

Design Methodologies for High Frequency Multiwinding Magnetics: from Fundamental Principles to Design Tools

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Assistant Professor

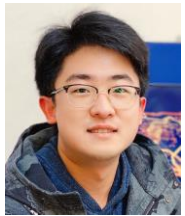
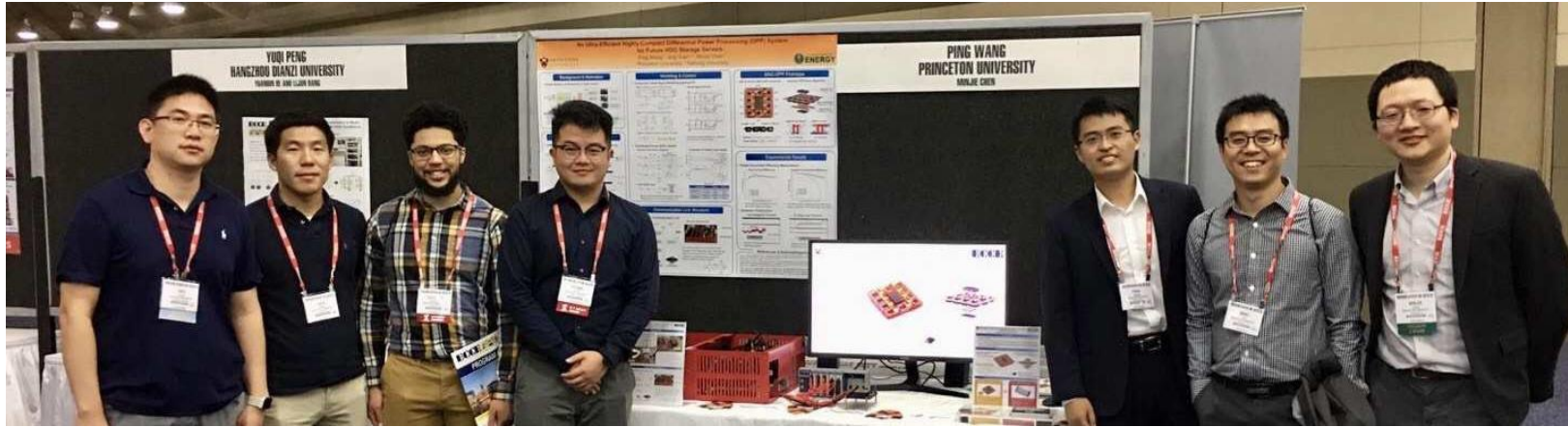
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Design Methodology Webinar Series, 2021



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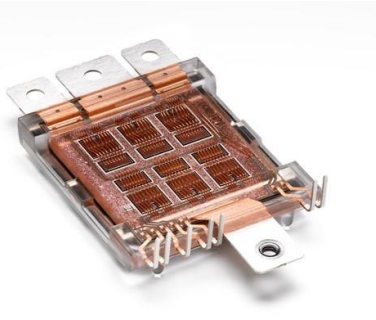


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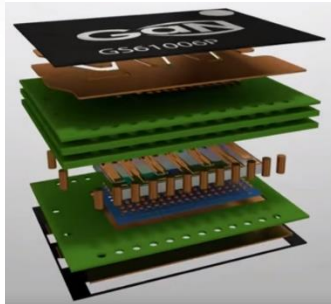


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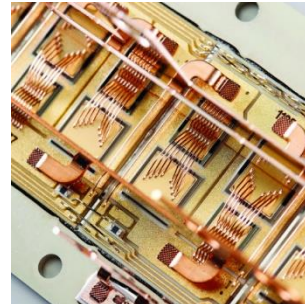
❑ Major breakthroughs in power semiconductor devices



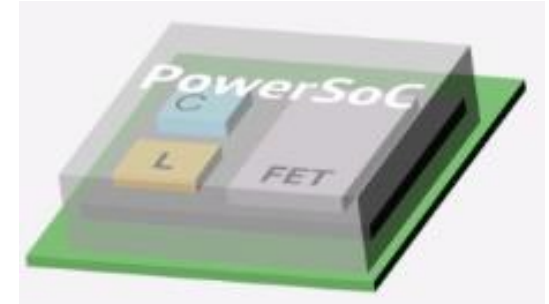
SiC modules



GaN switches

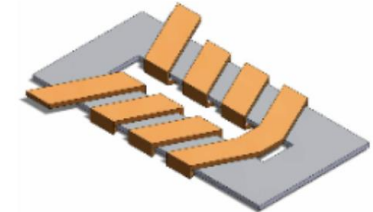
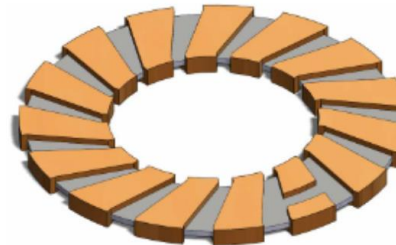
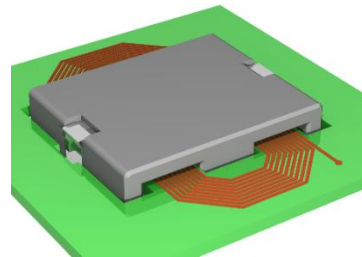
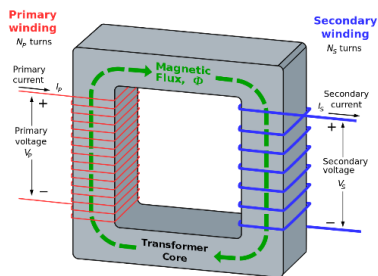


IGBT modules



Packaging & cooling

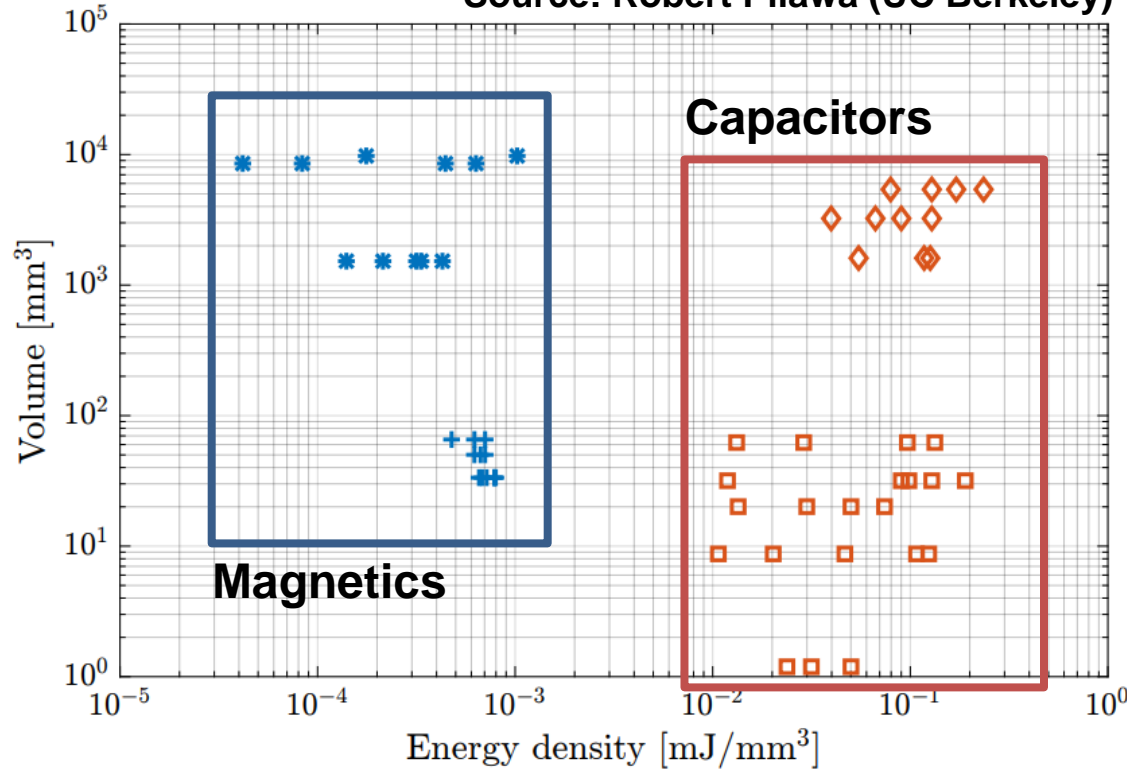
❑ Magnetics are lagging behind (both discrete and integrated)



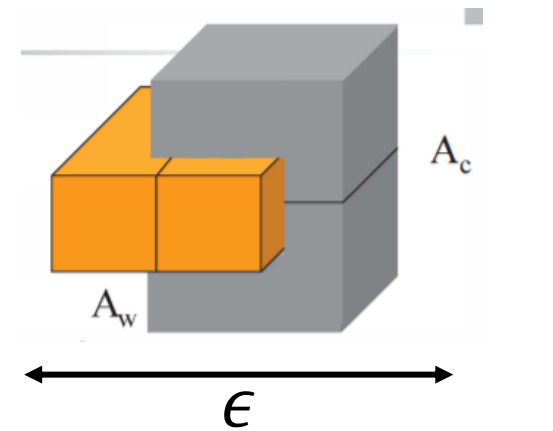
- C. R. Sullivan, M. Chen, "Coupled Inductors for Fast-Response High-Density Power Delivery: Discrete and Integrated," IEEE Custom Integrated Circuits Conference (CICC), 2021 (accepted).

Energy Density vs. Functionality

Source: Robert Pilawa (UC Berkeley)



Source: Charles Sullivan (Dartmouth)



$$V \propto \epsilon^2 \quad I \propto \epsilon^2$$

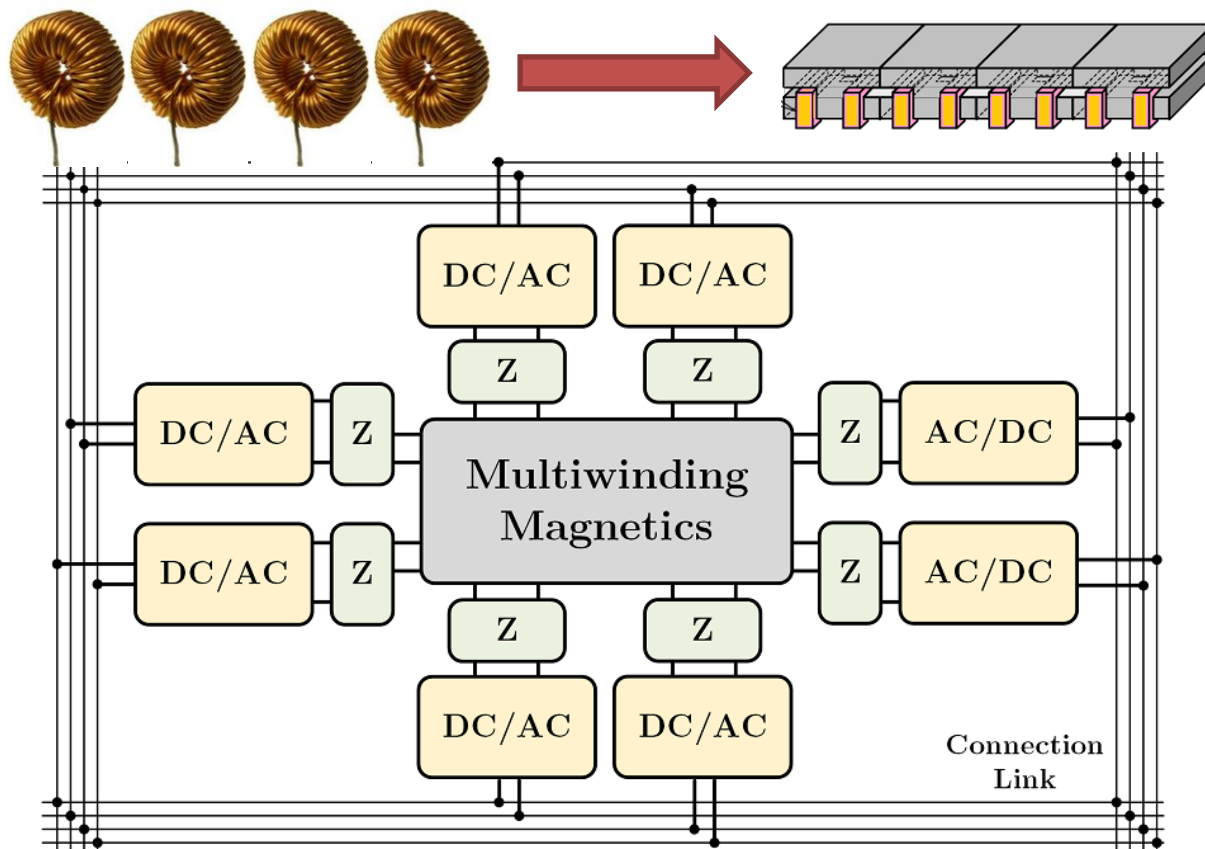
core area copper area

$$P = VI \propto \epsilon^4$$

↑
scaling factor

- Capacitors win in **energy / power density**
- Magnetic components win in **functionality / flexibility**
- Larger magnetics offer higher power density
- **Small & multifunctional magnetics** → high frequency & multiwinding

The “integrated magnetic” concept is not new...



before 1970s

Coupled inductor buck

1990s

Multiphase buck

2000s

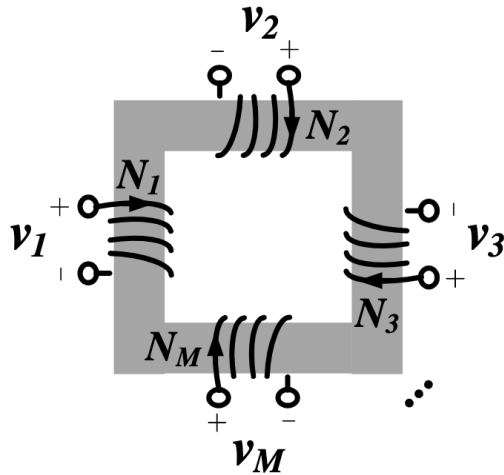
Isolated dc-dc

2010s

Solid state xformer

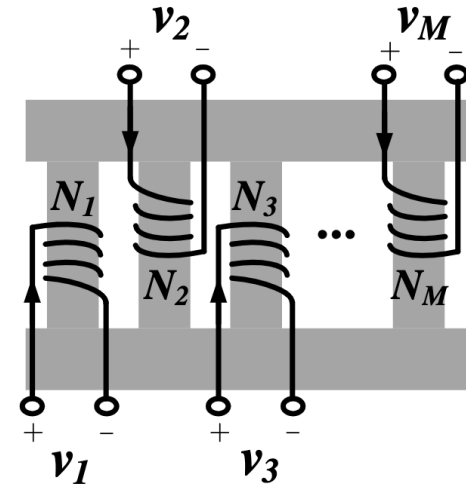
Need design methods and tools for “integrated” magnetics at HF

