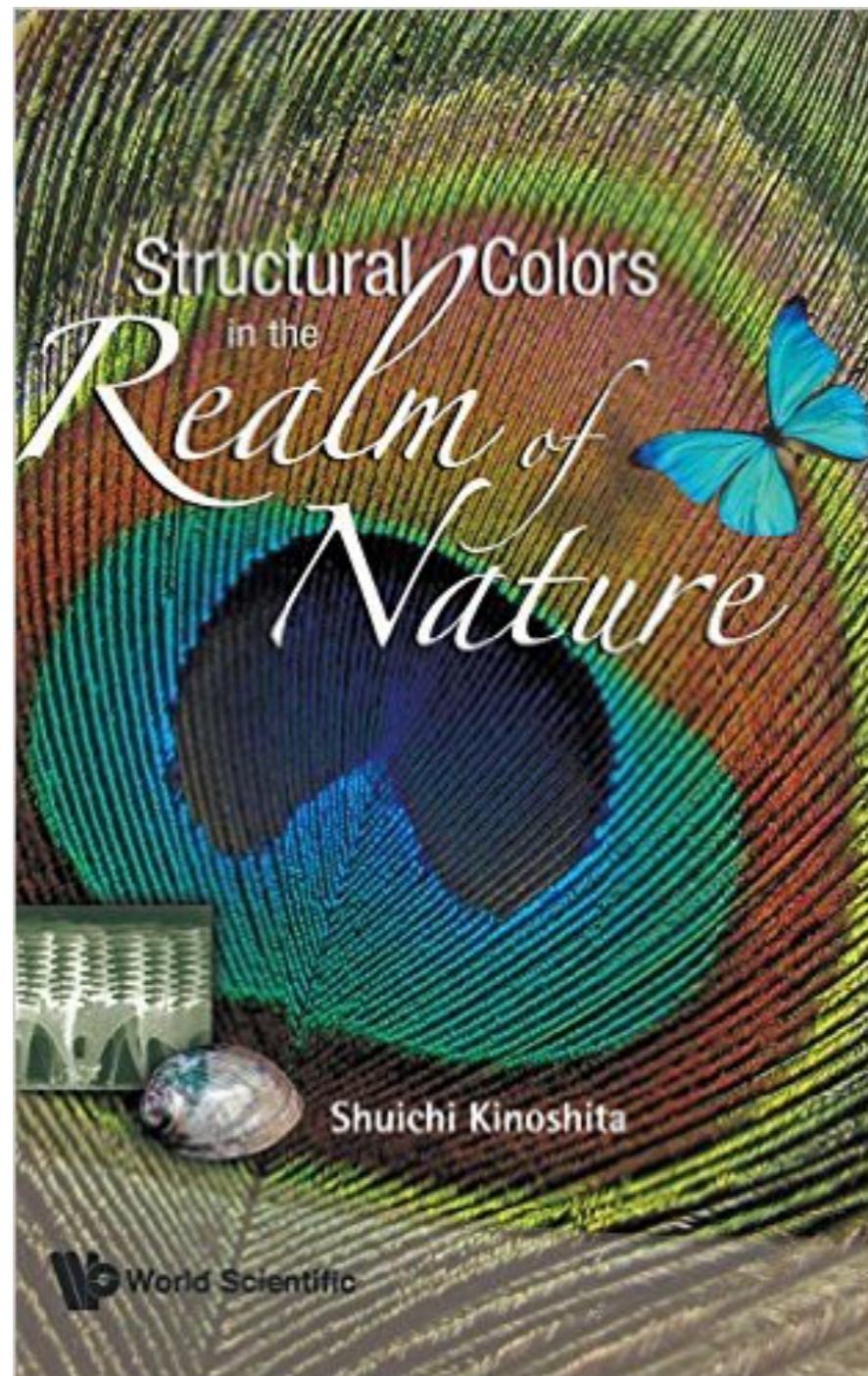
In periodic structures waves are completely reflected only at certain angles.



Note: channels with certain bends act as waveguides only for those waves that are completely reflected at these angles!

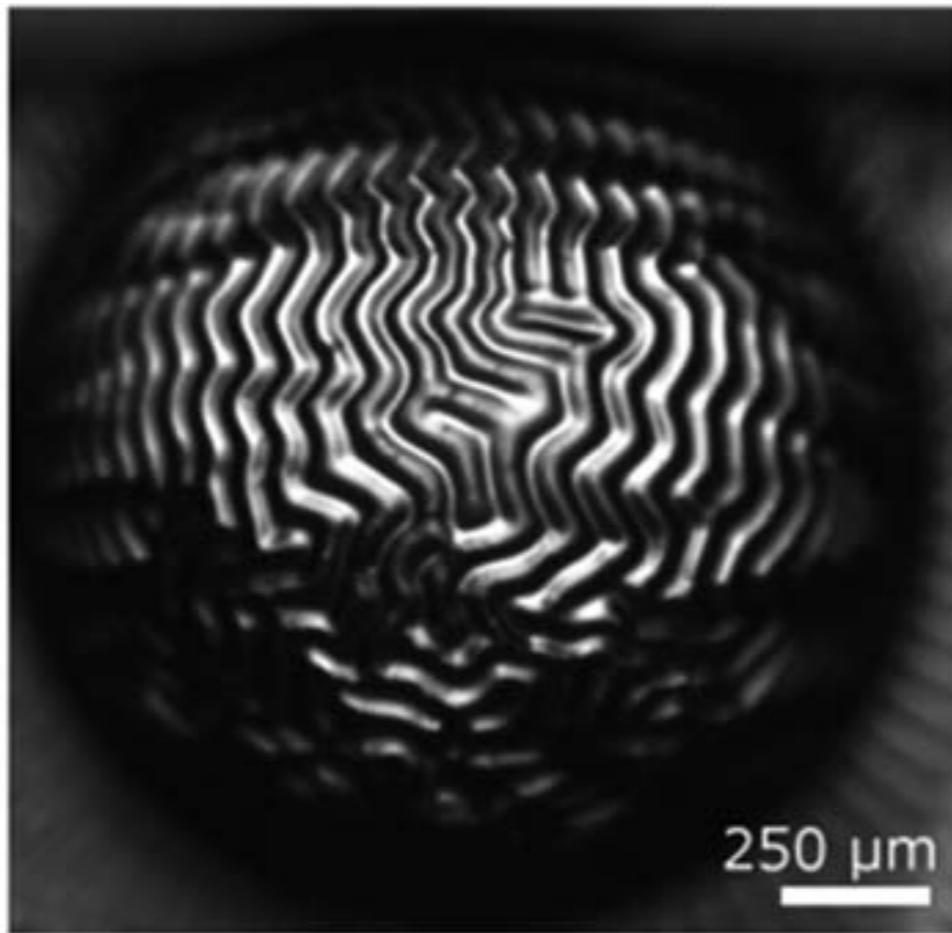


Further reading about structural colors and photonic crystals



<http://ab-initio.mit.edu/book/>

Wrinkled surfaces

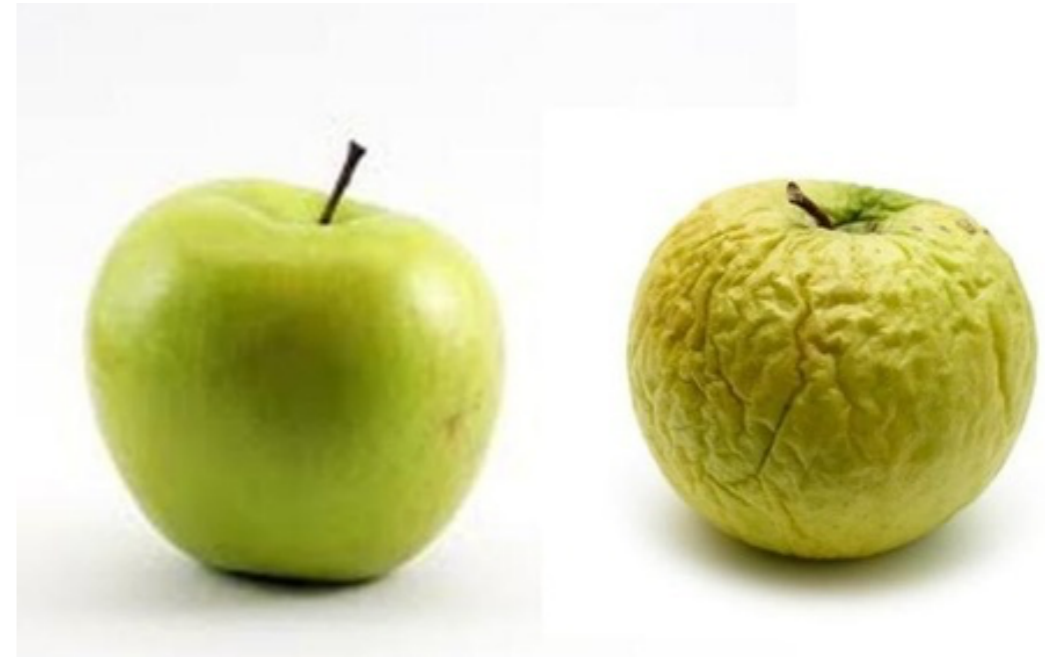


Why do we get wrinkled surfaces?

Fingers after being exposed to water for some time



Old apple



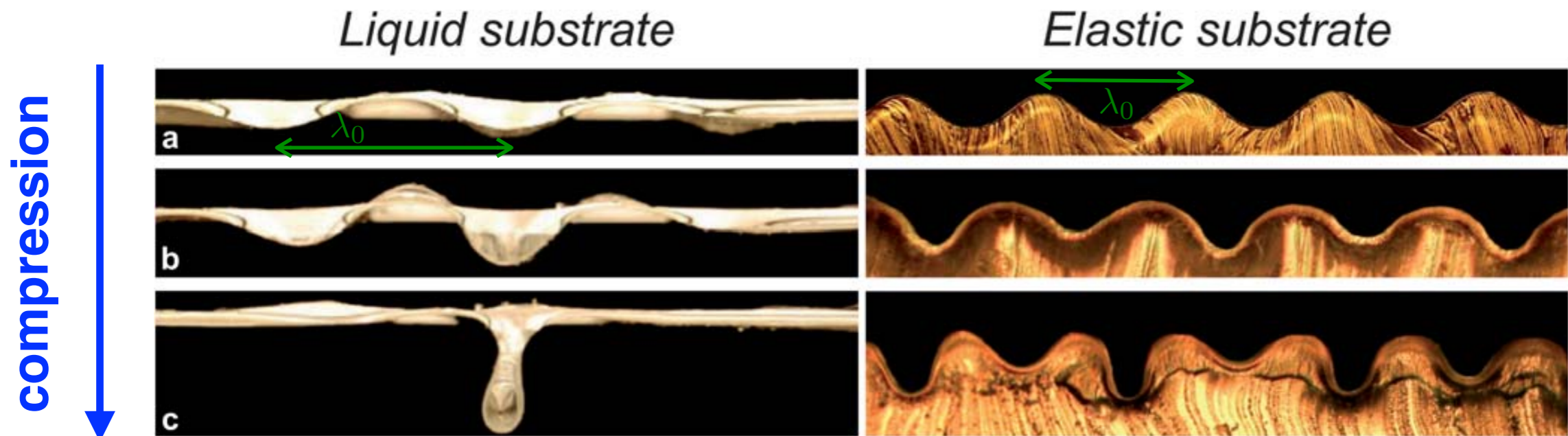
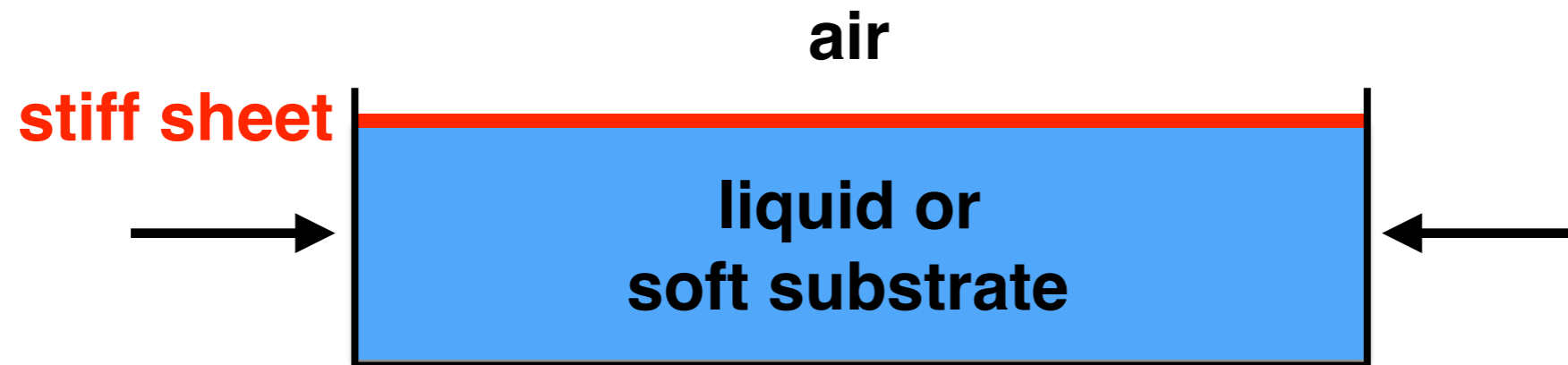
Brain



Rising dough



Compression of stiff thin sheets on liquid and soft elastic substrates



10 μm thin sheet of polyester on water

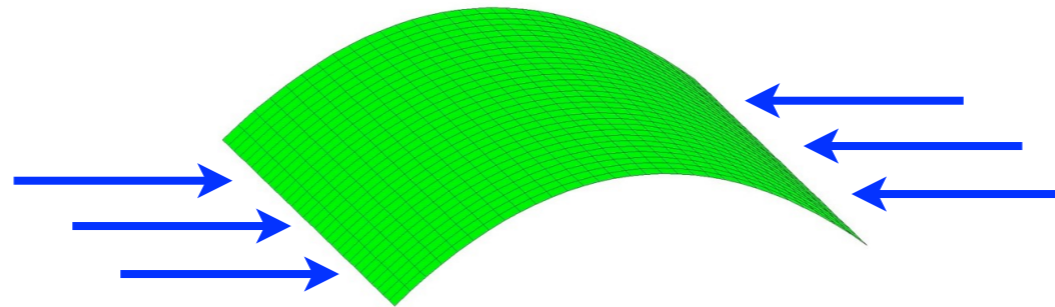
$$\lambda_0 = 1.6 \text{ cm}$$

$\sim 10 \mu\text{m}$ thin PDMS (stiffer) sheet on PDMS (softer) substrate

$$\lambda_0 = 70 \mu\text{m}$$

Buckling vs wrinkling

Compressed thin sheets buckle



Compressed thin sheets on liquid and soft elastic substrates wrinkle

Liquid substrate

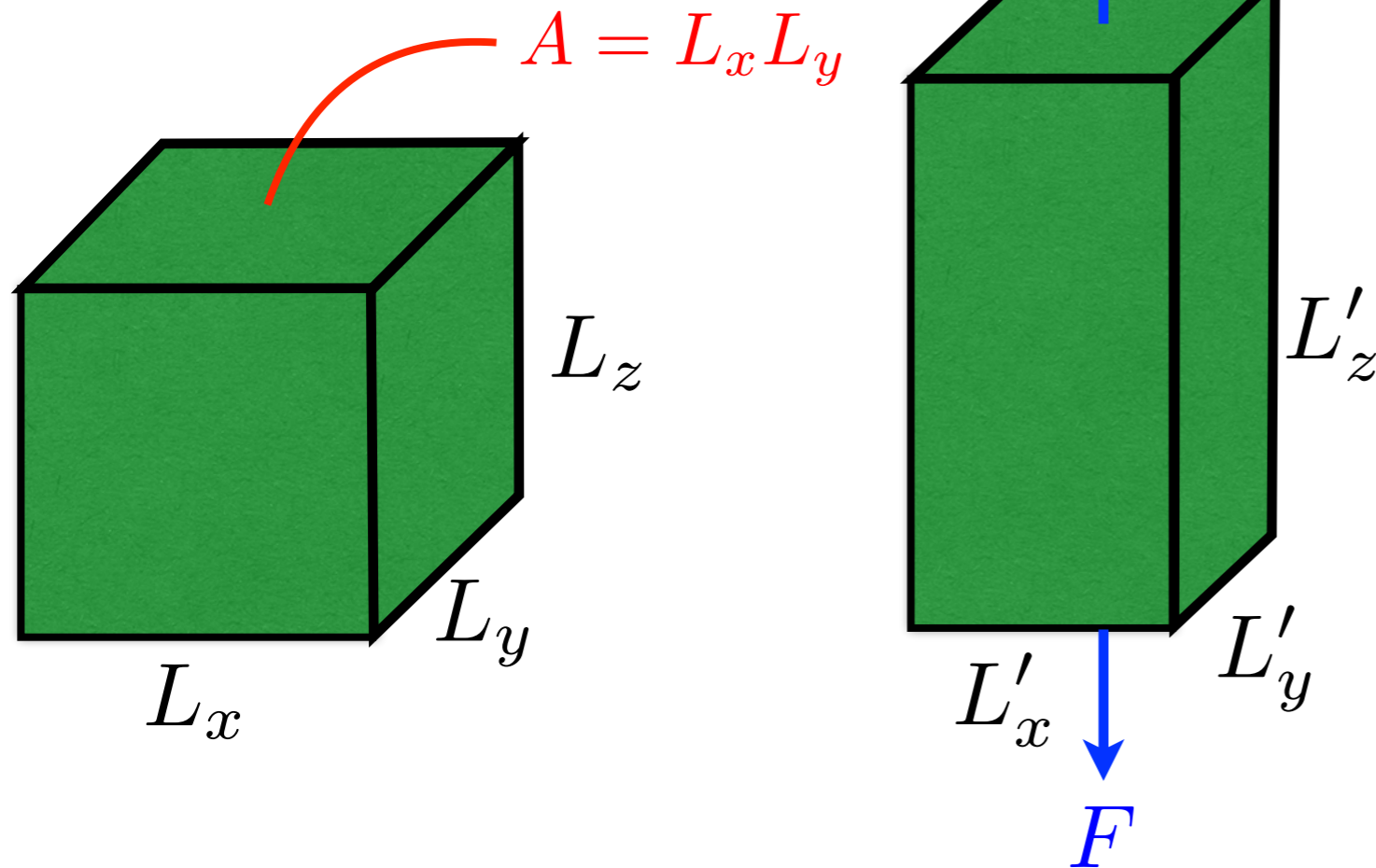
Elastic substrate



In compressed thin sheets on liquid and soft elastic substrates global buckling is suppressed, because it would result in very large energy cost associated with deformation of the liquid or soft elastic substrate!

Brief intro to mechanics: Young's modulus

undeformed
material element



Hooke's law
(small deformations)

$$\frac{F}{A} = E \frac{\Delta L_z}{L_z}$$

normal stress: $\sigma = F/A$

Young's modulus: E

normal strain: $\epsilon = \Delta L_z / L_z$

Elastic energy of deformation

$$U = \frac{1}{2} V E \epsilon^2$$

element volume: $V = L_x L_y L_z$

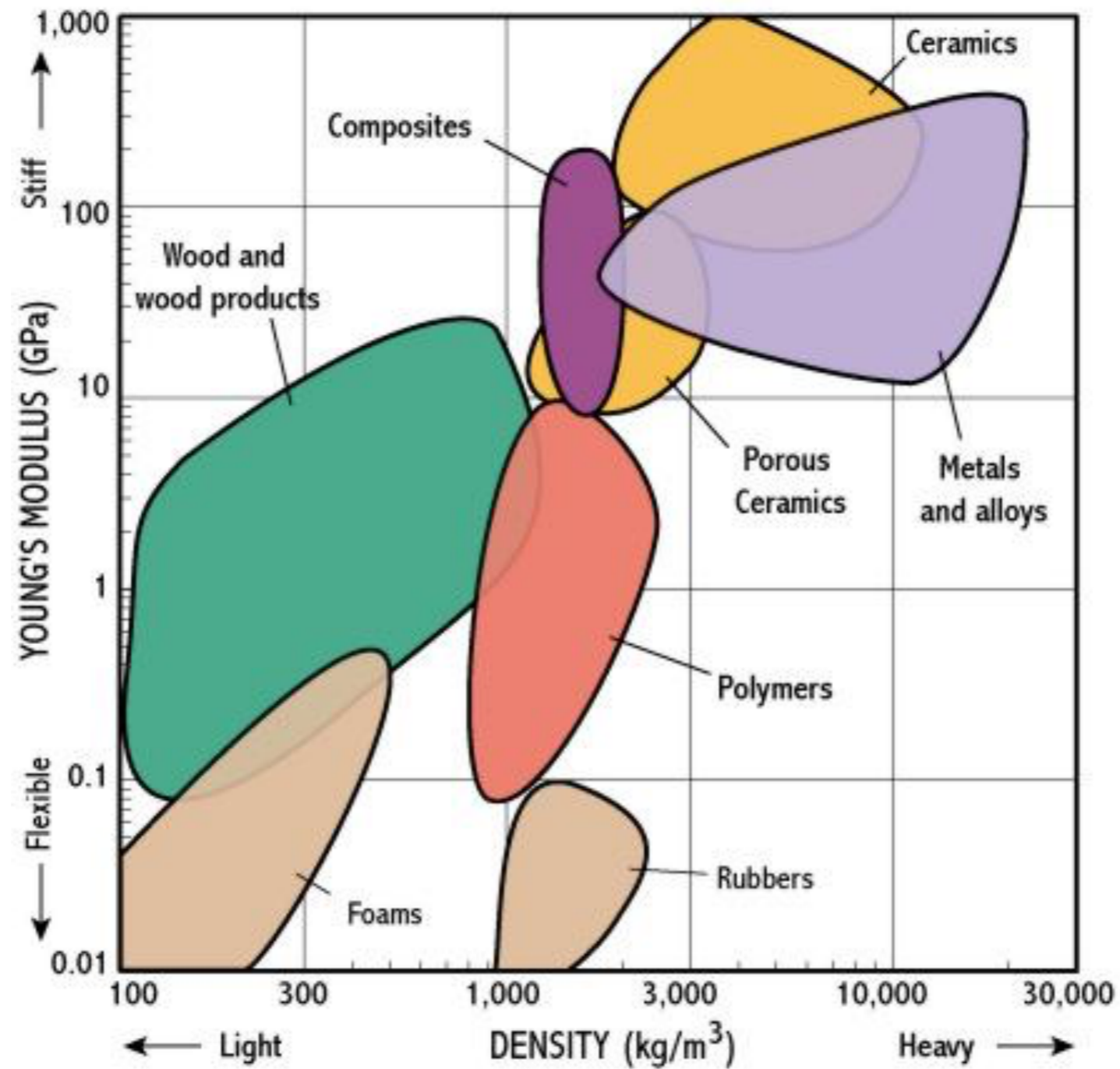
Robert Hooke
(1635-1703)