Series Coupled Structure
single flux multi linkage

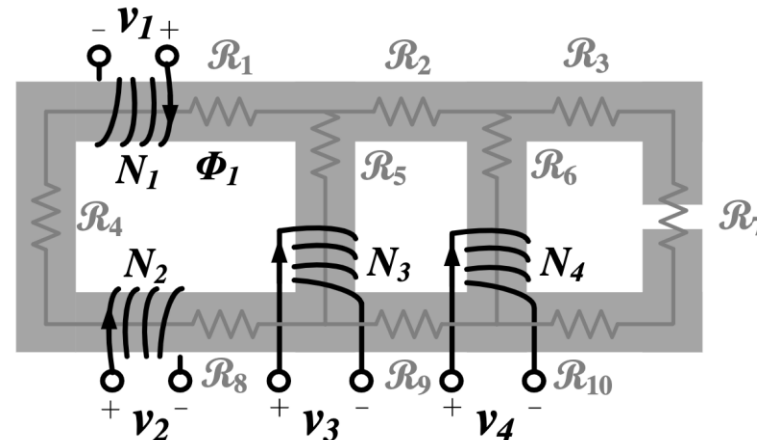


Parallel Coupled Structure
multi flux single linkage

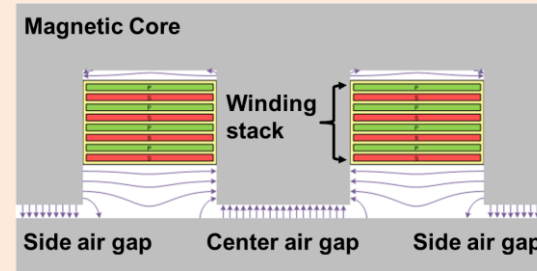
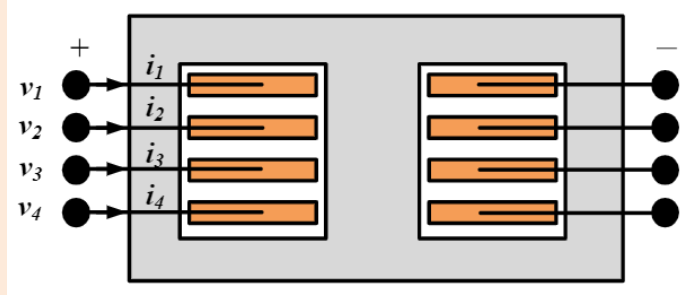
Geometrical Dual



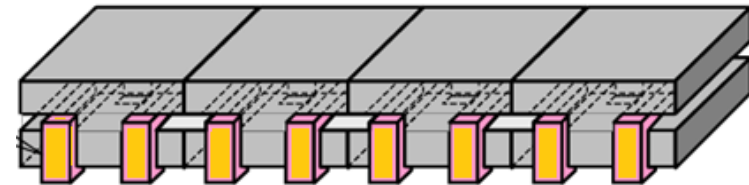
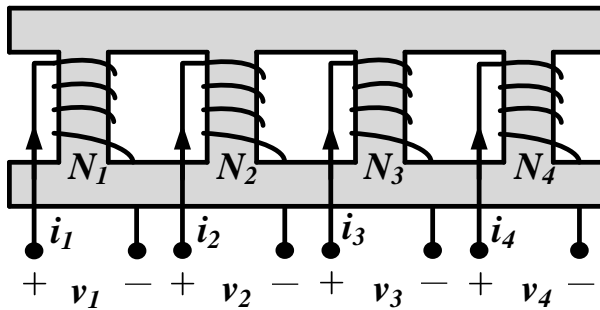
All multiwinding magnetics are combinations of series and parallel coupled structures



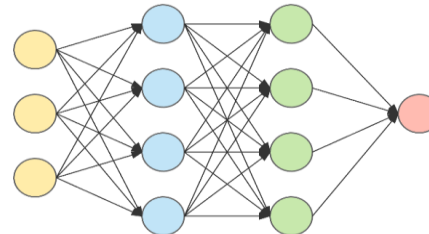
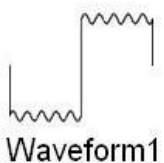
□ Design methodologies for series coupled structure (planar core)



□ Design methodologies for parallel coupled structure (ladder core)



□ Machine learning based magnetic core loss modeling methods



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1. What is the optimal way to interleave many layers?



Alternating interleave



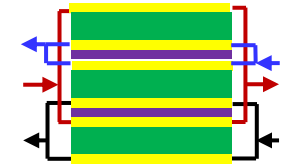
1 & 3 as primary
2 & 4 as secondary

Symmetric interleave



1 & 4 as primary
2 & 3 as secondary

More complicated?



.....?

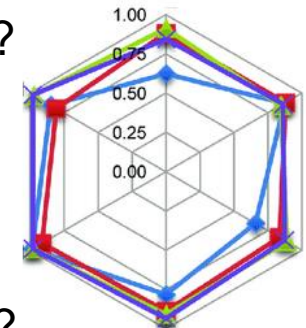
2. What are the optimal winding stack and winding spacing?

Thin Middle Spacing Thick Middle Spacing



3. Multi-object optimization space

- 1) Interleaving options?
- 2) Materials?
- 3) Geometry?
- 4) Size?
- 5) Efficiency?
- 6) Coupling coefficient?



Every model starts from assumptions ...

(1) MQS assumption

- Assume $\frac{\partial E}{\partial t} = 0$.
- Applicable when the wavelength is much longer than the device size (usually lower than ~100 MHz).

Magneto-Quasi-Static Maxwell's equations

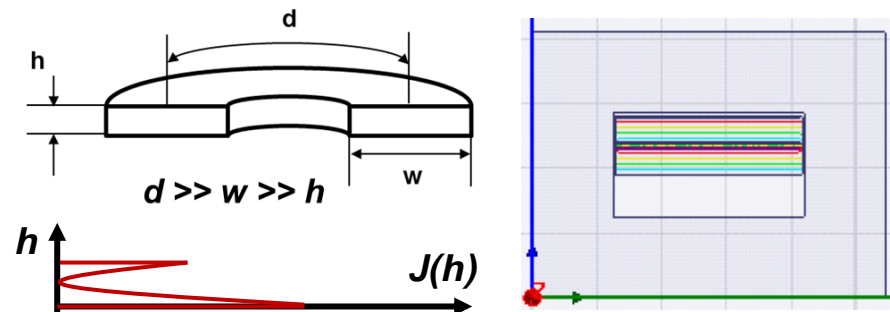
$$\left\{ \begin{array}{l} \nabla E = \frac{\rho}{\epsilon_0} \\ \nabla B = 0 \\ \nabla \times E = -\frac{\partial B}{\partial t} \\ \nabla \times B = \mu_0(J + \epsilon_0 \frac{\partial E}{\partial t}) \end{array} \right.$$

Ignore the time evolution of the electric field

(2) 1-D assumption

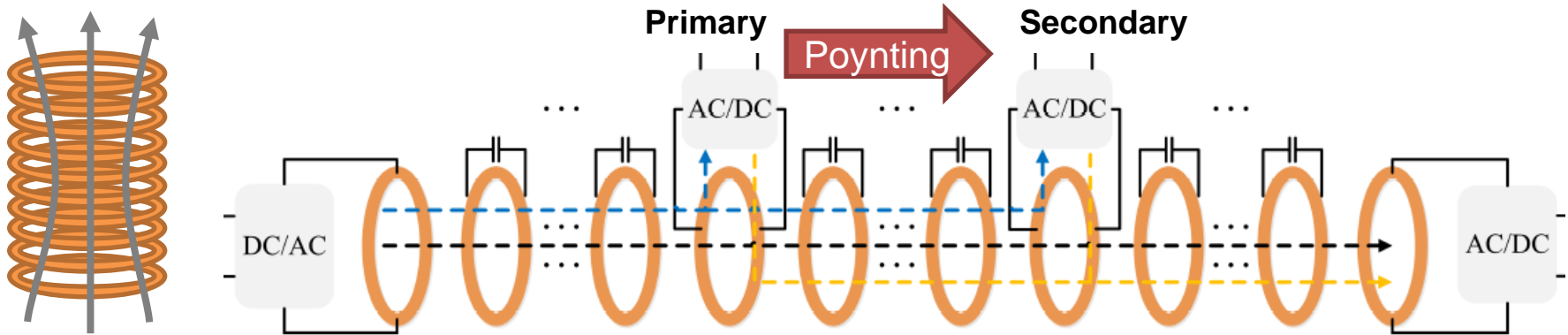
- Fields vary only along the thickness direction.
- Applicable when the flux is guided by the magnetic core.

Magnetic core guides the flux

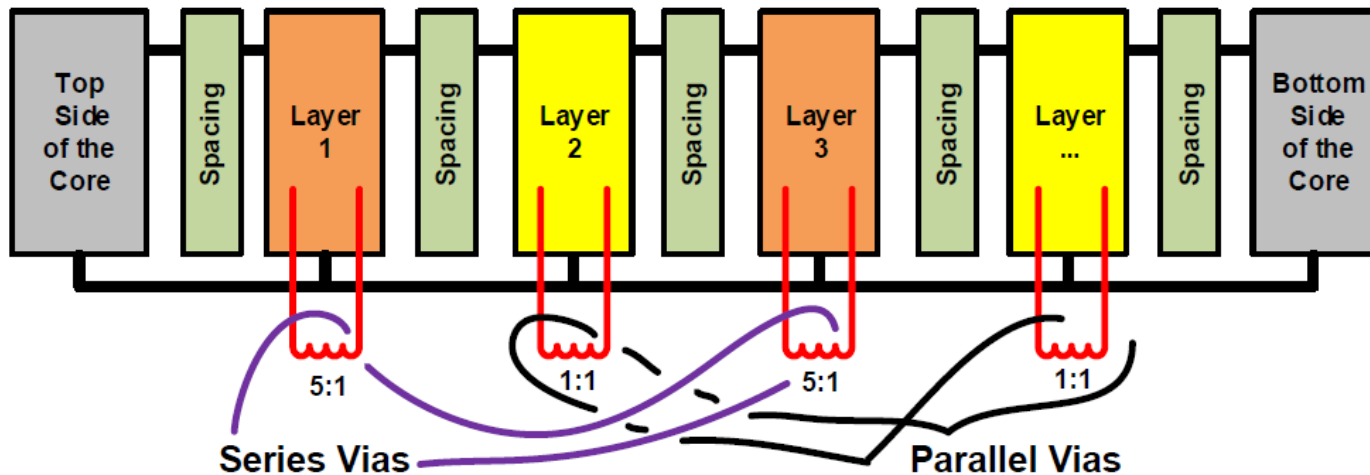


Skin and proximity effects change current distribution

□ 1-D energy wave propagation method (Poynting vector)



□ Modular lumped circuit models for repeating building blocks



Field diffusion equations:

$$H_X(z) = \frac{H_T \sinh(\Psi z) + H_B \sinh(\Psi(h - z))}{\sinh(\Psi h)}$$

Ampere's law:

$$\nabla \times H = J = \sigma E \quad \Psi = \frac{1+j}{\delta} \quad \delta = \sqrt{\frac{2}{\mu\omega\sigma}}$$

E field as a function of H and K:

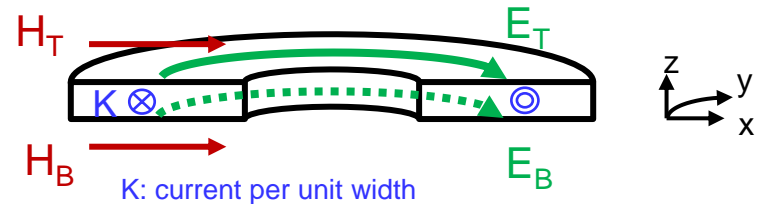
$$\begin{cases} E_T = E_Y(h) = \frac{\Psi}{\sigma} \left(\frac{H_T e^{\Psi h} - H_B}{e^{\Psi h} - e^{-\Psi h}} - \frac{H_B - H_T e^{-\Psi h}}{e^{\Psi h} - e^{-\Psi h}} \right) & Z_a = \frac{\Psi(1 - e^{-\Psi h})}{\sigma(1 + e^{-\Psi h})} \\ E_B = E_Y(0) = \frac{\Psi}{\sigma} \left(\frac{H_T - H_B e^{-\Psi h}}{e^{\Psi h} - e^{-\Psi h}} - \frac{H_B e^{\Psi h} - H_T}{e^{\Psi h} - e^{-\Psi h}} \right) & Z_b = \frac{2\Psi e^{-\Psi h}}{\sigma(1 - e^{-2\Psi h})} \end{cases}$$

KVL/KCL relationships:

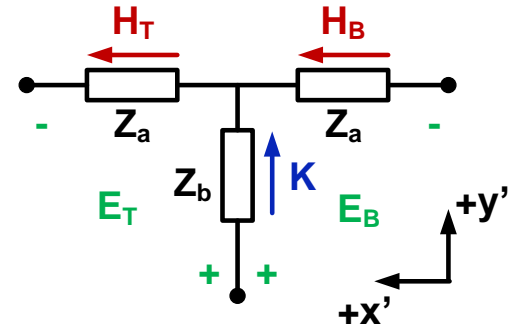
V/m Ω A/m

$$\begin{cases} E_T = Z_a H_T + Z_b K & \text{KVL} \\ E_B = Z_b K - Z_a H_B & \text{KVL} \\ K = H_T - H_B & \text{KCL} \end{cases}$$

Electromagnetic Fields



Modular Layer Model



H & K : through variables ~ unit (A/m)
 E : across variable ~ unit (V/m)
 Z_a, Z_b : impedances ~ unit (Ω)

Intuition:

- Two three-terminal networks
- Connected by the H field between them

Faraday's Law and Field Continuity

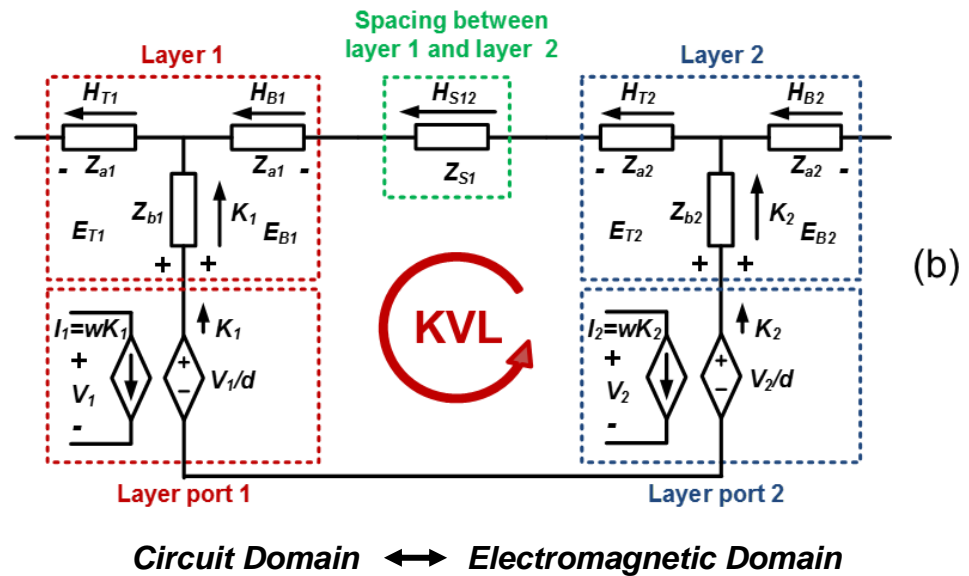
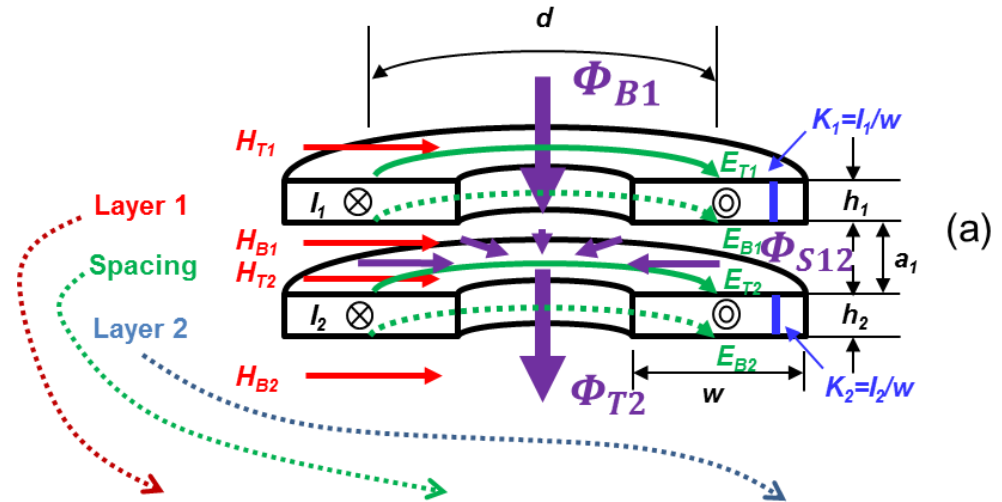
$$E_{B1}d - V_1 = -\frac{d\Phi_{B1}}{dt} \quad E_{T2}d - V_2 = -\frac{d\Phi_{T2}}{dt}$$

$$\frac{d\Phi_{T2}}{dt} = \frac{d\Phi_{B1}}{dt} + \frac{d\Phi_A}{dt}$$

Flux Linking Two Layers:

An additional KVL equation

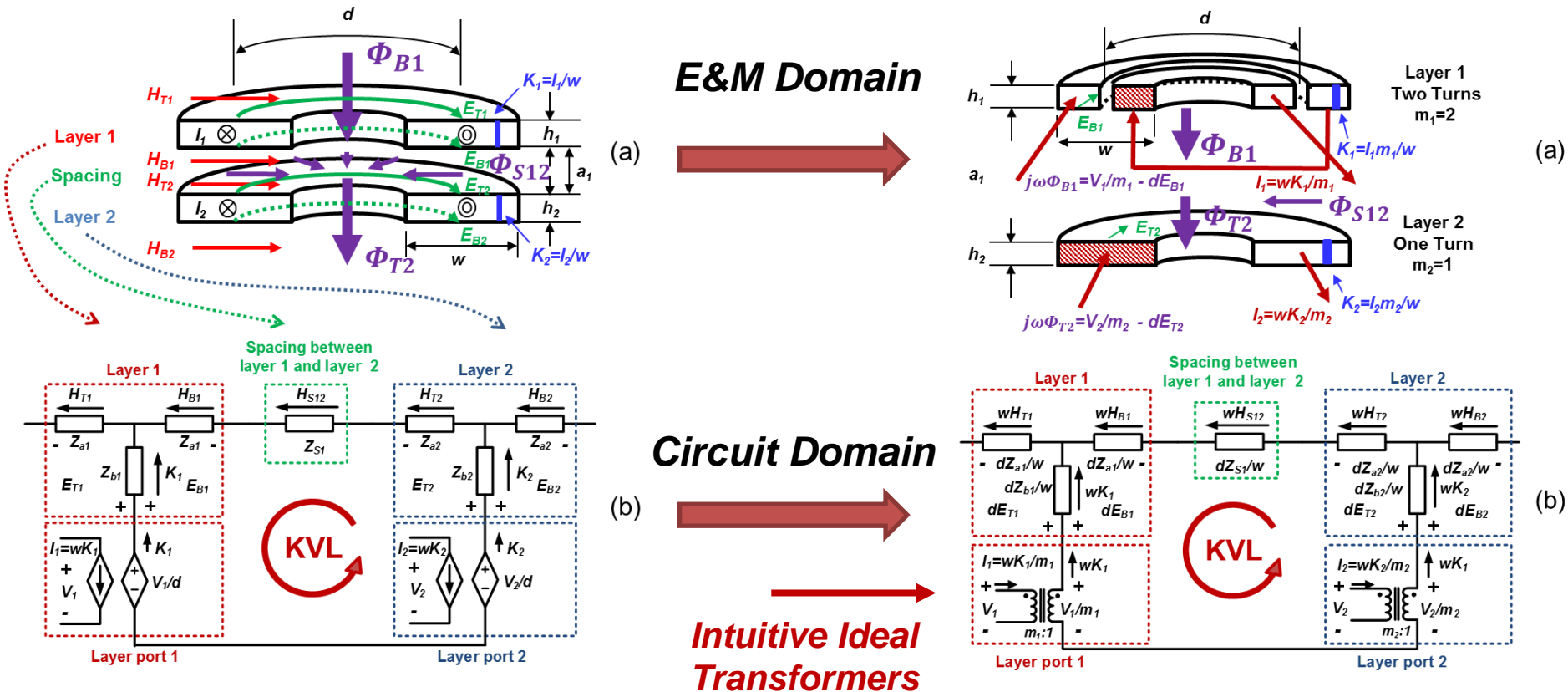
$$\underbrace{j\omega\mu_0 a_1}_{\Omega} \underbrace{H_{S12}}_{A/m} = \underbrace{\frac{V_2}{d} - E_{T2} - \frac{V_1}{d} + E_{B1}}_{V/m}$$



Circuit Domain ↔ Electromagnetic Domain

Fields distributions in multiple-turns layers are linearly related to those in single-turn layers

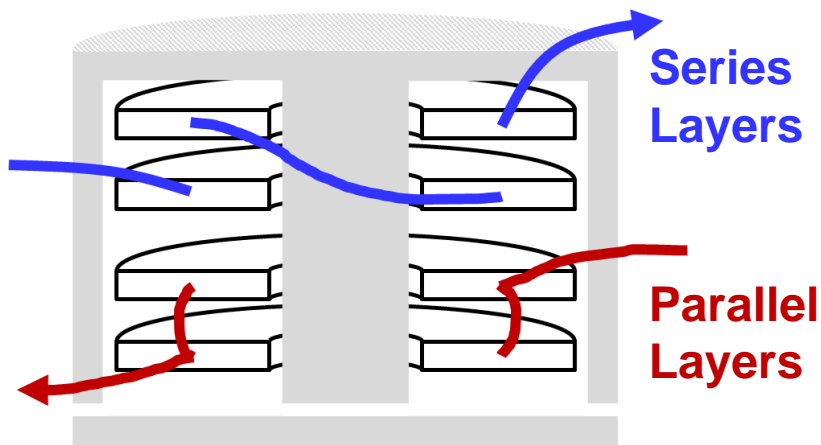
Multiple turns \rightarrow Additional Linear Conversions



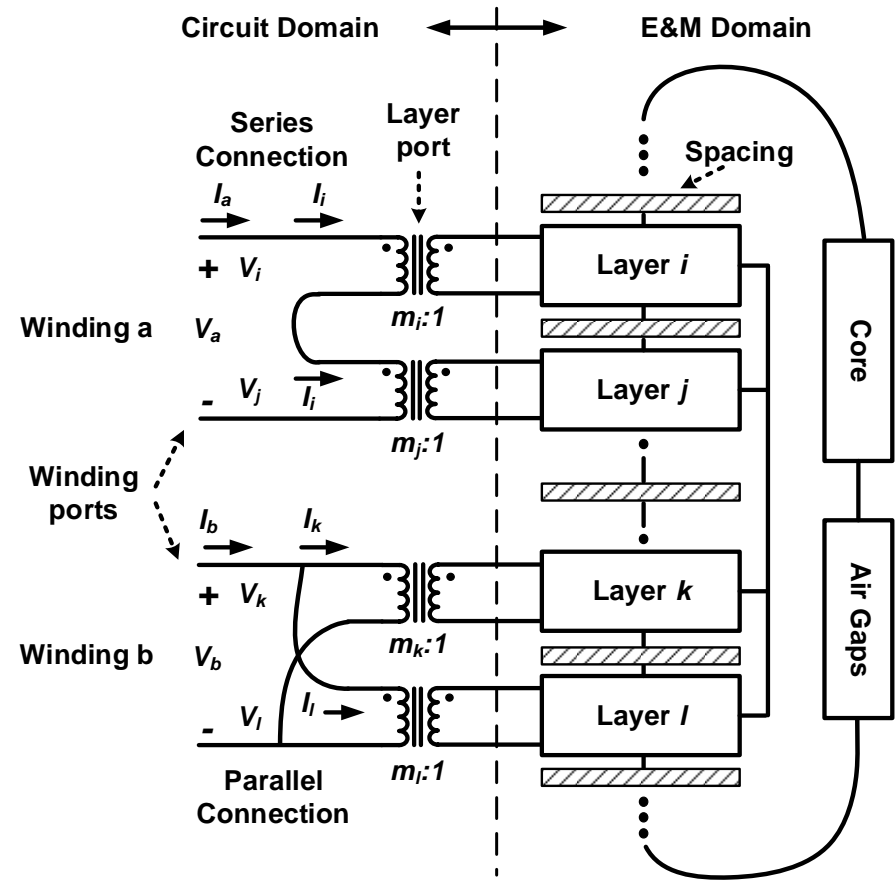
Modeling vias is equivalent to adding KVL, KCL constraints:

Layer i and Layer j in series
 Layer k and Layer l in parallel

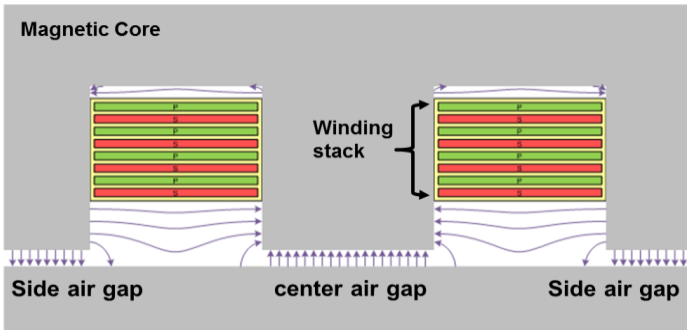
$$\begin{cases} V_i + V_j = V_a \\ V_k = V_l = V_b \end{cases} \quad \begin{cases} I_i = I_j = I_a \\ I_k + I_l = I_b \end{cases}$$



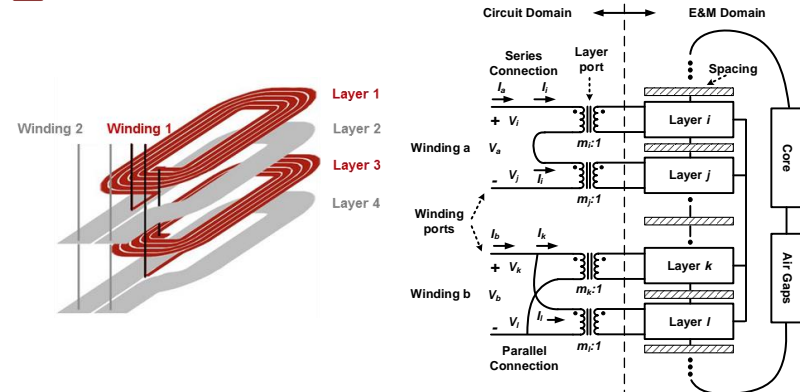
Connect the layer ports in the same pattern as they are in the real circuit