Thomas Young
(1773-1829)

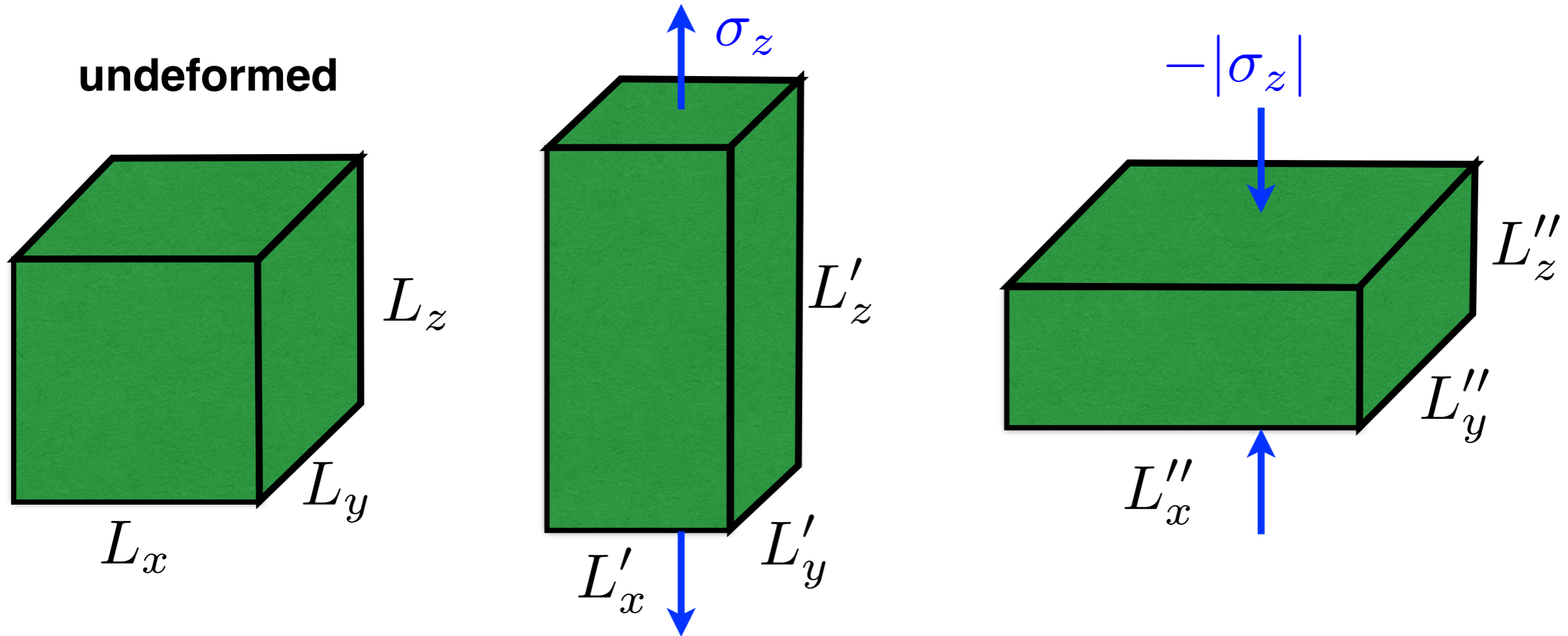


Young's modulus of materials



<http://www-materials.eng.cam.ac.uk/mpsite/physics/introduction/>

Poisson's ratio



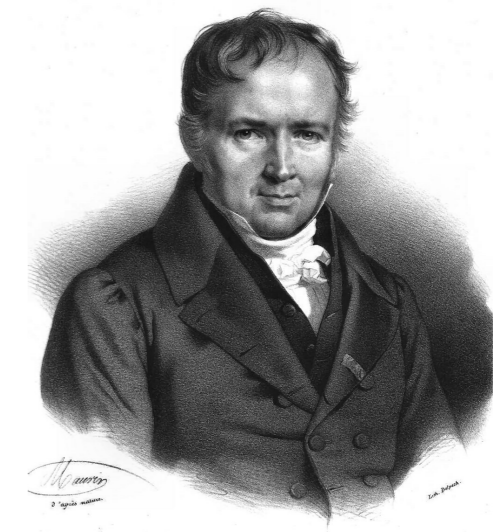
Typically material shrinks (expands) in the transverse direction of the axial tension (compression)!

Simeon Poisson
(1781-1840)

$$\nu = -\frac{\epsilon_x}{\epsilon_z} = -\frac{\epsilon_y}{\epsilon_z}$$

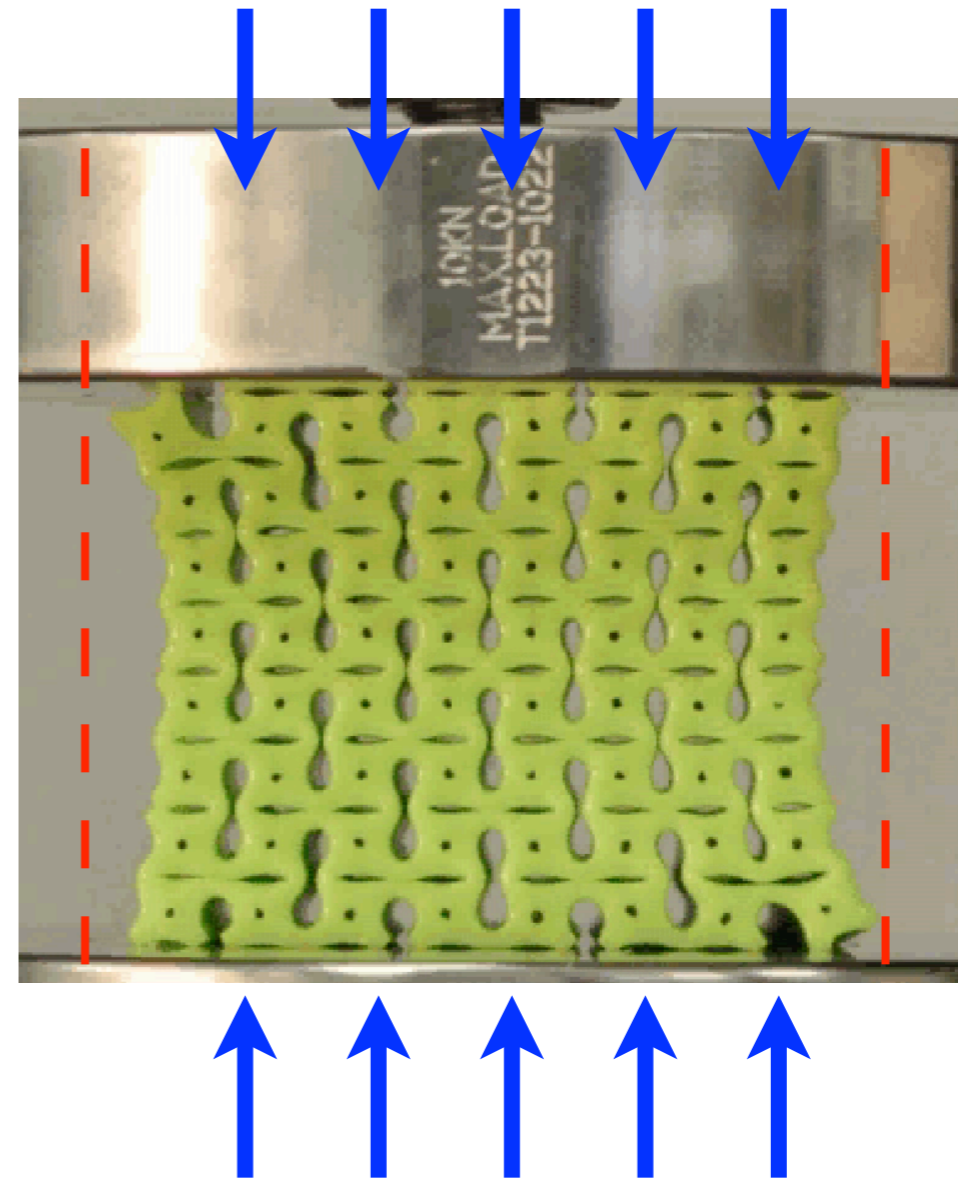
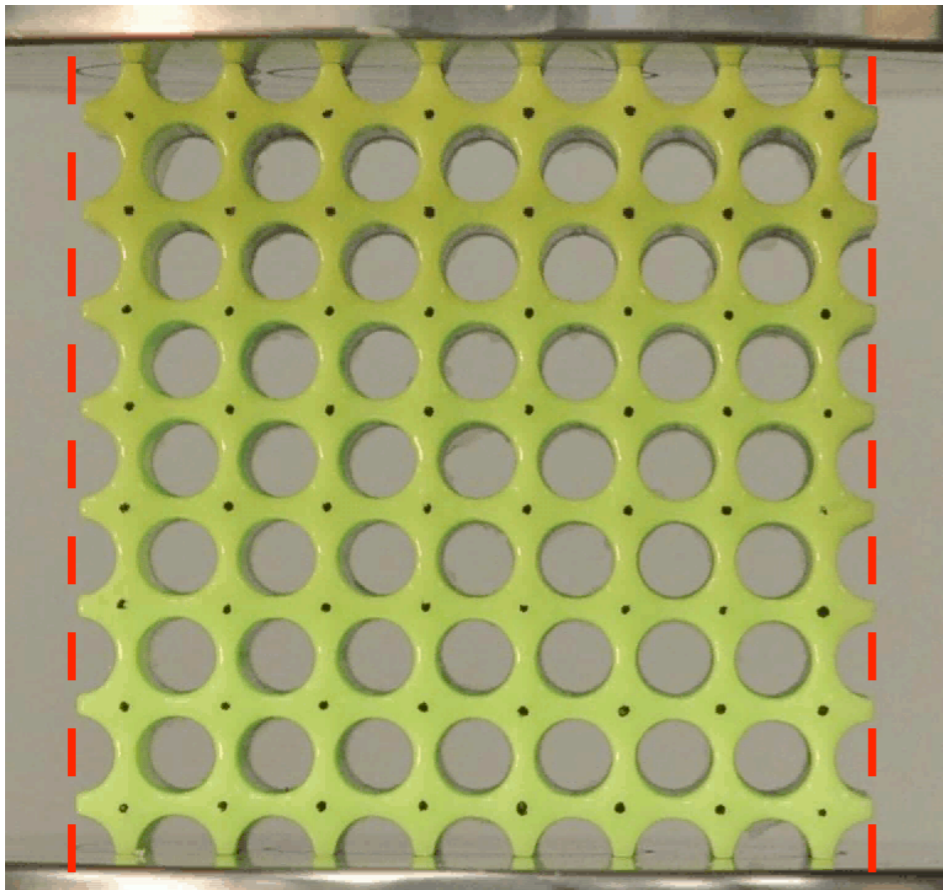
$$\epsilon_z = \frac{\sigma_z}{E}$$

normal strains: $\epsilon_i = \frac{\Delta L_i}{L_i}$



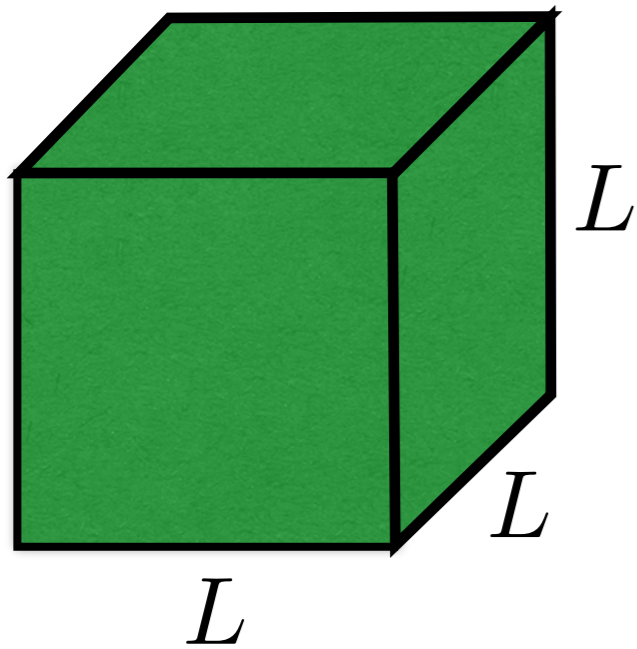
Effective negative Poisson's ratio for structures

Certain structures behave like they have effective negative Poisson's ratio, even though they are made of materials with positive Poisson's ratio!