1 Geometry Information

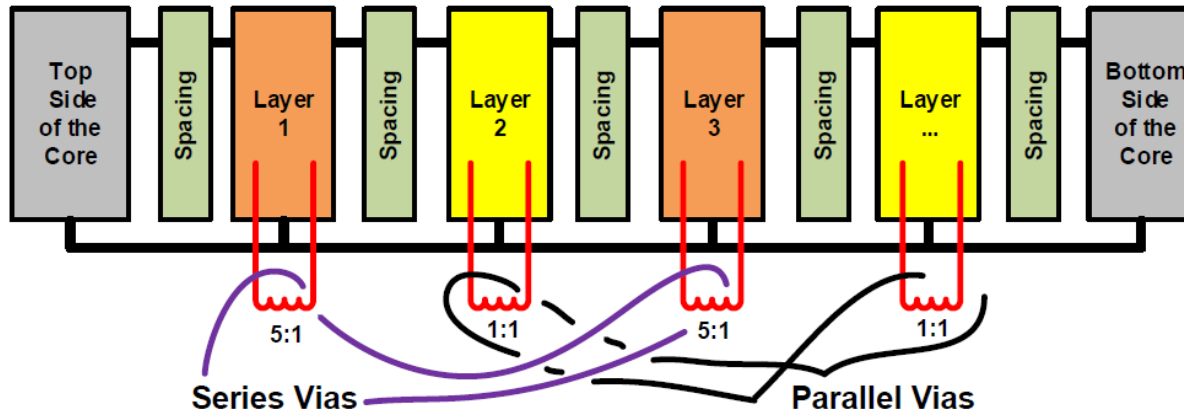


3 SPICE Netlist



2

Modular Layer Model

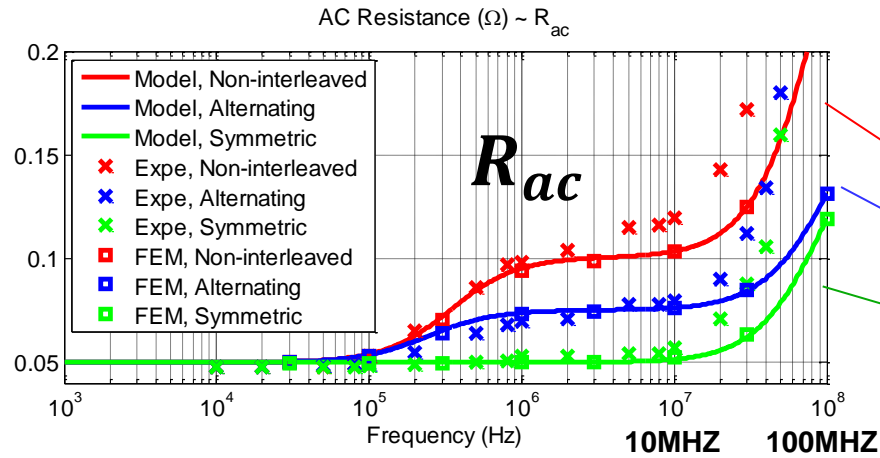
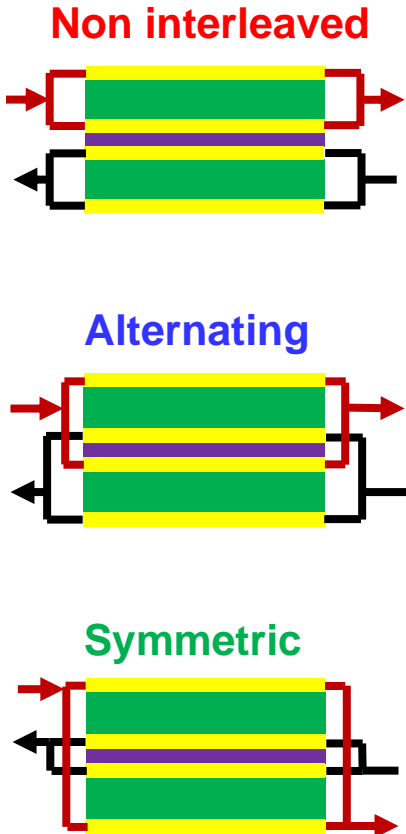


Simulations!



Search: M2SPICE

Comparing the P_{ac} and E_{ac} of three 1:1 transformers with three different interleaving patterns

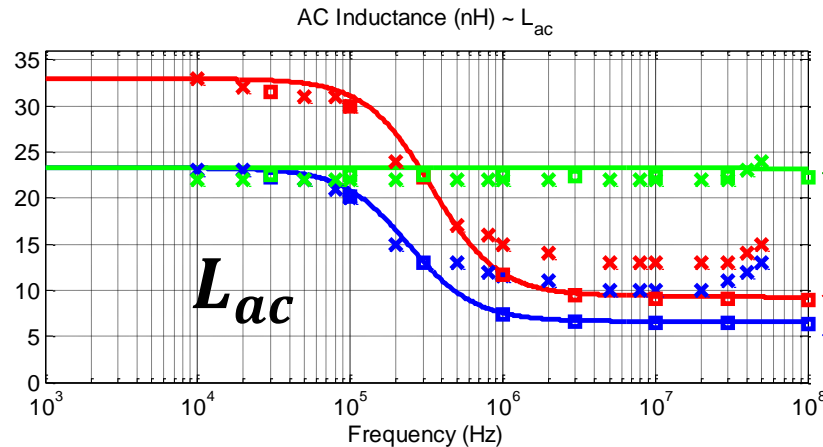


$$P_{ac} = \sum I^2 R_{ac}$$

Non Interleaved

Alternating

Symmetric



$$E_{ac} = \frac{1}{2} \sum I^2 L_{ac}$$

Symmetric

Non interleaved

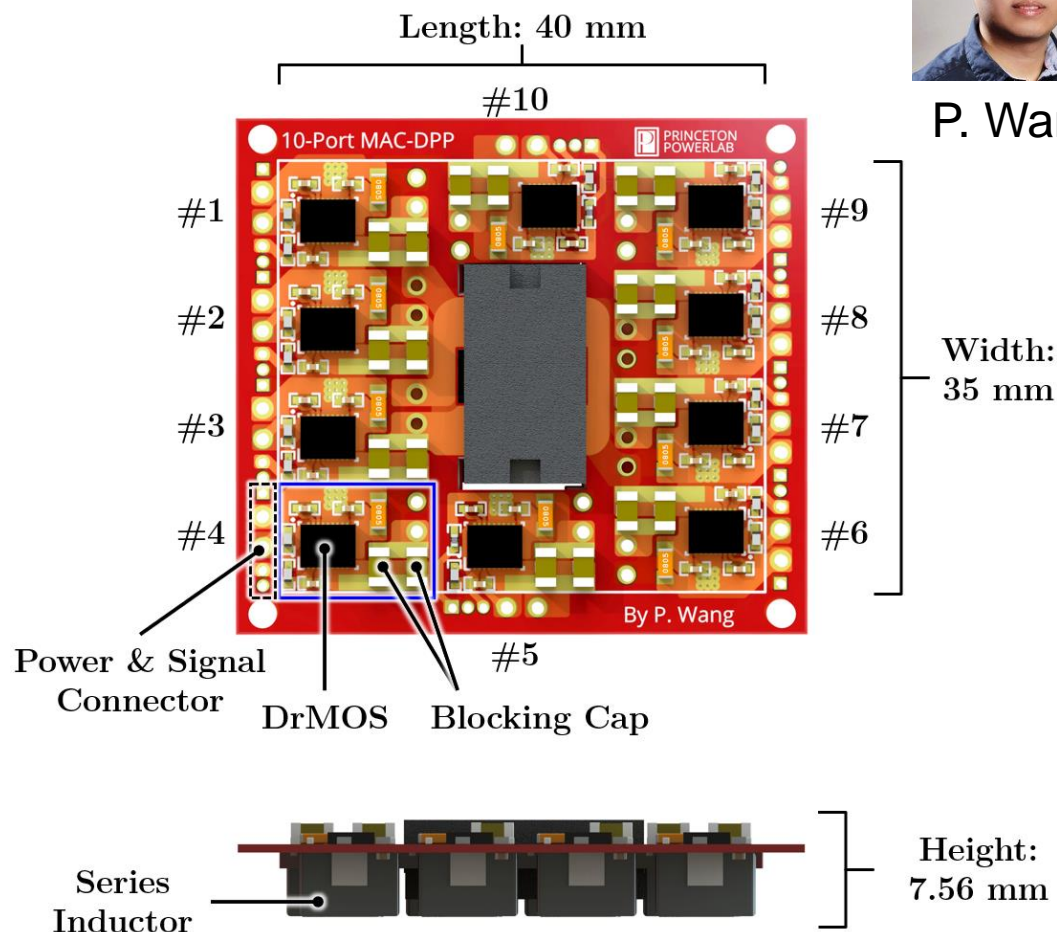
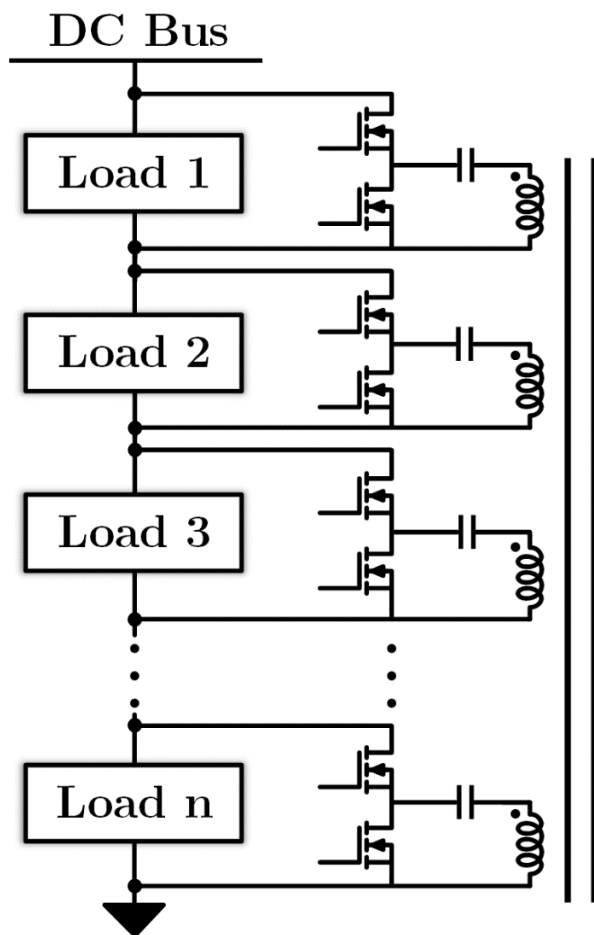
Alternating

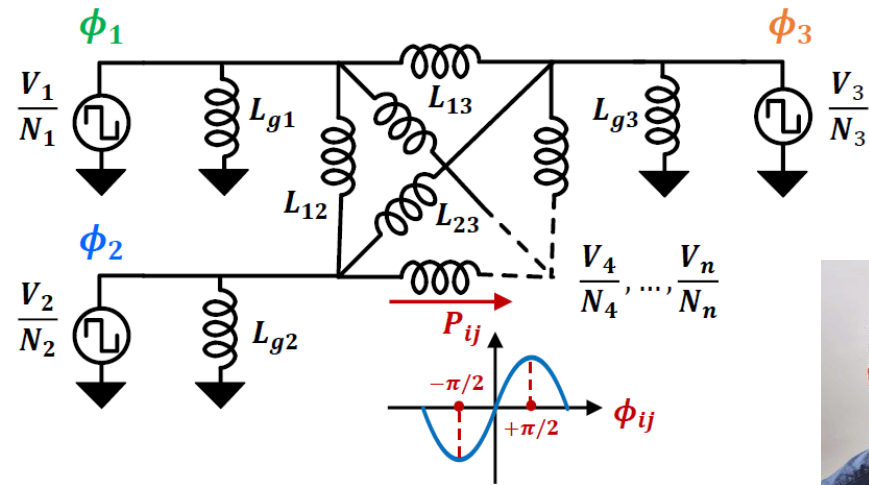
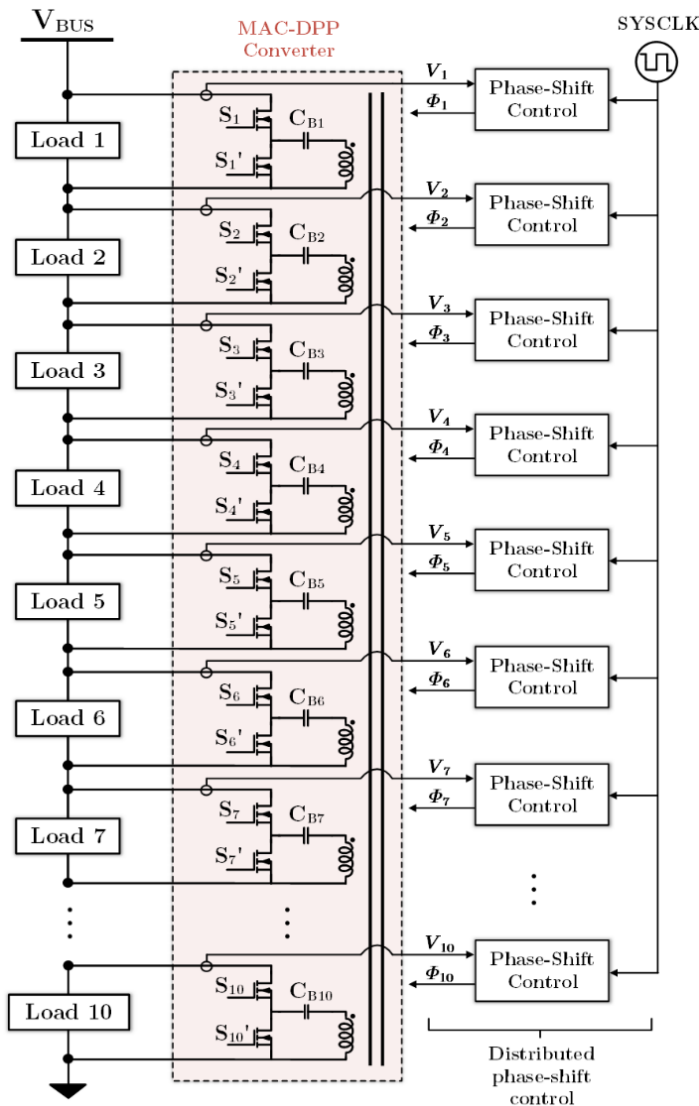
Interleaving has to be done in the right way !!!