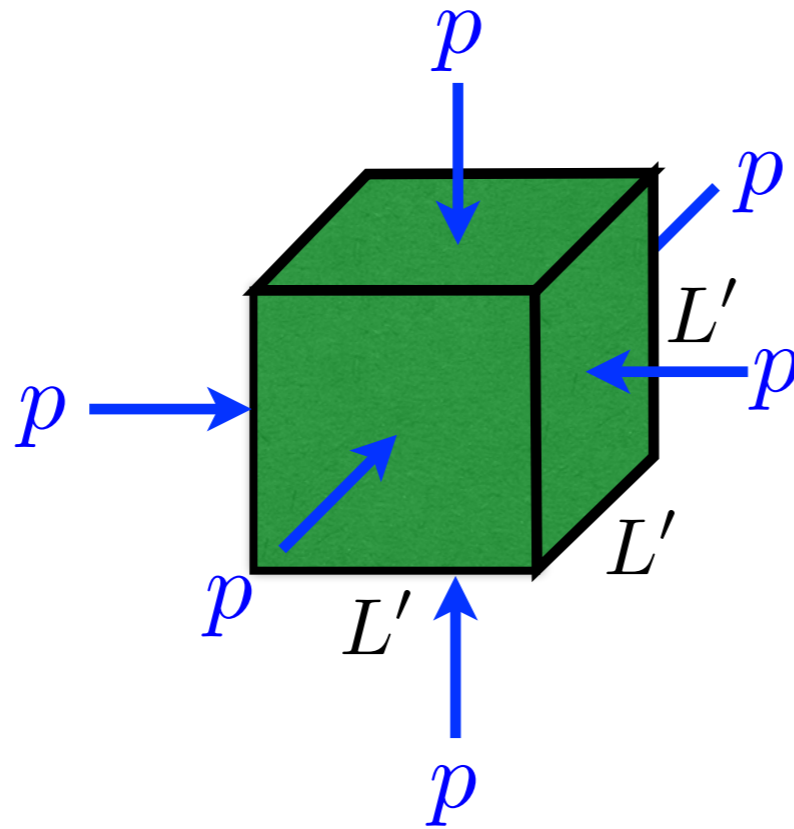


Bulk modulus

undeformed material element



hydrostatic stress



Hooke's law
(small deformations)

$$\frac{\Delta V}{V} = - \frac{p}{K}$$

hydrostatic stress: p

bulk modulus: $K = \frac{E}{3(1 - 2\nu)}$

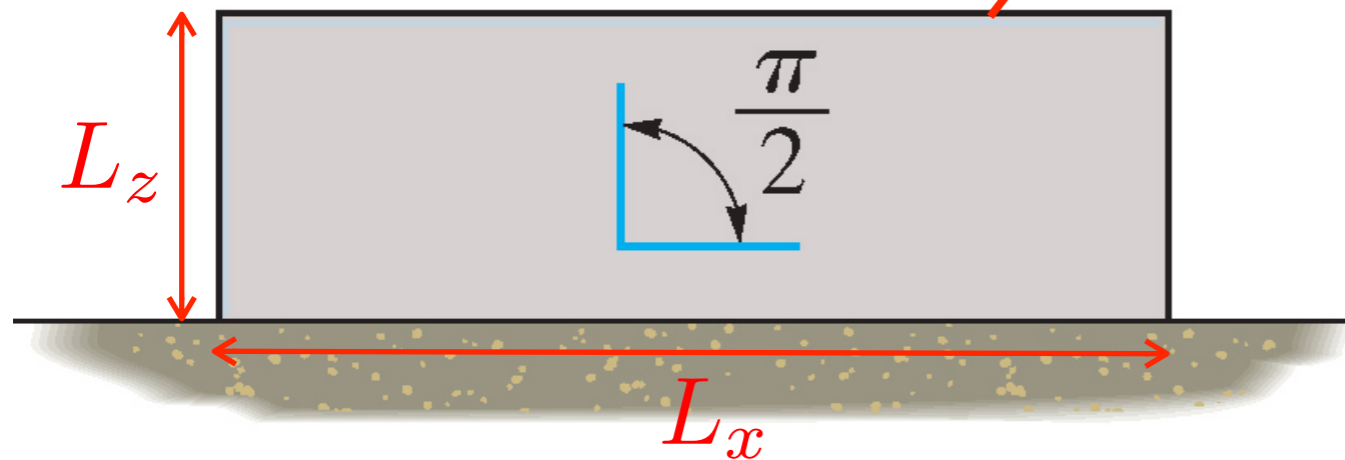
volumetric strain: $\frac{\Delta V}{V} \approx 3 \frac{\Delta L}{L}$

Elastic energy of deformation

$$U = \frac{1}{2} V K \left(\frac{\Delta V}{V} \right)^2 \sim V E \left(\frac{\Delta L}{L} \right)^2$$

Shear

undeformed material element



$$A = L_x L_y$$

Hooke's law
(small deformations)

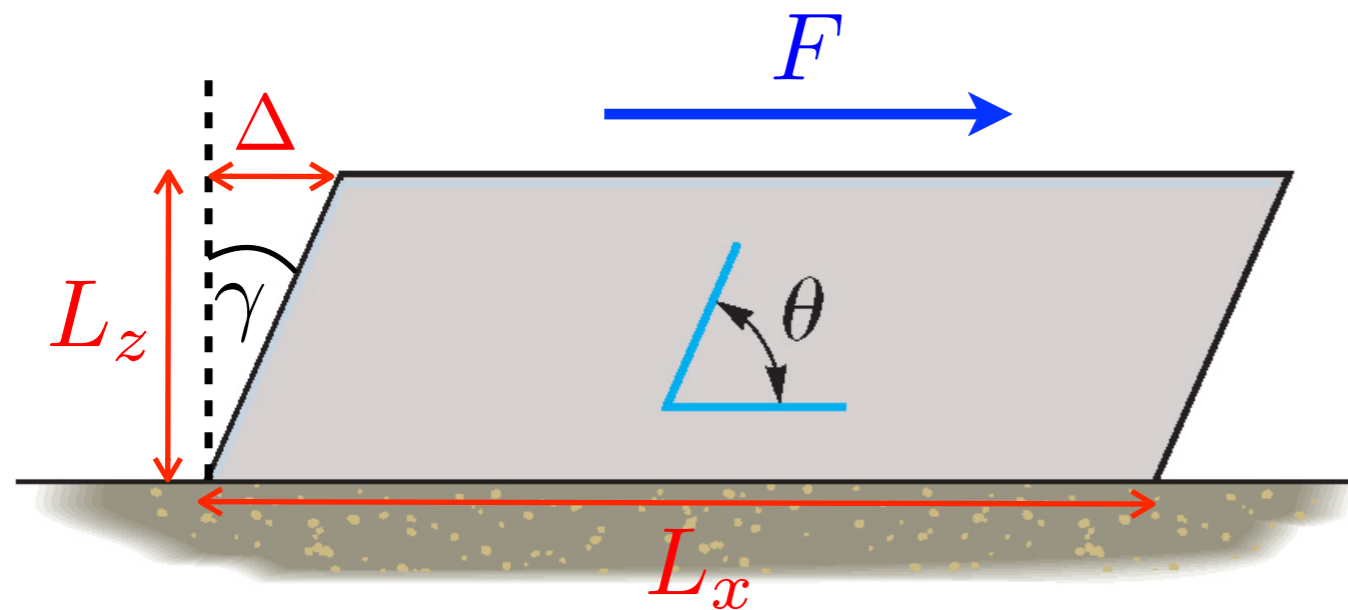
$$\frac{F}{A} = G \gamma$$

shear stress: $\tau = F/A$

shear modulus: $G = \frac{E}{2(1 + \nu)}$

shear strain: $\gamma = \arctan(\Delta/L_z)$

$$\gamma \approx \Delta/L_z$$



Elastic energy of deformation

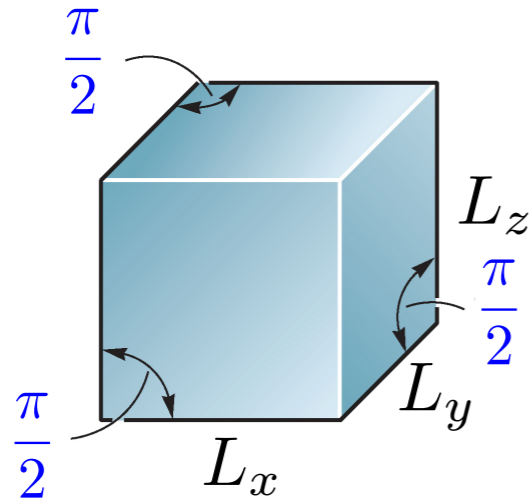
$$U = \frac{1}{2} V G \gamma^2 \sim V E \left(\frac{\Delta}{L_z} \right)^2$$

Note: shear does not change the volume of material element!

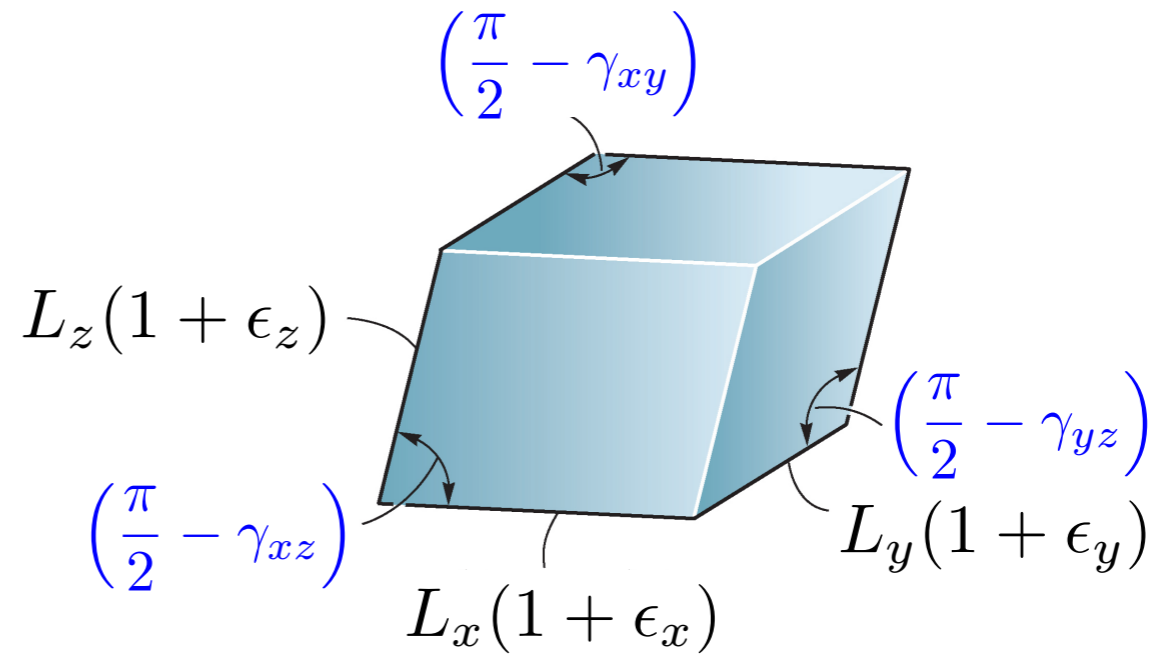
element volume: $V = L_x L_y L_z$

Arbitrary deformation of 3D solid element

undeformed element



deformed element

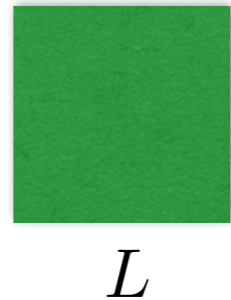


Arbitrary deformation can be decomposed to the volume change and the shear deformation.

$$U = U_{\text{bulk}} + U_{\text{shear}}$$

In plane deformations of thin sheets

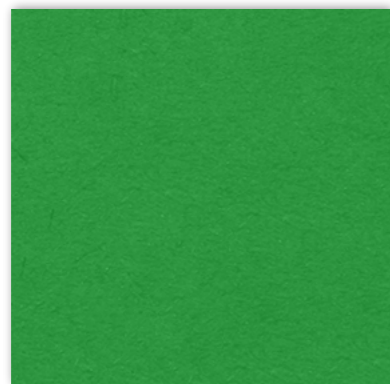
undeformed square patch of thin sheet



patch area
 $A = L^2$

sheet thickness t
Young's modulus E
Poisson's ratio ν

isotropic deformation



$L + \Delta L$

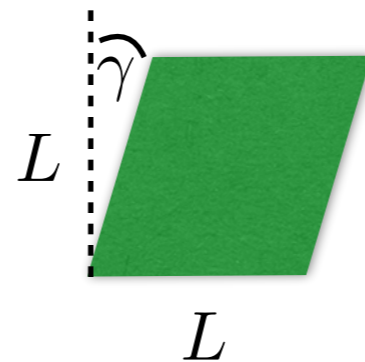
$L + \Delta L$

$$\frac{U}{A} = \frac{B}{2} \left(\frac{\Delta A}{A} \right)^2 \approx \frac{B}{2} \left(\frac{2\Delta L}{L} \right)^2$$

2D bulk modulus

$$B = \frac{Et}{2(1 - \nu)}$$

shear deformation



L

L

$$\frac{U}{A} = \frac{\mu\gamma^2}{2}$$

2D shear modulus

$$\mu = Gt = \frac{Et}{2(1 + \nu)}$$

anisotropic stretching



$L(1 + \epsilon_2)$

$L(1 + \epsilon_1)$

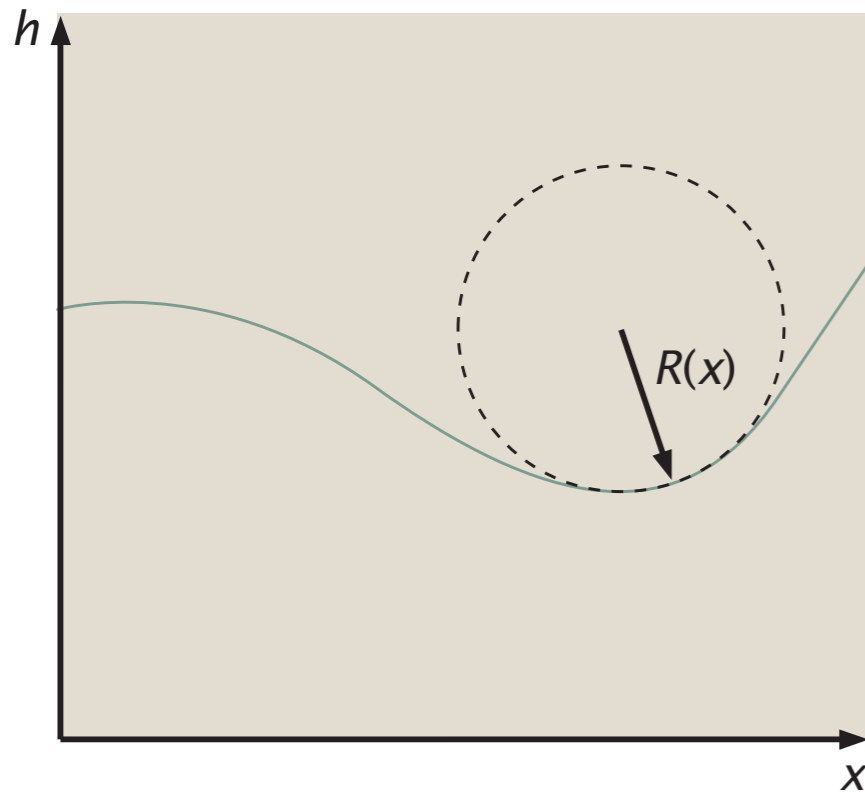
$$\frac{U}{A} = \frac{B}{2} (\epsilon_1 + \epsilon_2)^2 + \frac{\mu}{2} (\epsilon_1 - \epsilon_2)^2$$

$\epsilon_1, \epsilon_2 \ll 1$

(shearing can be interpreted as anisotropic stretching)

Curvature of surfaces

(A)

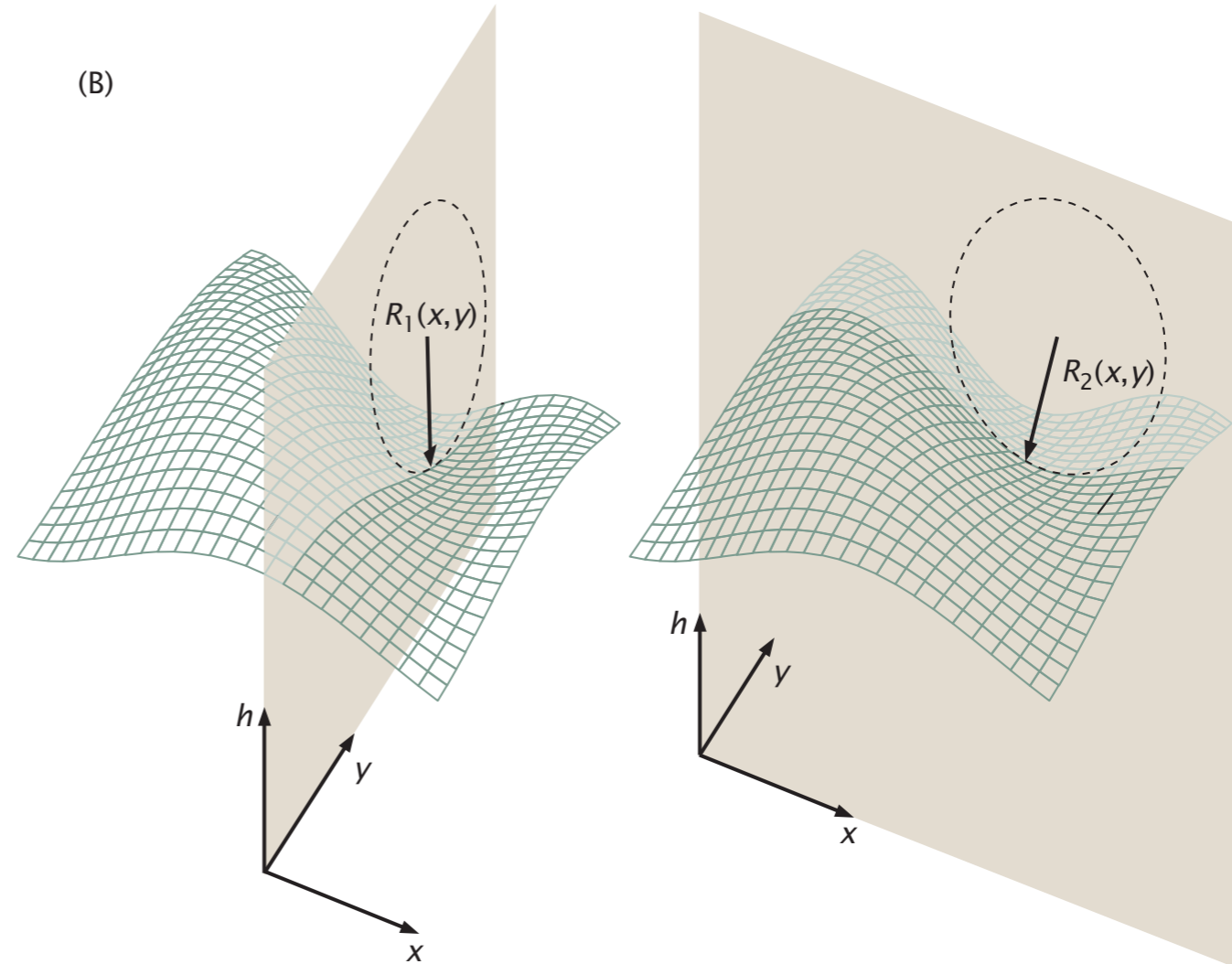


**curvature
of space curves**

$$\frac{1}{R} = \frac{h''}{(1 + h'^2)^{3/2}} \approx h''$$

R. Phillips et al., Physical
Biology of the Cell

(B)