Distributed Phase-Shift Modulation for MIMO Power Flow

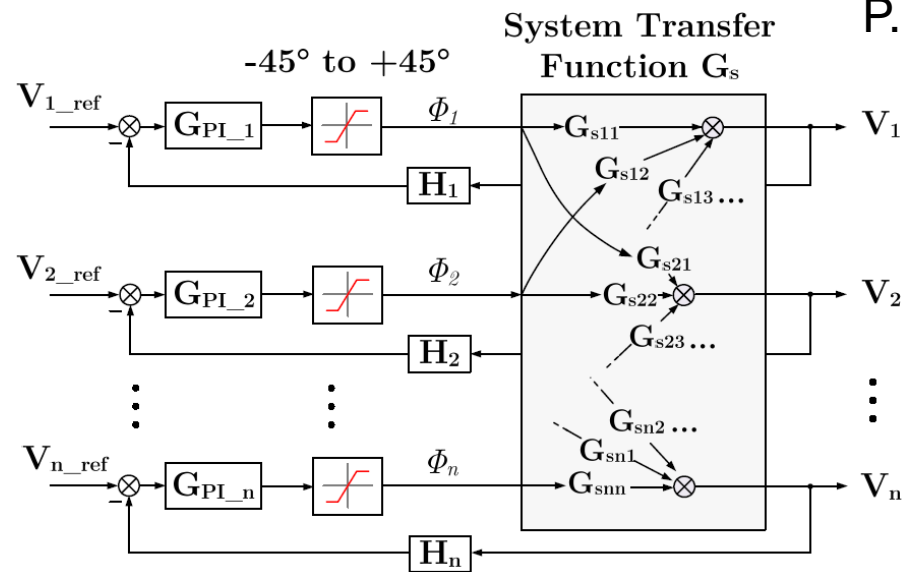


P. Wang



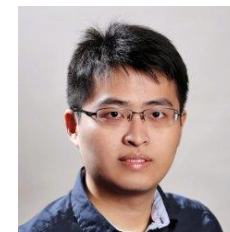
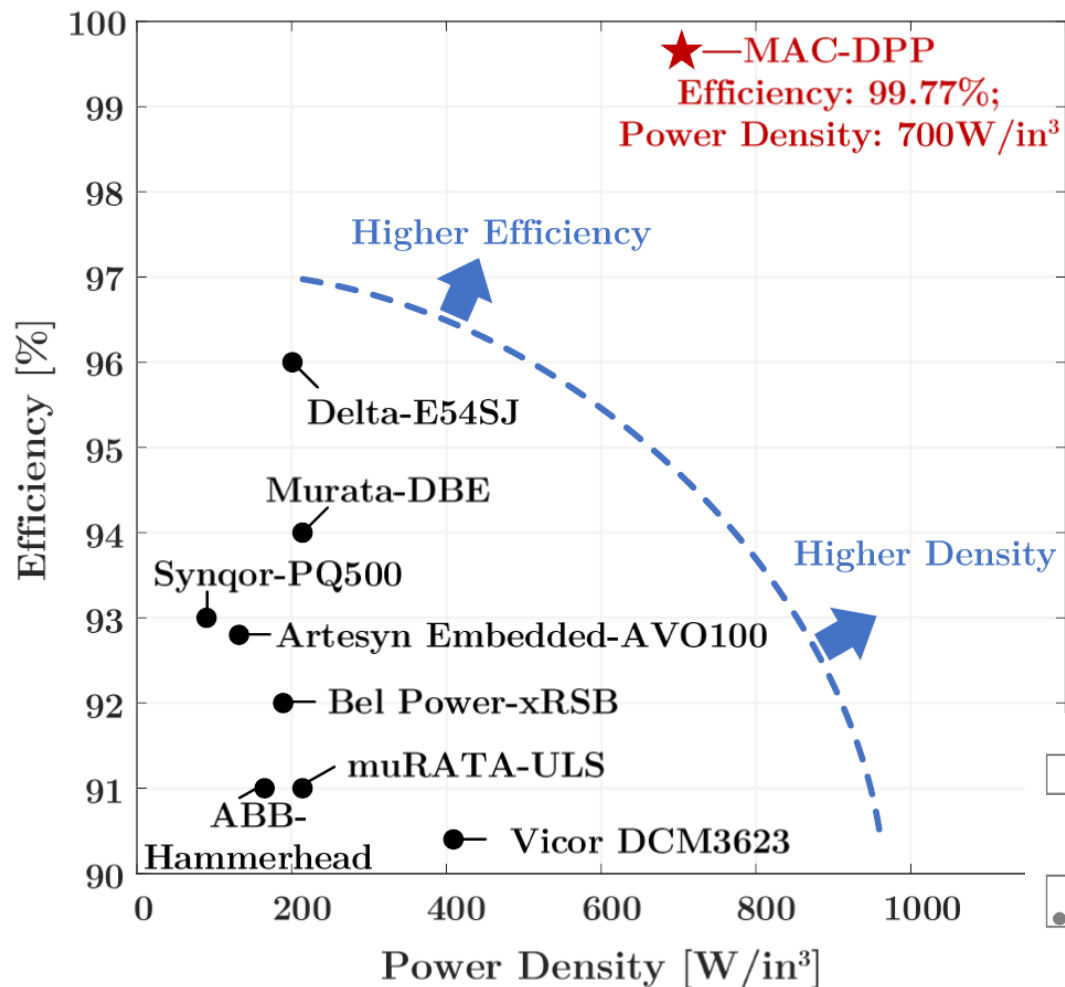


P. Wang

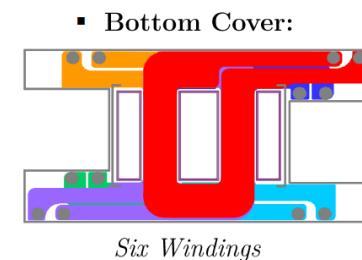
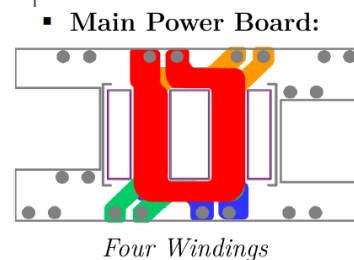
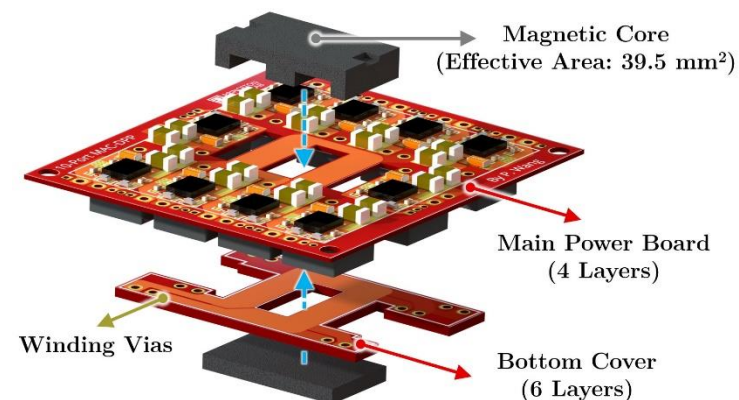


Ultra Efficient DPP System

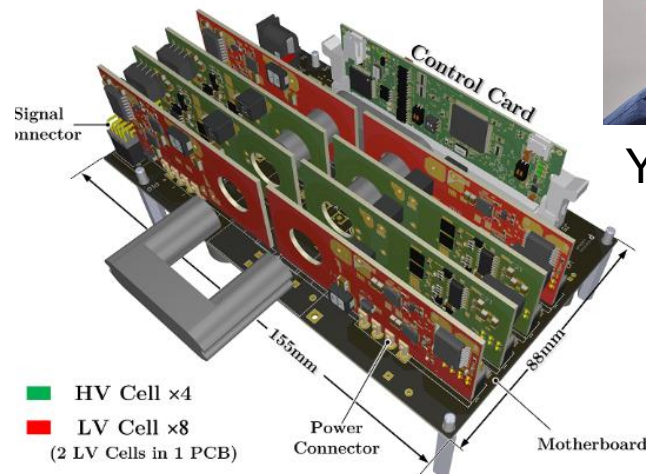
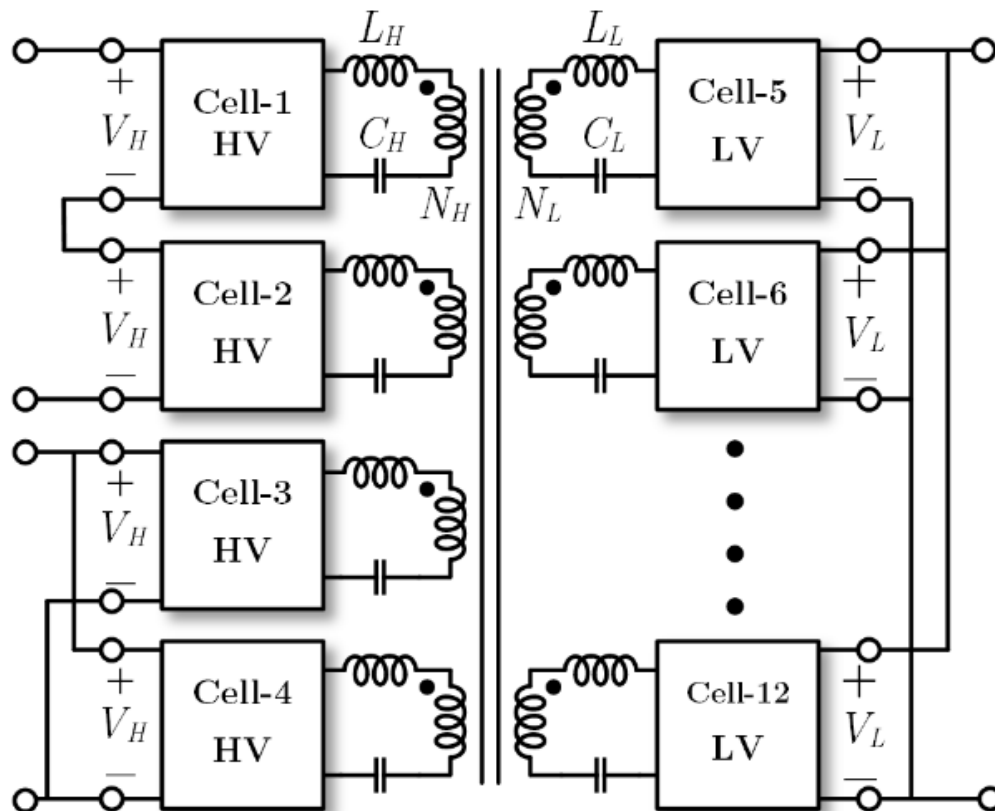
Efficiency comparison of 50 V-5 V dc-dc systems



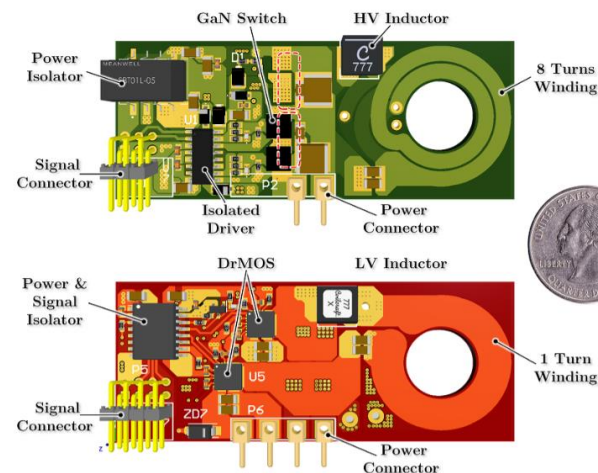
P. Wang



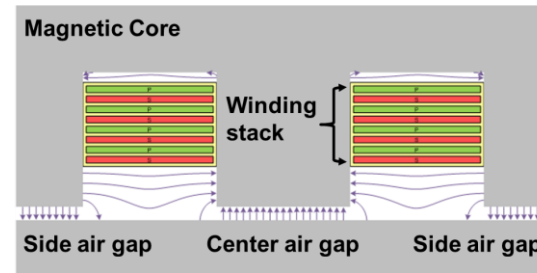
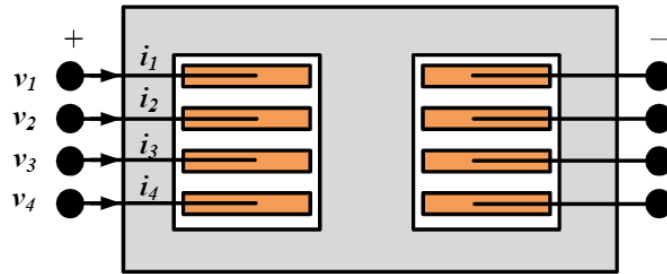
Reconfigurable MIMO Energy Router



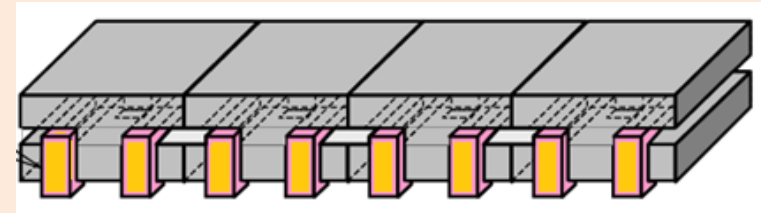
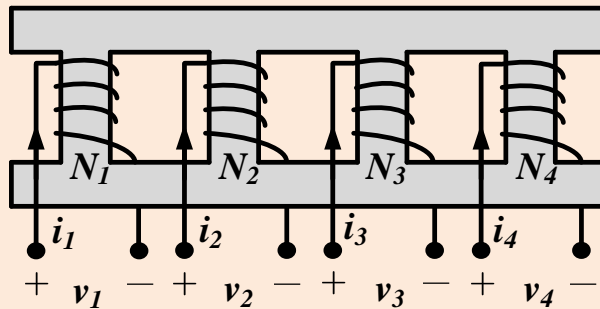
Y. Chen



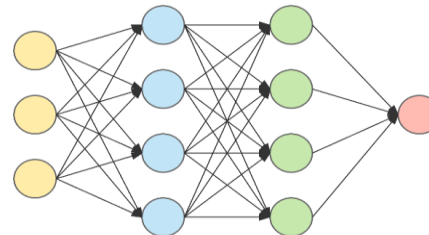
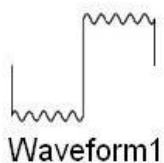
□ Design methodologies for series coupled structure (planar core)



□ Design methodologies for parallel coupled structure (ladder core)