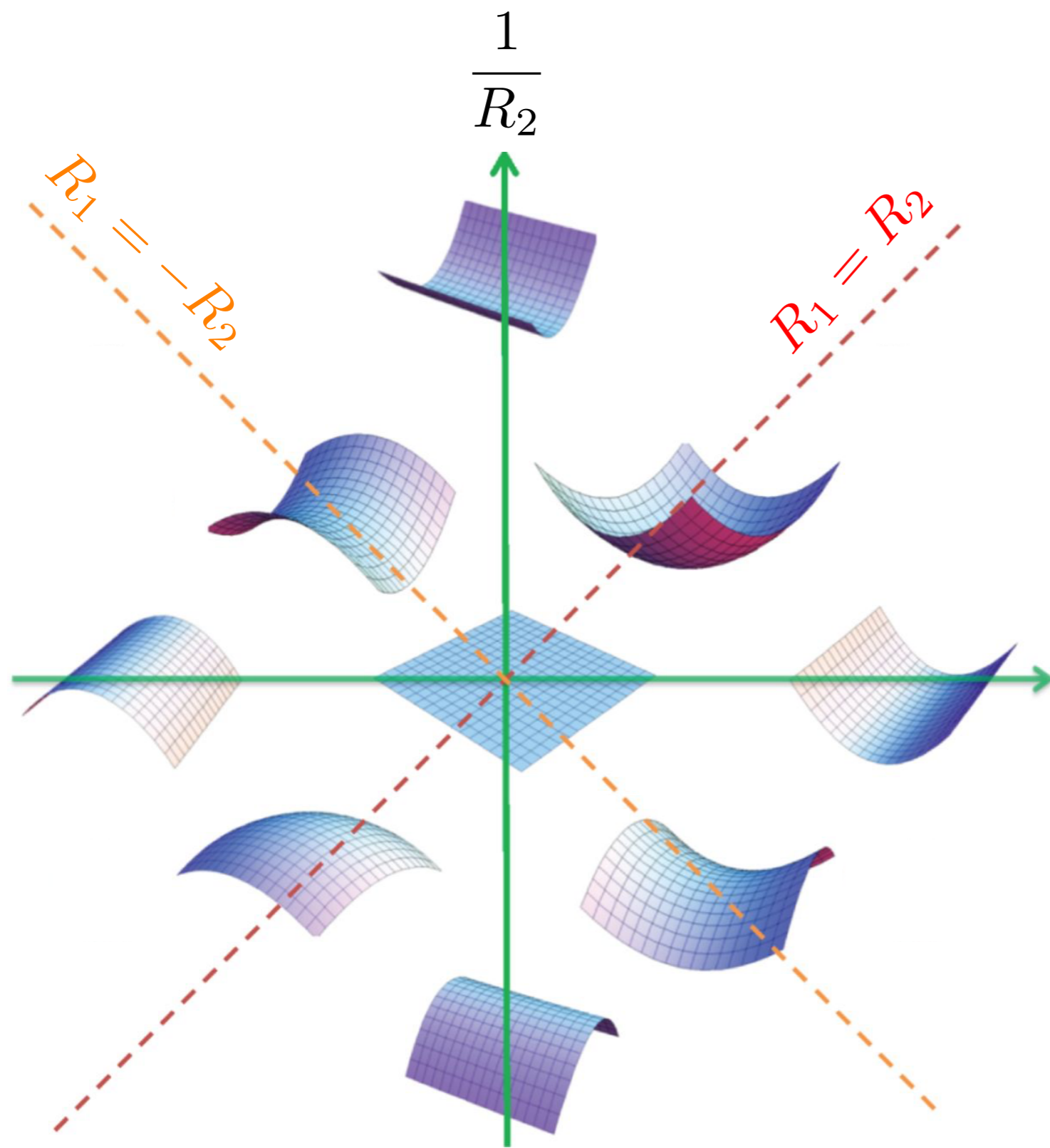


**curvature tensor
for surfaces**

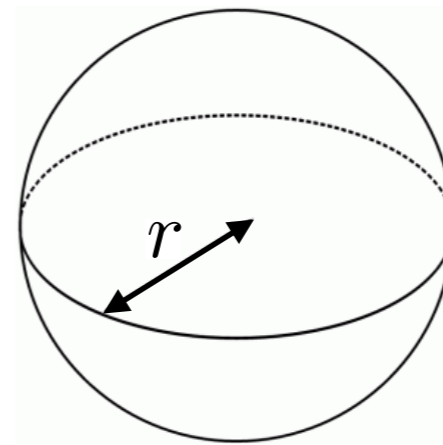
$$K_{ij} \approx \begin{pmatrix} \frac{\partial^2 h}{\partial x^2} & \frac{\partial^2 h}{\partial x \partial y} \\ \frac{\partial^2 h}{\partial x \partial y} & \frac{\partial^2 h}{\partial y^2} \end{pmatrix}$$

**maximal and
minimal curvatures
(principal curvatures)
correspond to the
eigenvalues of
curvature tensor**

Surfaces of various principal curvatures

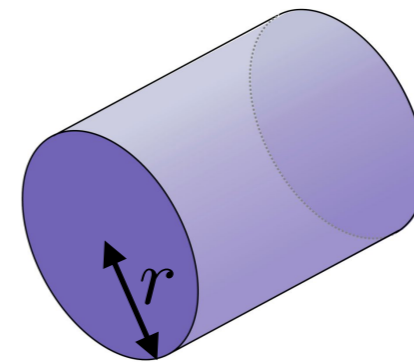


sphere



$$\frac{1}{R_1} = \frac{1}{R_2} = \frac{1}{r}$$

cylinder



$$\frac{1}{R_1}$$

$$\frac{1}{R_1} = \frac{1}{r}$$

$$\frac{1}{R_2} = 0$$

potato chips = "saddle"

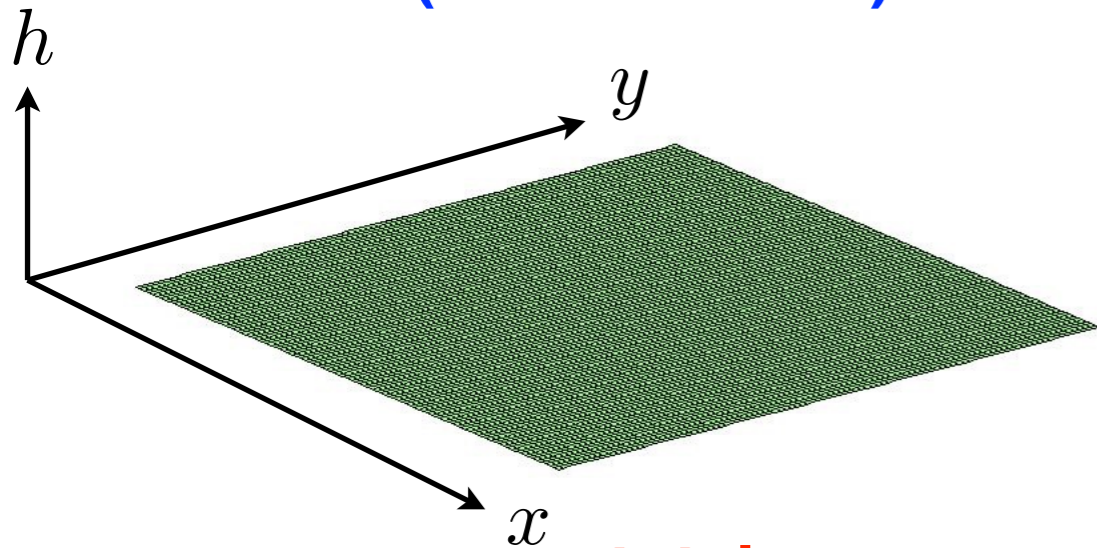


$$\frac{1}{R_1} > 0$$

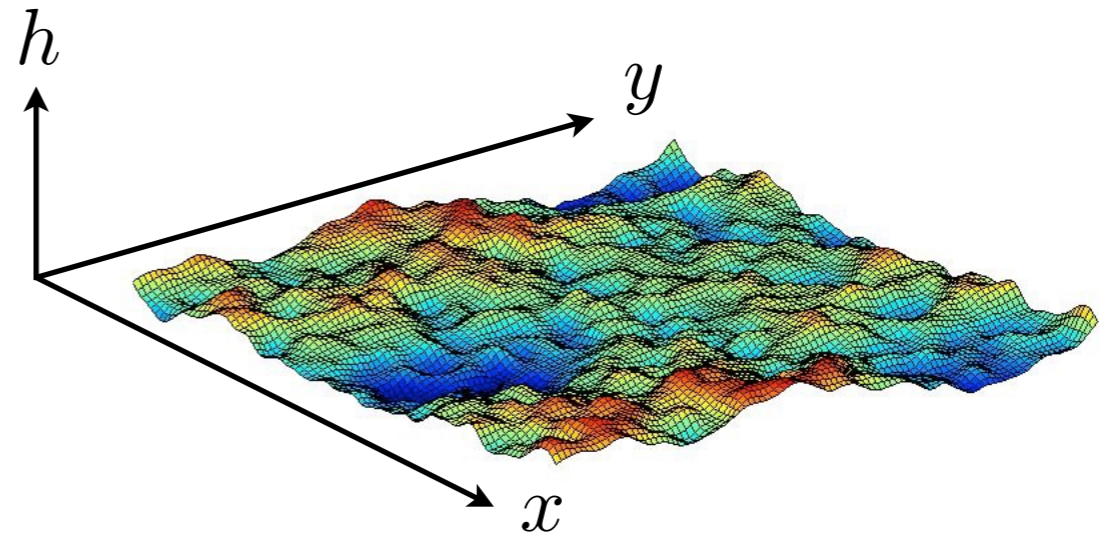
$$\frac{1}{R_2} < 0$$

Bending energy cost for thin sheets

undeformed thin sheet
(thickness t)



deformed thin sheet



total mean curvature

Gaussian curvature

$$U = \int dA \left[\frac{\kappa}{2} \left(\frac{1}{R_1} + \frac{1}{R_2} \right)^2 + \kappa_G \frac{1}{R_1 R_2} \right]$$

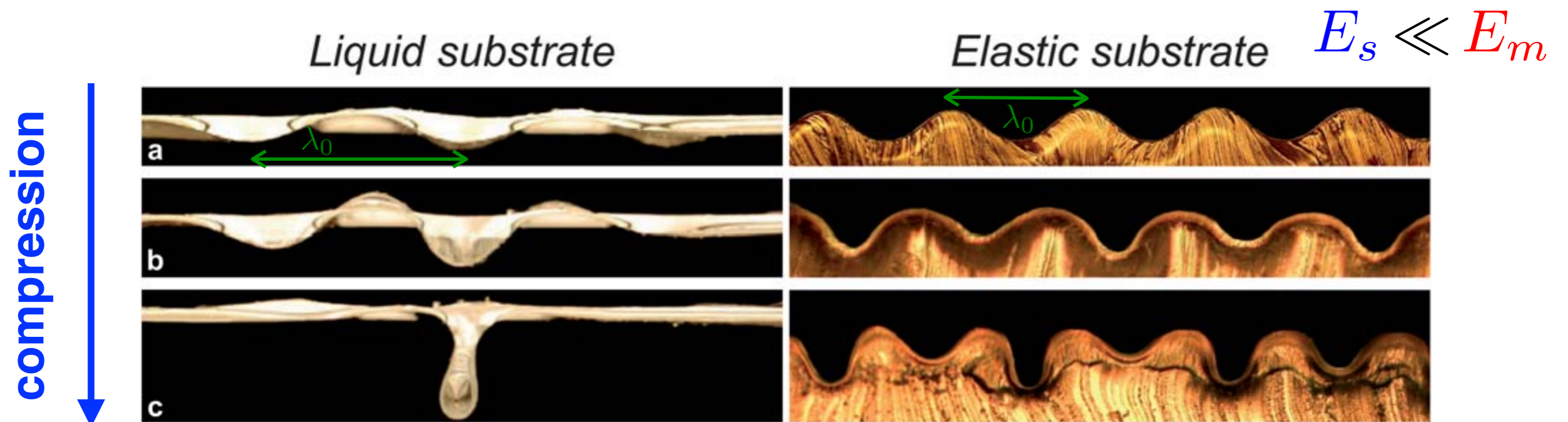
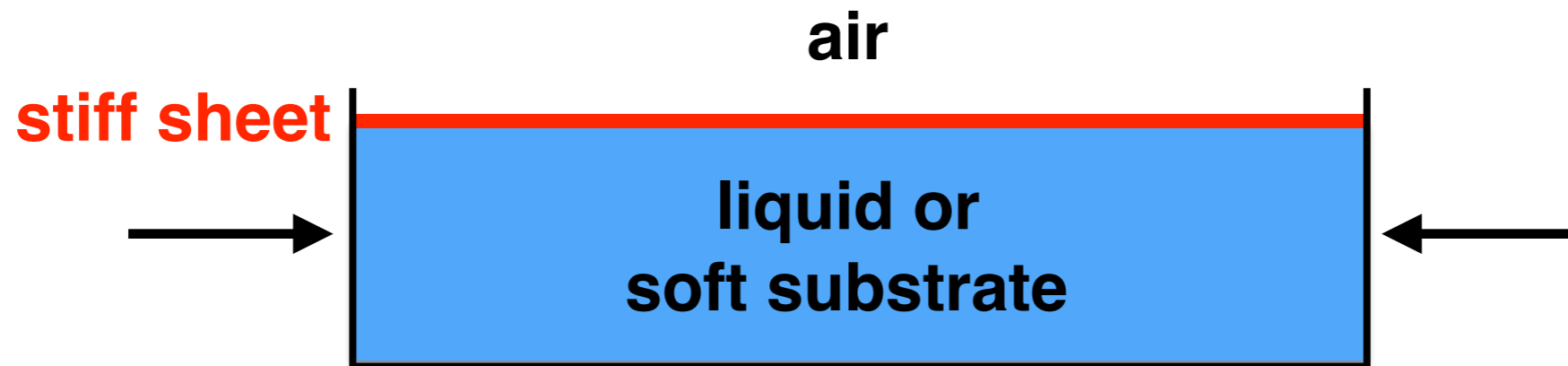
$$U \approx \int dx dy \left[\frac{\kappa}{2} \left(\frac{\partial^2 h}{\partial x^2} + \frac{\partial^2 h}{\partial y^2} \right)^2 + \kappa_G \det \left(\frac{\partial^2 h}{\partial x_i \partial x_j} \right) \right]$$

$$x_i, x_j \in \{x, y\}$$

bending rigidity
(flexural rigidity) $\kappa = \frac{Et^3}{12(1-\nu^2)}$

Gauss bending rigidity $\kappa_G = -\frac{Et^3}{12(1+\nu)}$

Compression of stiff thin sheets on liquid and soft elastic substrates



10 μm thin sheet of polyester on water

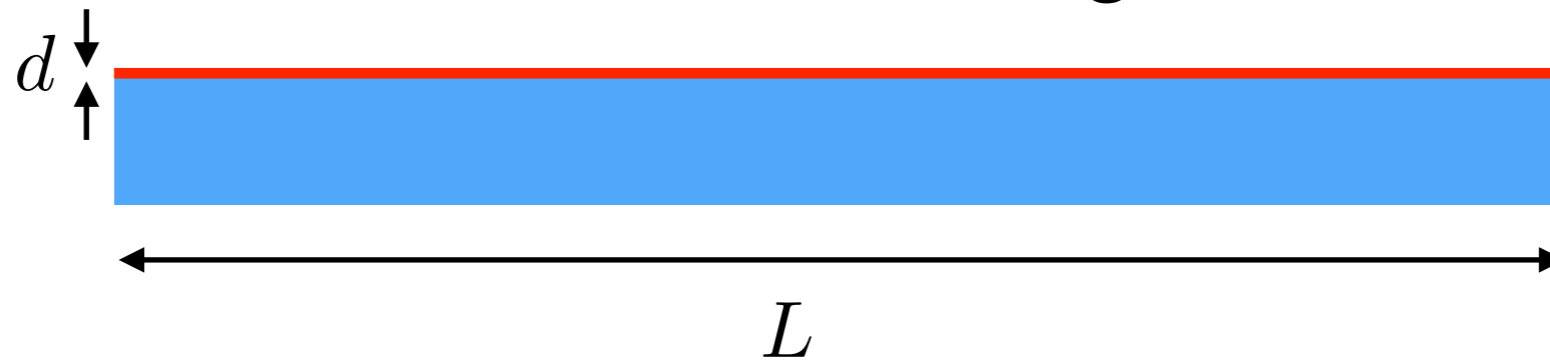
$$\lambda_0 = 1.6 \text{ cm}$$

$\sim 10 \mu\text{m}$ thin PDMS (stiffer) sheet on PDMS (softer) substrate

$$\lambda_0 = 70 \mu\text{m}$$

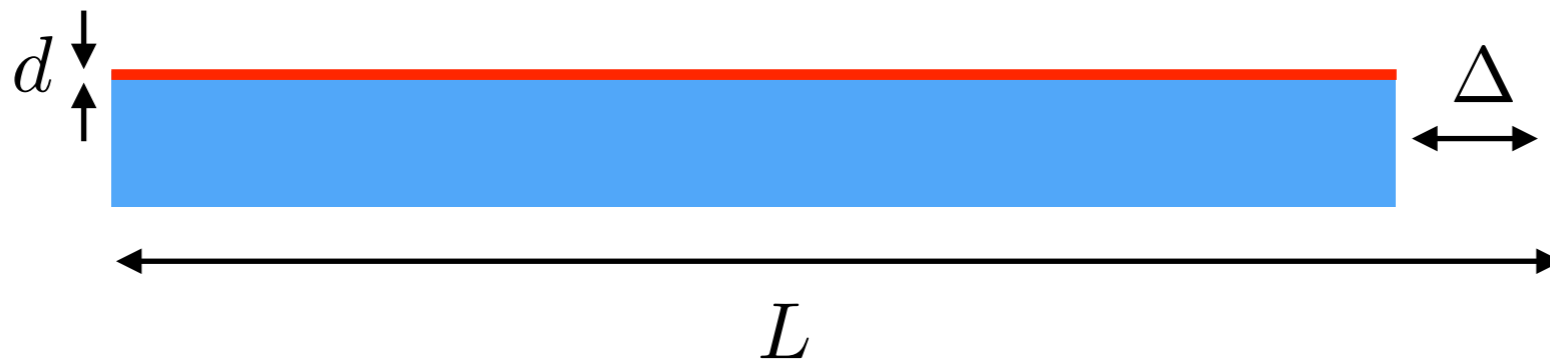
Compression of stiff thin membranes on liquid substrates

initial undeformed configuration

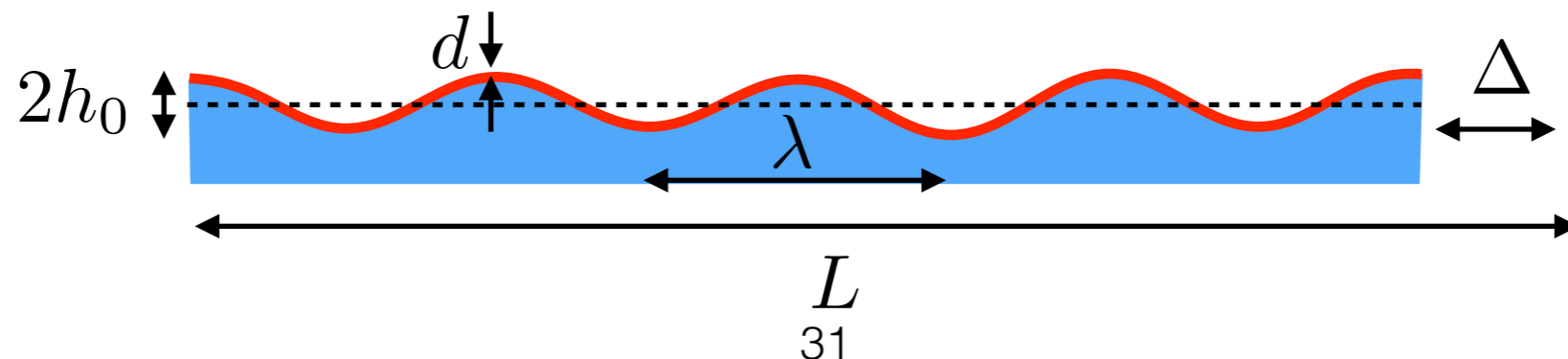


Consider the energy cost for two different scenarios:

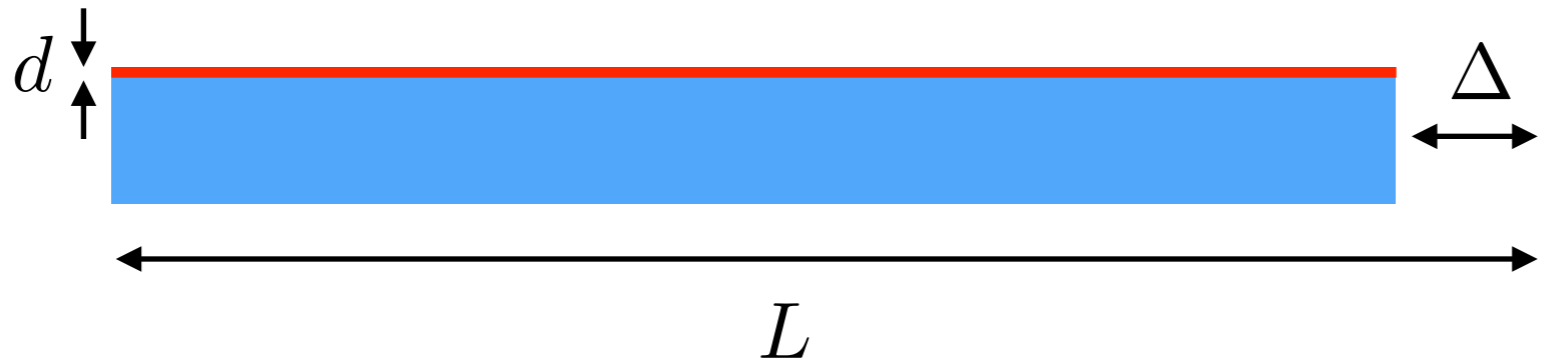
1.) thin membrane is compressed (no bending)



**2.) thin membrane is wrinkled (no compression)
+ additional potential energy of liquid**



Compression of stiff thin membranes on liquid substrates



compression energy of thin membrane

$$U_c \sim A \times E_m d \times \epsilon^2$$

**membrane
area**

$$A = WL$$

**membrane
3D Young's
modulus**

$$E_m$$

strain

$$\epsilon = \frac{\Delta}{L}$$

**liquid
density**

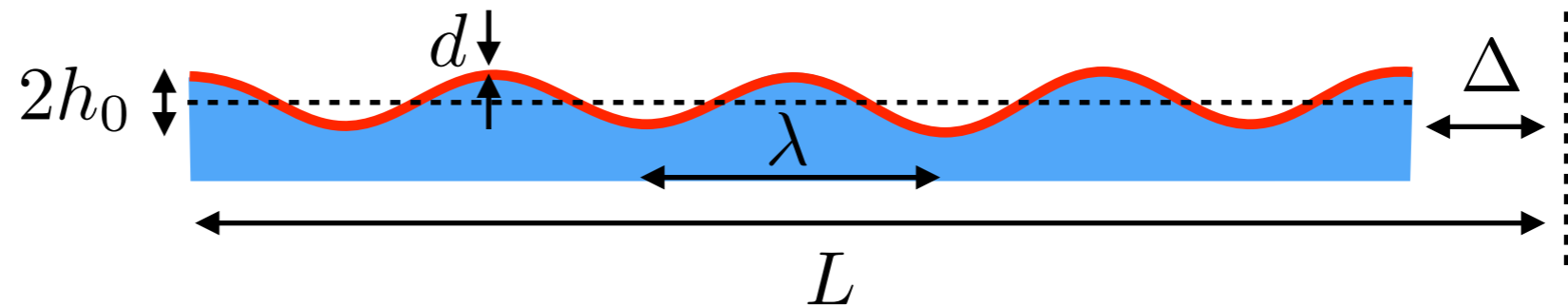
$$\rho$$

Note: upon compression the liquid surface also raises, but we will measure the potential energy relative to this new height!