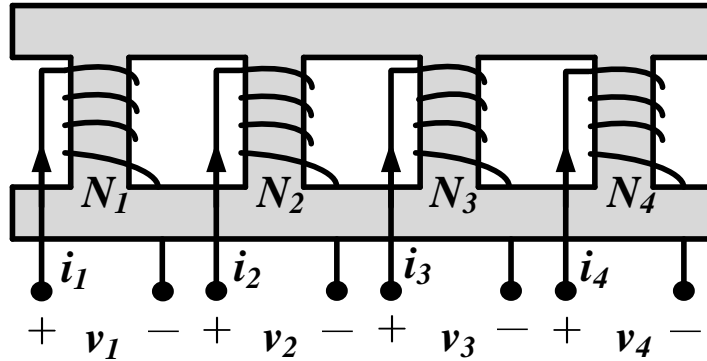


□ Machine learning based magnetic core loss modeling methods

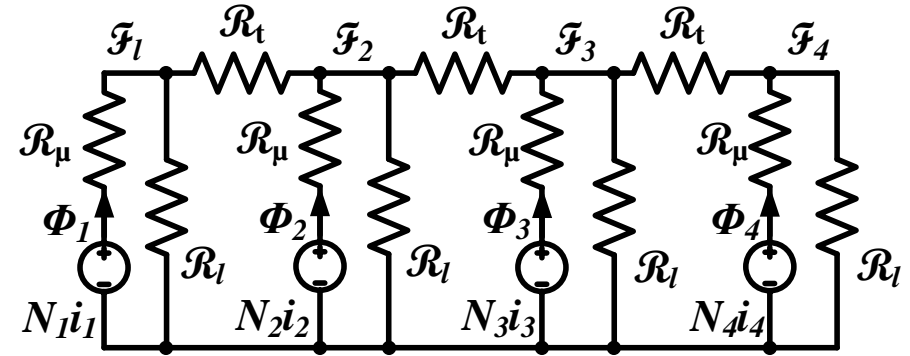


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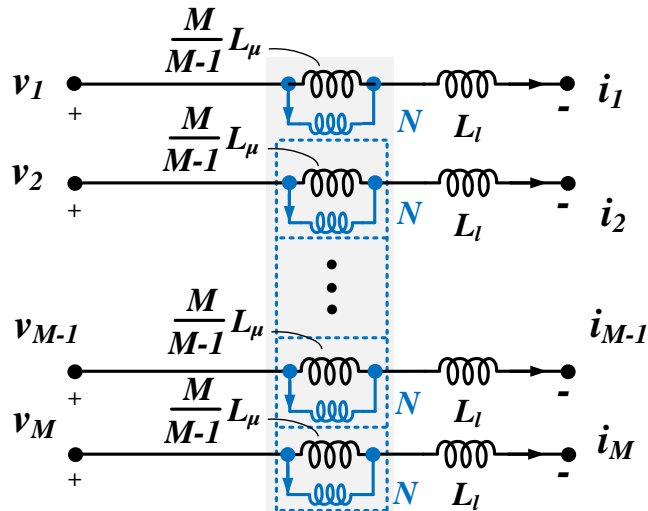
Physical Structure



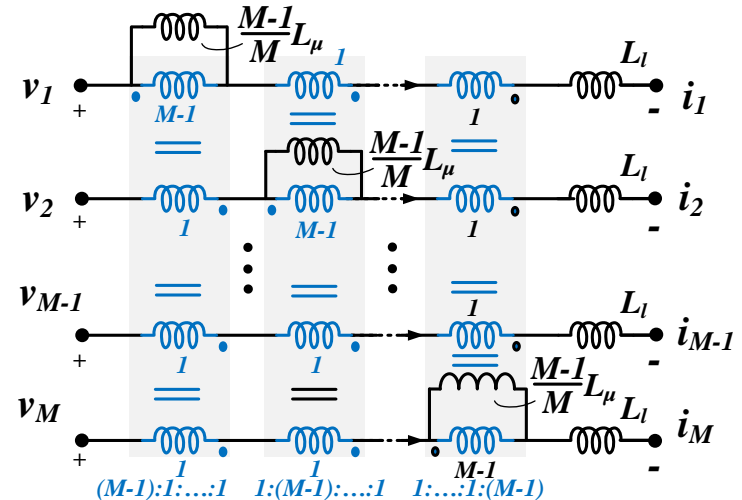
Reluctance Model



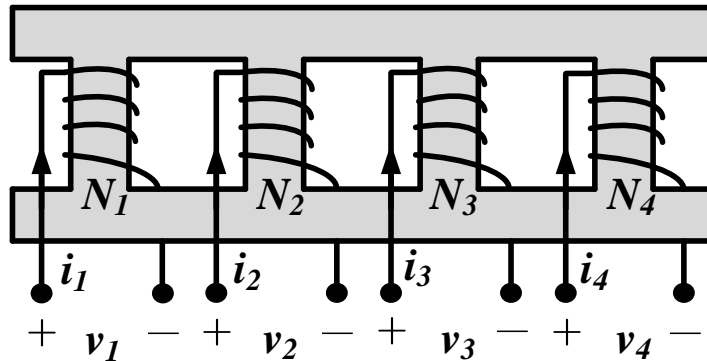
Current Equalizing Transformer Model



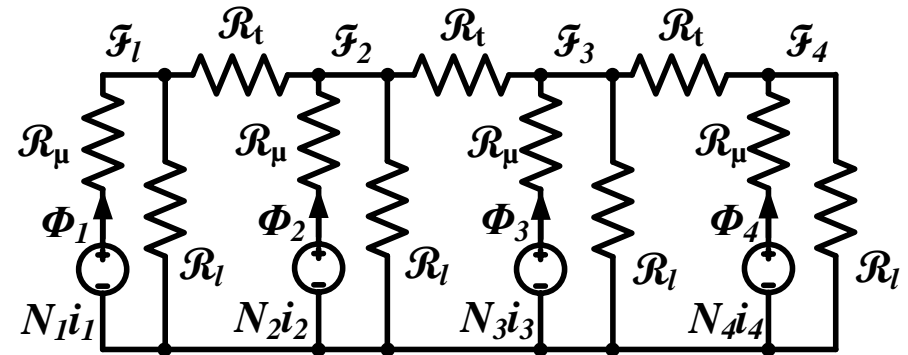
Voltage Equalizing Transformer Model



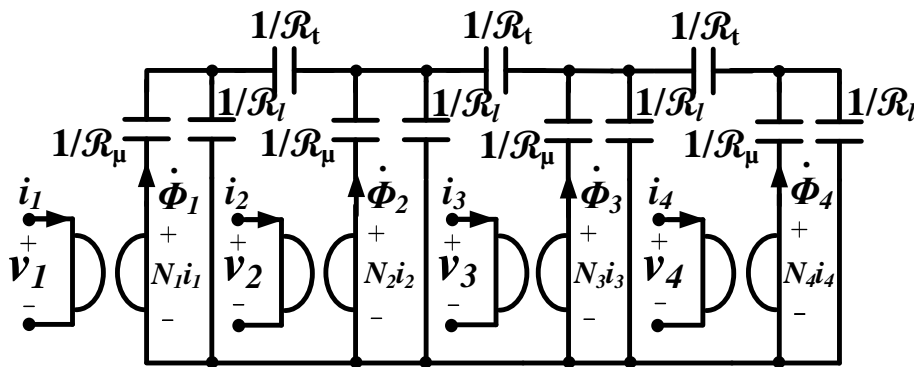
Physical Structure



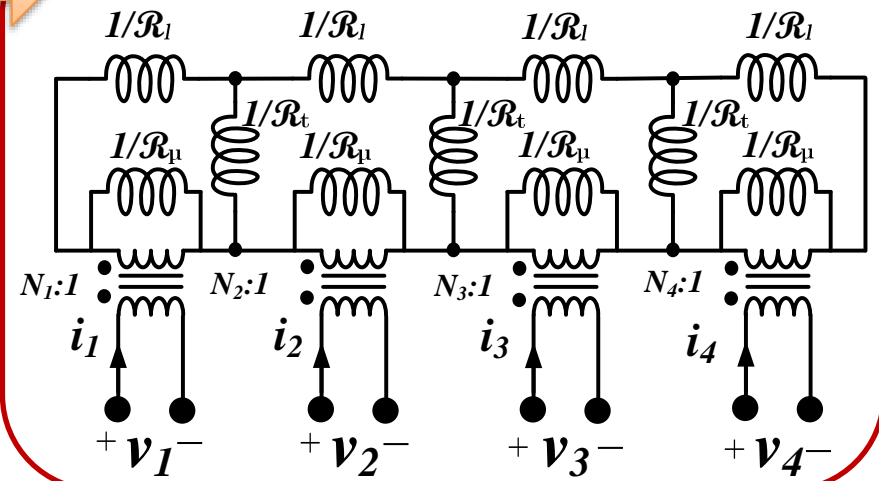
Reluctance Model



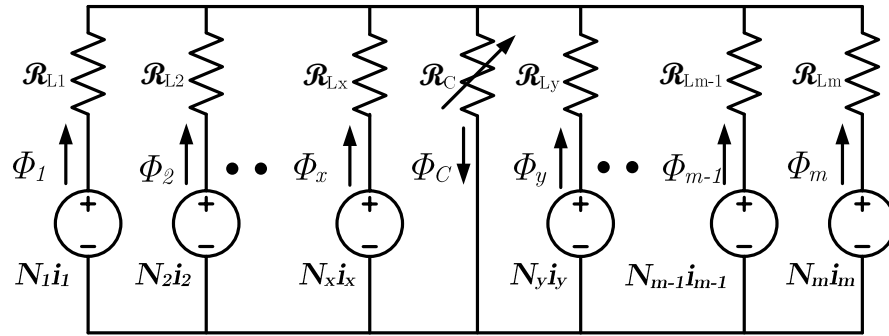
Gyrator-Capacitor Model



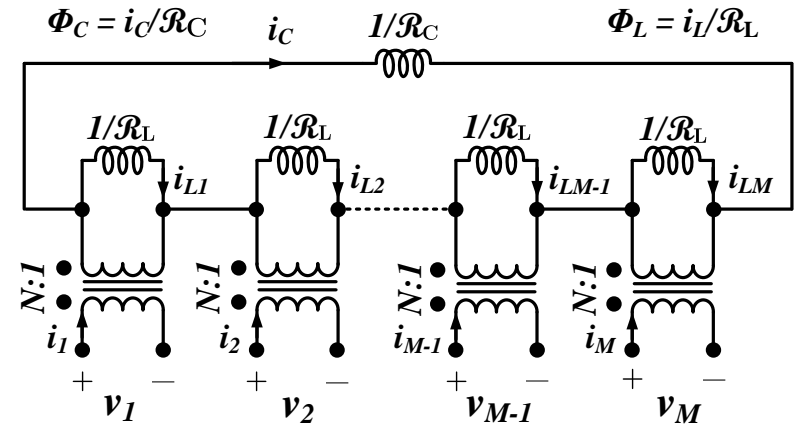
Inductance Dual Model



Reluctance Model



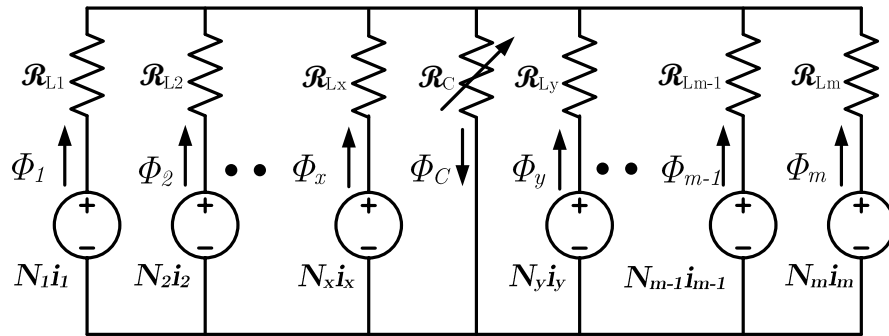
Inductance Dual Model



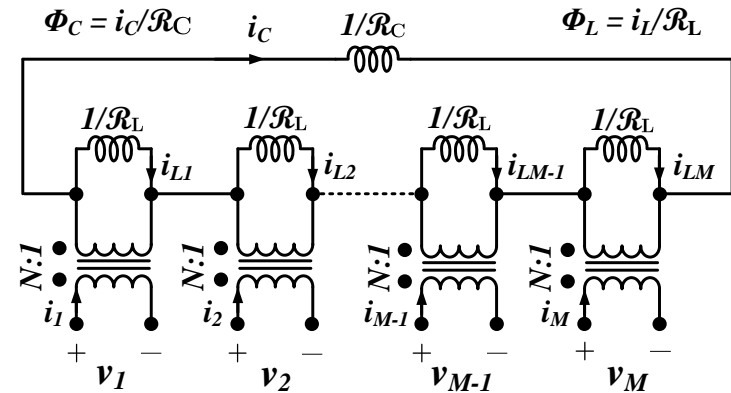
- Through variable: Flux (Φ)
- Cross variable: MMF (Ni)
- Element value: Reluctance (R)
- Energy storage: $E = \frac{1}{2} R \Phi^2$
- Power: $MMF \frac{d\Phi}{dt}$ or $R\Phi \frac{d\Phi}{dt}$

- Through variable: Current (I)
- Cross variable: Voltage (V)
- Element value: Inductance (L)
- Energy storage: $E = \frac{1}{2} LI^2$
- Power: VI

Reluctance Model



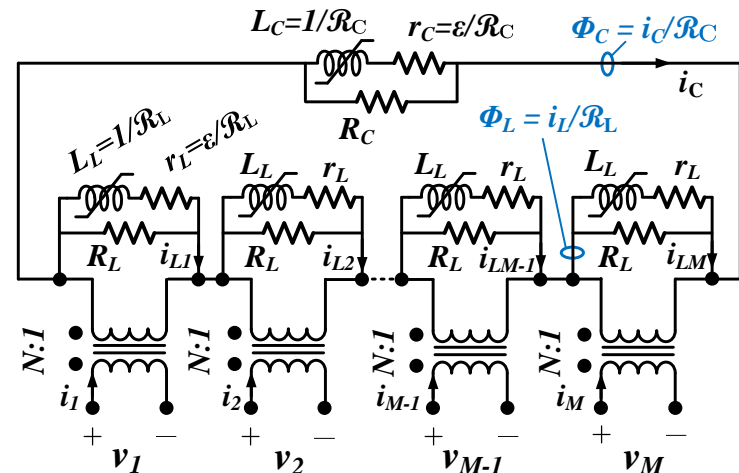
Inductance Dual Model



Advantage:

- Simple
- Intuitive
- No coupling relationships
- Explicit design equations
- Capability of capturing core loss
- Visualizing flux distribution