Compression of stiff thin membranes on liquid substrates

assumed profile

$$h(s) = h_0 \cos(2\pi s/\lambda)$$



projected length assuming that membrane doesn't stretch

$$L - \Delta = \int_0^L ds \sqrt{1 - h'(s)^2} \approx \int_0^L ds \left(1 - \frac{h'(s)^2}{2}\right) \approx L \left(1 - \frac{\pi^2 h_0^2}{\lambda^2}\right)$$

amplitude of wrinkles

$$h_0 = \frac{\lambda}{\pi} \sqrt{\frac{\Delta}{L}} = \frac{\lambda \sqrt{\epsilon}}{\pi}$$

bending energy of stiff membrane

$$U_b \sim A \times \kappa \times \frac{1}{R^2} \sim A \times E_m d^3 \times \frac{h_0^2}{\lambda^4} \sim \frac{A E_m d^3 \epsilon}{\lambda^2}$$

potential energy of liquid

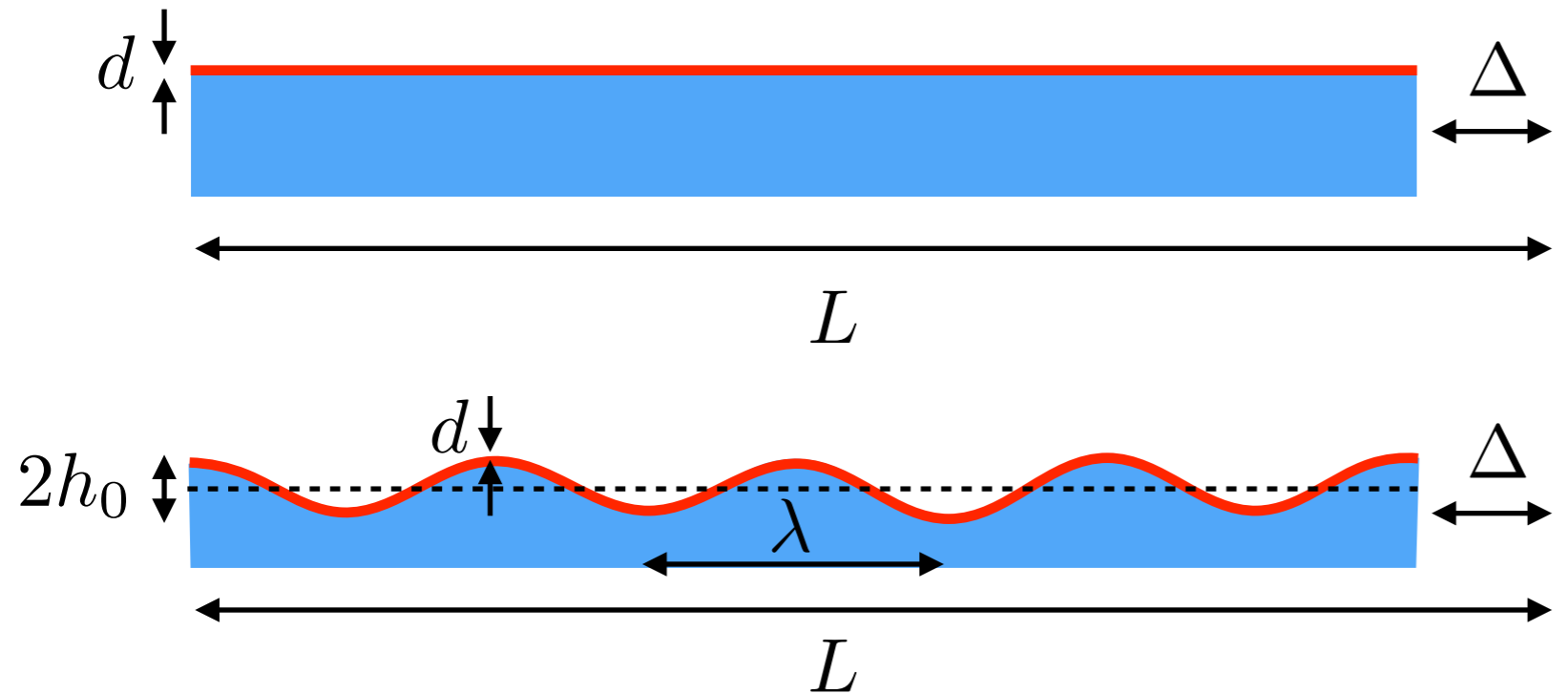
$$U_p \sim m \times g \times \Delta h \sim \rho \times A h_0 \times g \times h_0 \sim A \rho g \lambda^2 \epsilon$$

minimize total energy ($U_b + U_p$) with respect to λ

$$\lambda \sim \left(\frac{E_m d^3}{\rho g}\right)^{1/4}$$

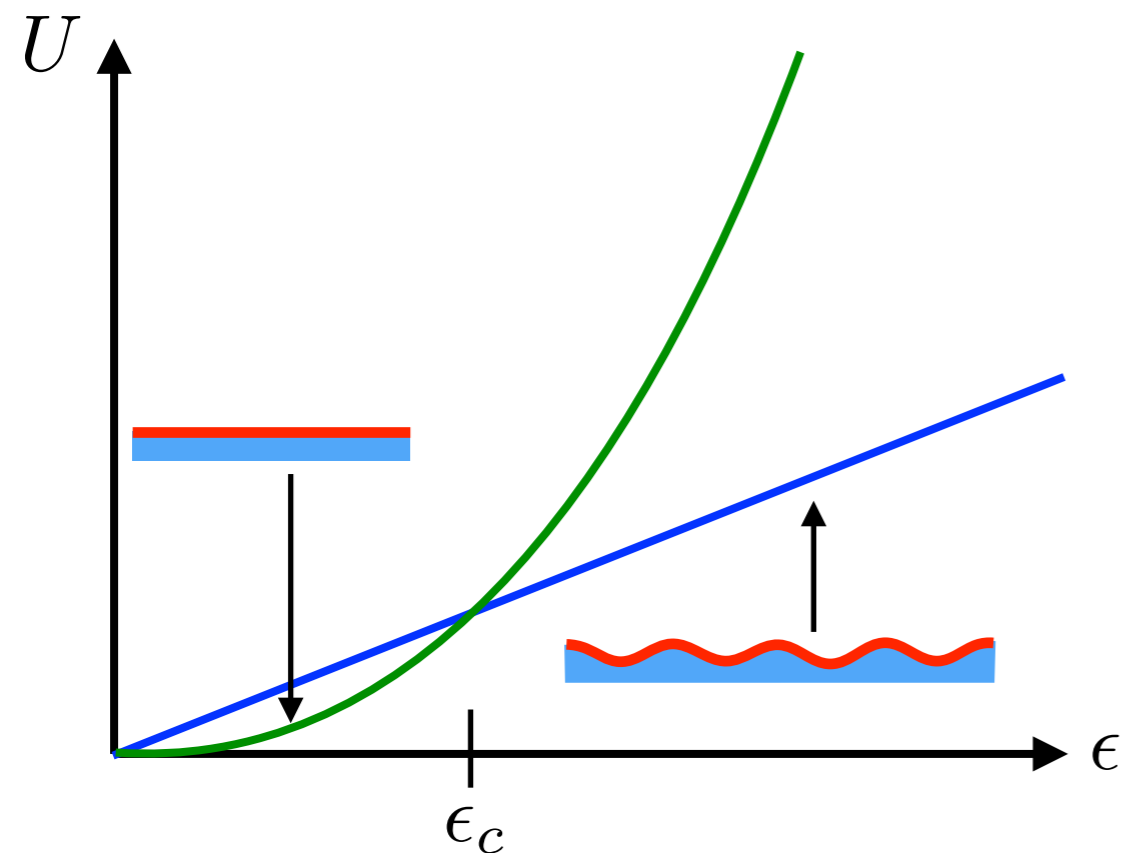
$$U_b, U_p \sim A \epsilon \sqrt{E_m d^3 \rho g}$$

Compression of stiff thin membranes on liquid substrates



$$U_c \sim A \times E_m d \times \epsilon^2$$

$$U_b, U_p \sim A \epsilon \sqrt{E_m d^3 \rho g}$$



wrinkles are stable above the critical strain

wavelength of wrinkles

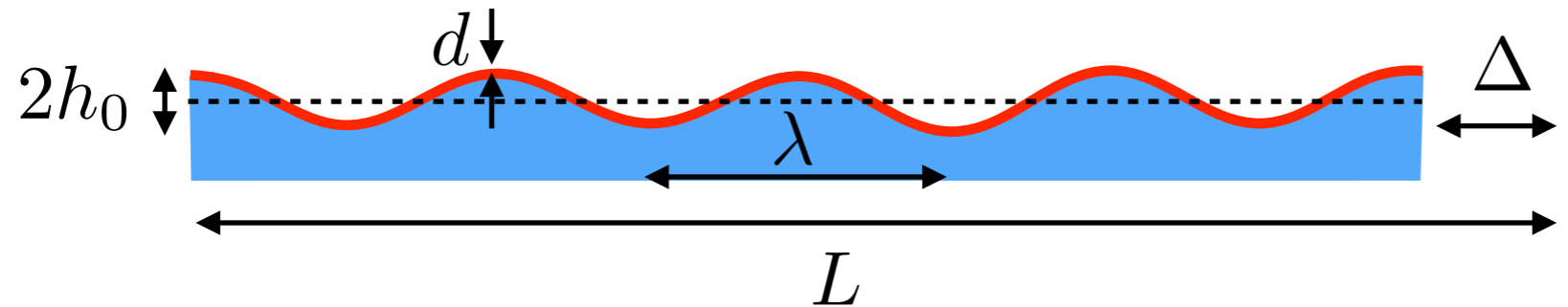
amplitude of wrinkles at the critical strain

$$\epsilon > \epsilon_c \sim \sqrt{\frac{\rho g d}{E_m}}$$

$$\lambda \sim \left(\frac{E_m d^3}{\rho g} \right)^{1/4}$$

$$h_0^* \sim \lambda \sqrt{\epsilon_c} \sim d$$

Compression of stiff thin membranes on liquid substrates



scaling analysis

$$\lambda \sim \left(\frac{E_m d^3}{\rho g} \right)^{1/4}$$

exact result

$$\lambda = 2\pi \left(\frac{\kappa}{\rho g} \right)^{1/4}$$

$$\kappa = \frac{E_m d^3}{12(1 - \nu_m^2)}$$