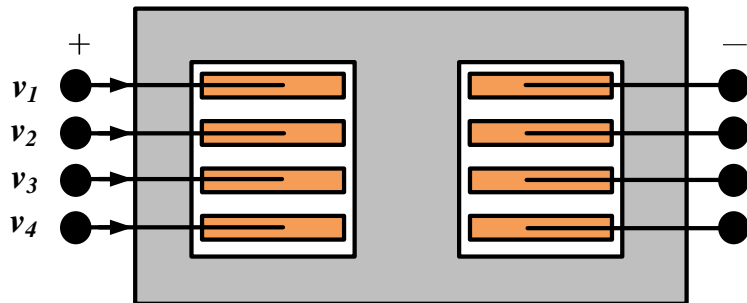
Inductance Dual Model with Core Loss



Geometrical Dual

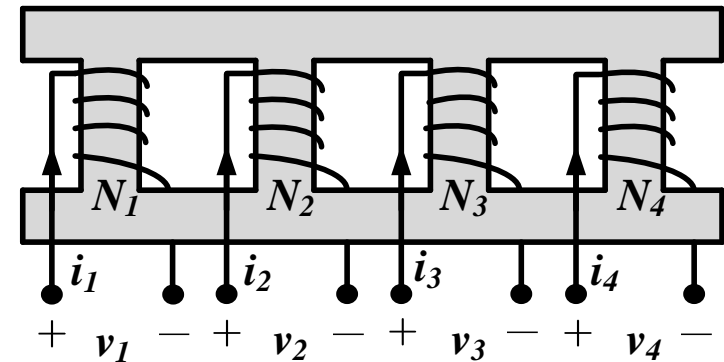
Equal Φ

Series Coupled

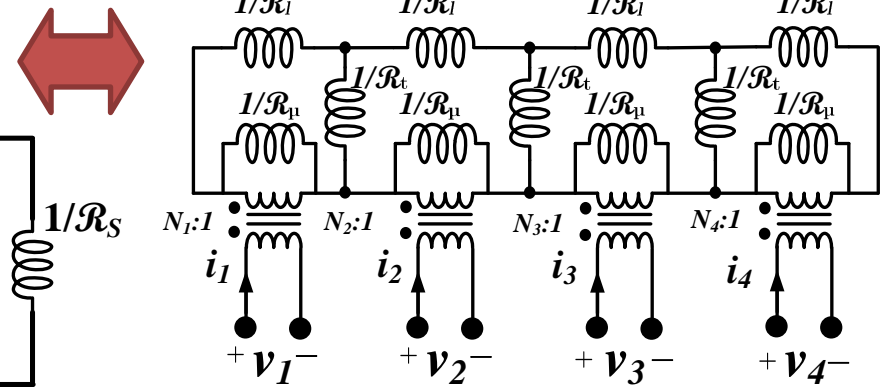
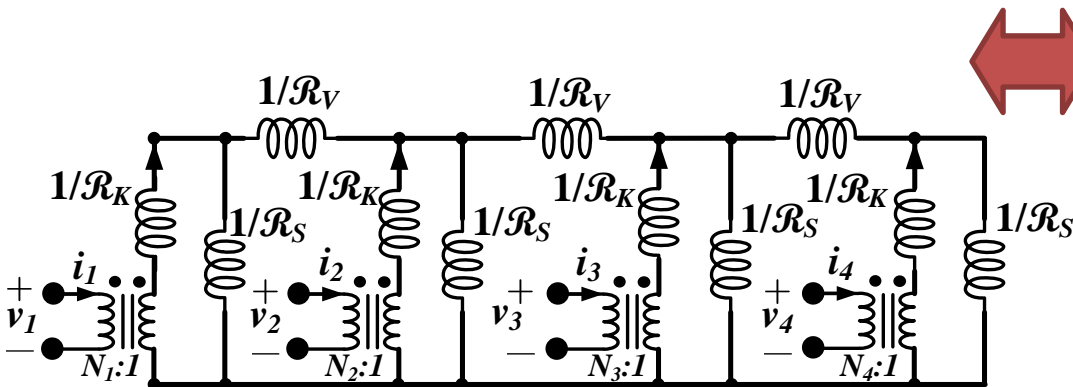


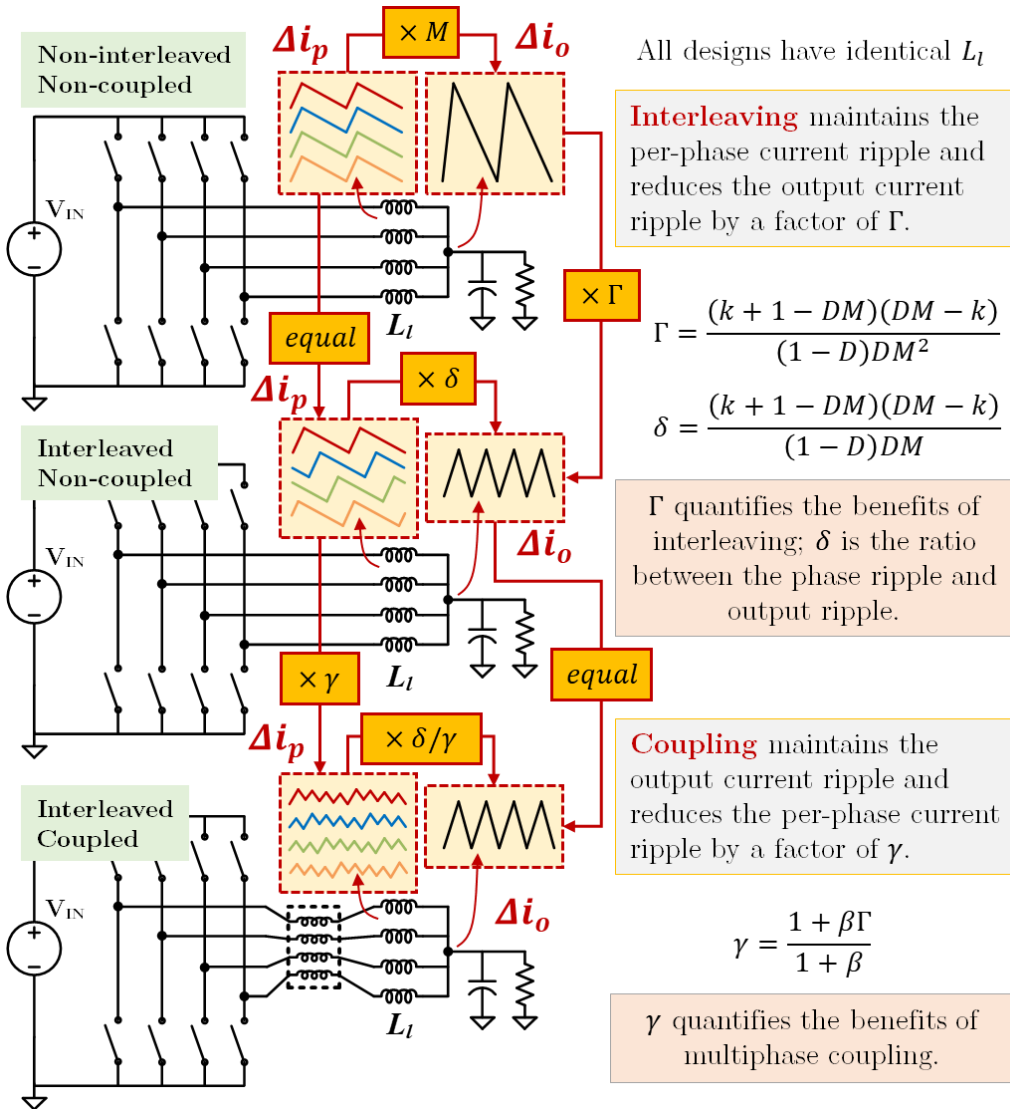
Equal MMF

Parallel Coupled



Topological Dual





Benefits of interleaving

- reduced output current ripple

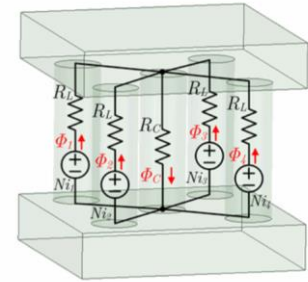
$$\Gamma = \frac{(k+1-DM)(DM-k)}{(1-D)DM^2}$$

Benefits of coupling

- reduced per-phase current ripple

$$\gamma = \frac{1+\beta\Gamma}{1+\beta}$$

$$\beta = \frac{MR_C}{R_L}$$




Clarified the relationship between multiphase coupling and multiphase interleaving!



D. Zhou C. R. Sullivan

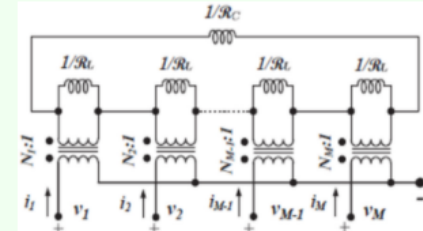
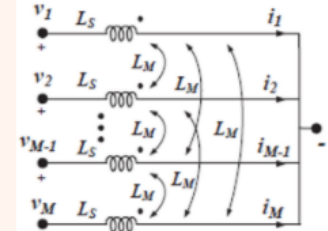
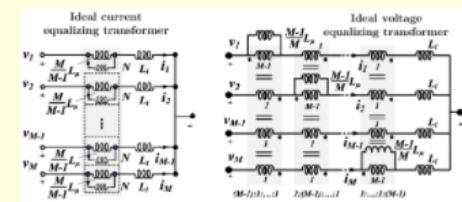
Unifies the design equations for multiphase coupled inductors for different models

<http://www.princeton.edu/~minjie/coupl/coupl.html>



Princeton Coupled Magnetics Design Tool

By Princeton Power Electronics Research Lab

Input Parameters	Duty Ratio (D)		Number of Phases (M)		Number of Turns per Winding (N)	
Derived Parameters	Interleaving Boosting Inductance ($1/\delta$)		Number of Overlapped Phases (k)		Interleaving Ripple Compression (δ)	
Method Name	Inductance Dual Model		Inductance Matrix Model		Multiwinding Transformer Model	
Design Parameters	R_L	<input type="text"/>	L_S	<input type="text"/>	L_t	<input type="text"/>
	R_C	<input type="text"/>	L_M	<input type="text"/>	L_p	<input type="text"/>
	$\beta = \frac{R_C}{R_L}$		$\alpha = \frac{L_M}{L_S}$		$\rho = \frac{L_p}{L_t}$	
Description Matrix	$N^2 \begin{bmatrix} \frac{di_1}{dt} \\ \frac{di_2}{dt} \\ \vdots \\ \frac{di_M}{dt} \end{bmatrix} = \begin{bmatrix} R_L + R_C & R_C & \dots & R_C \\ R_C & R_L + R_C & \dots & R_C \\ \vdots & \vdots & \ddots & \vdots \\ R_C & \dots & R_C & R_L + R_C \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \\ \vdots \\ v_M \end{bmatrix}$		$\begin{bmatrix} v_1 \\ v_2 \\ \vdots \\ v_M \end{bmatrix} = \begin{bmatrix} L_S & L_M & \dots & L_M \\ L_M & L_S & \dots & L_M \\ \vdots & \vdots & \ddots & \vdots \\ L_M & \dots & L_M & L_S \end{bmatrix} \begin{bmatrix} \frac{di_1}{dt} \\ \frac{di_2}{dt} \\ \vdots \\ \frac{di_M}{dt} \end{bmatrix}$		$\begin{bmatrix} v_1 \\ v_2 \\ \vdots \\ v_M \end{bmatrix} = \begin{bmatrix} L_p + L_t & \frac{1}{M-1} L_p & \dots & \frac{1}{M-1} L_p \\ \frac{1}{M-1} L_p & L_p + L_t & \dots & \frac{1}{M-1} L_p \\ \vdots & \vdots & \ddots & \vdots \\ \frac{1}{M-1} L_p & \dots & \frac{1}{M-1} L_p & L_p + L_t \end{bmatrix} \begin{bmatrix} \frac{di_1}{dt} \\ \frac{di_2}{dt} \\ \vdots \\ \frac{di_M}{dt} \end{bmatrix}$	
Lumped Circuit Model						
	R_L		$R_L = \frac{N^2}{L_S - L_M}$		$R_L = \frac{N^2(M-1)}{(M-1)L_t + ML_p}$	
	R_C		$R_C = \frac{-N^2 L_M}{(L_S - L_M)(L_S + (M-1)L_M)}$		$R_C = \frac{-N^2 L_p}{L_t((M-1)L_t + ML_p)}$	

High Voltage Conversion Ratio

- 48 V: 1 V is the future standard

High Output Current

- Approaching 1000 A

Fast Transient Response

- Over 5 A/ns

Extreme Power Density

- >100 A/cm²

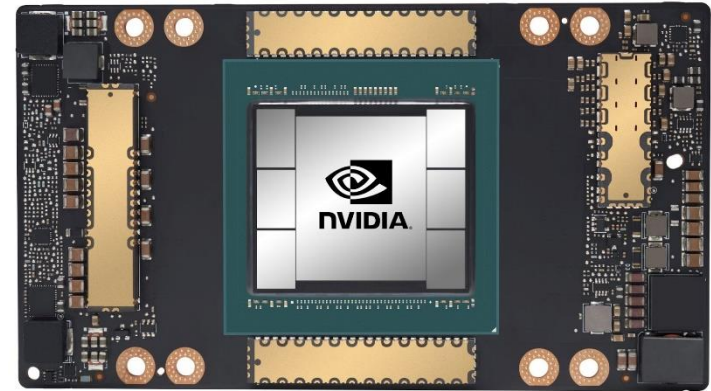
Extreme Efficiency Target

- >95% peak; >80% full load

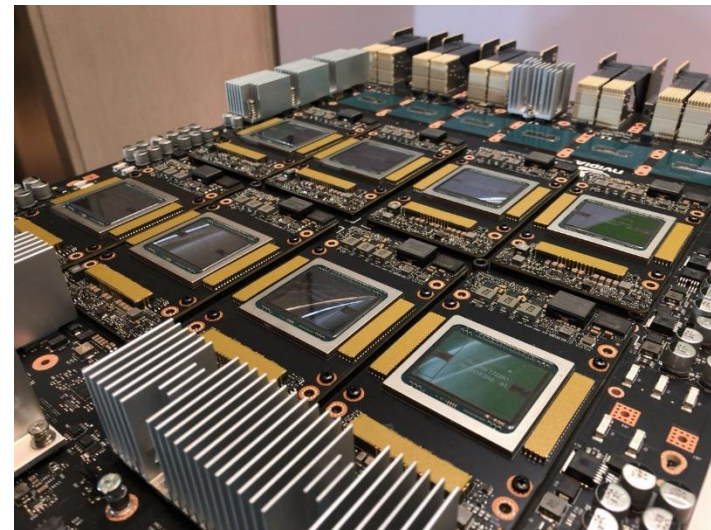
Collaborators



- J. Baek, M. Chen et al., "LEGO-PoL: A 48V-1.5V 300A Merged-Two-Stage Hybrid Converter for Ultra-High-Current Microprocessors," *APEC 2020*.

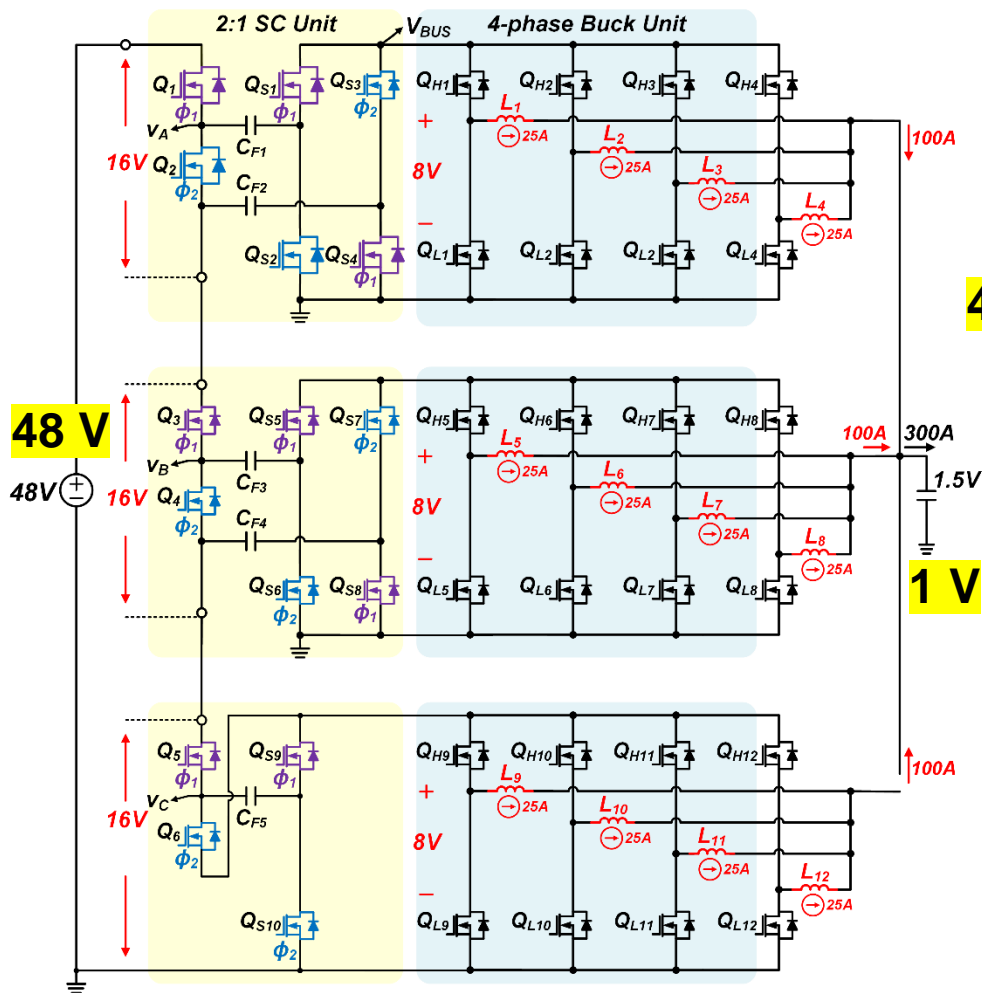


Nvidia Tesla A100



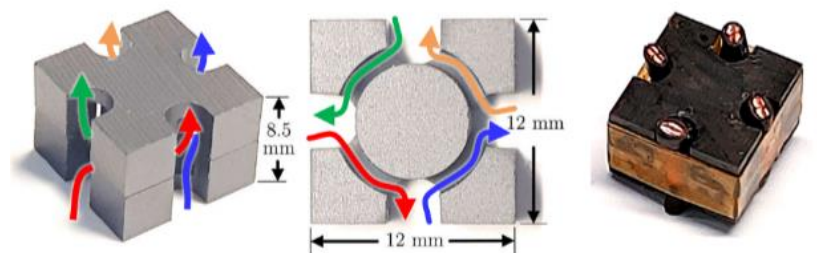
Nvidia A100 AI Server

LEGO-PoL Architecture

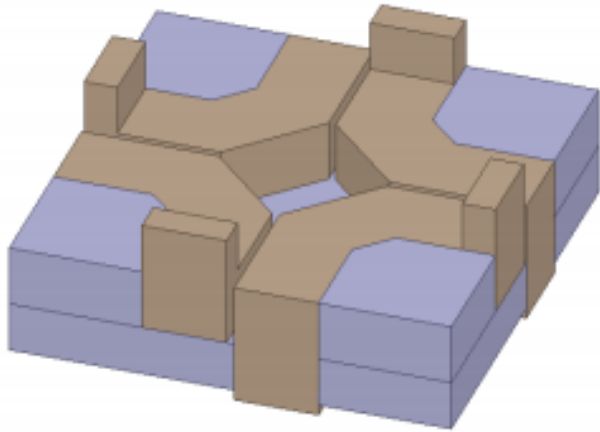


1 V
↑
48 V

1 V

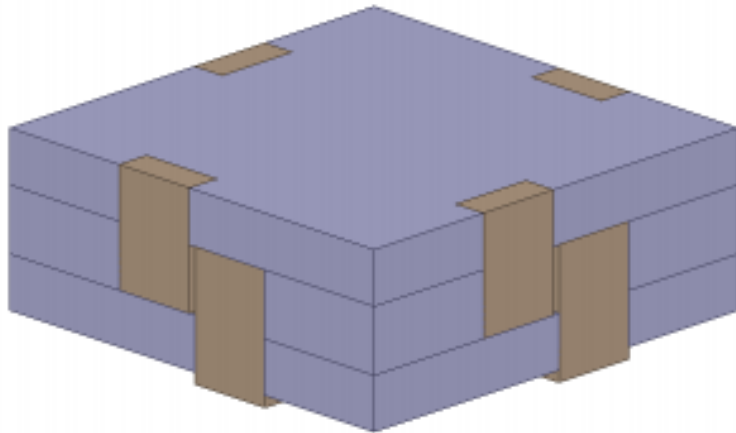


Four-Phase Coupled Magnetics (250 A)



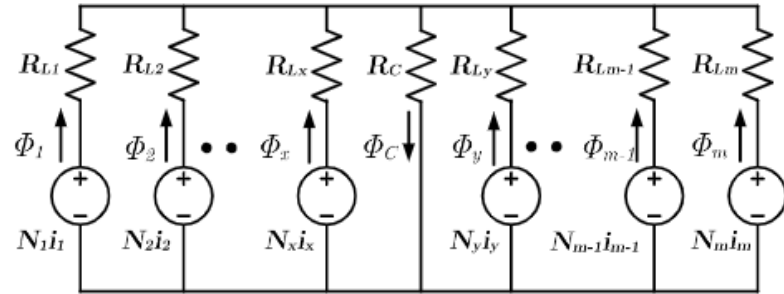
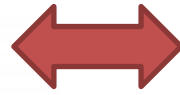
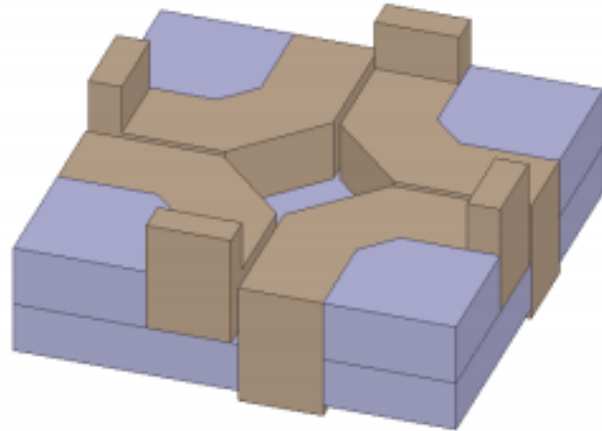
Sophisticated design space

- Side leg area
- Center leg area
- Winding area
- Plate thickness
- 2D layout
- 3D structure



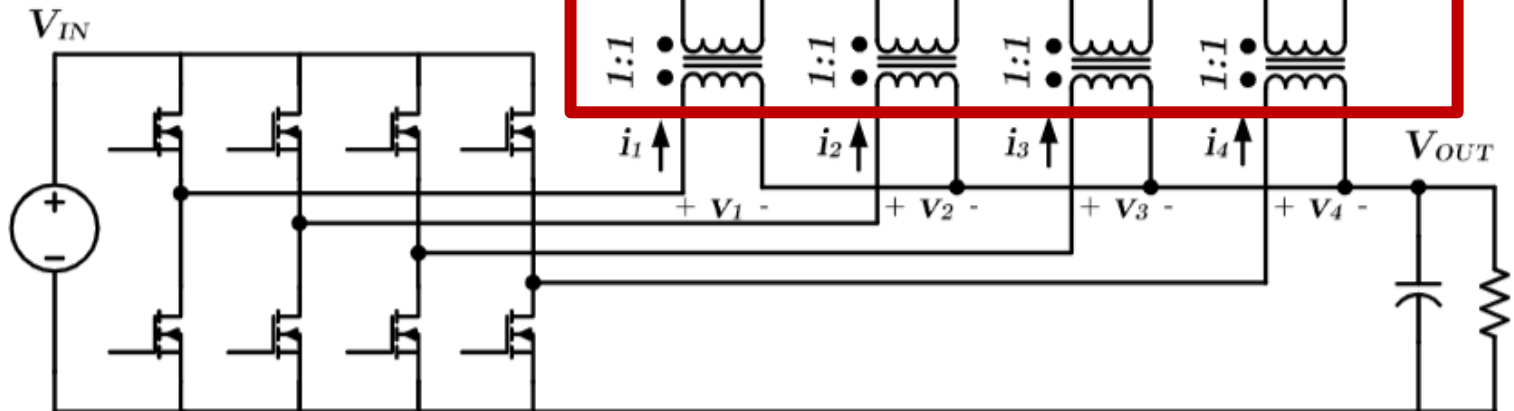
Optimization targets

- Smallest leakage inductance
- Largest magnetizing inductance
- Lowest loss
- Smallest size
- Sufficient saturation margin



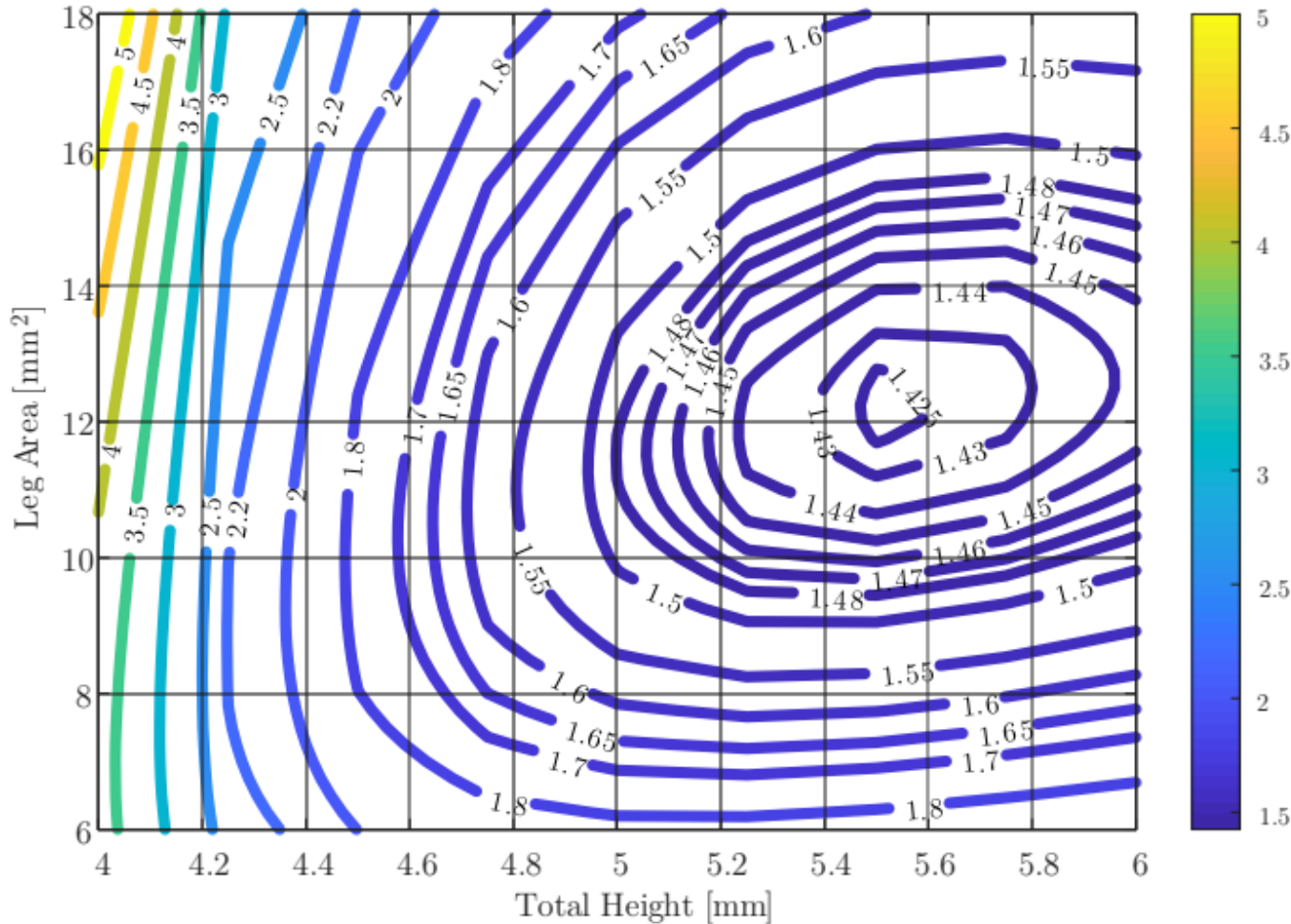
Topological duality

Multileg Coupled Magnetics



Vertical Magnetics Optimization

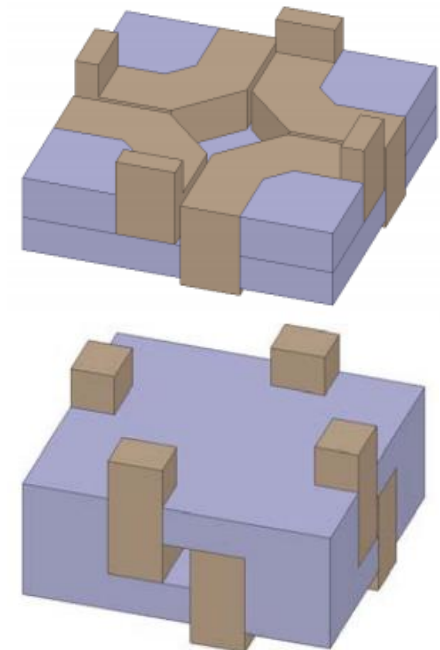
Min Loss: 1.4231W at $h=5.5\text{mm}$, $A_{\text{leg}}=12.25\text{mm}^2$



J. Baek



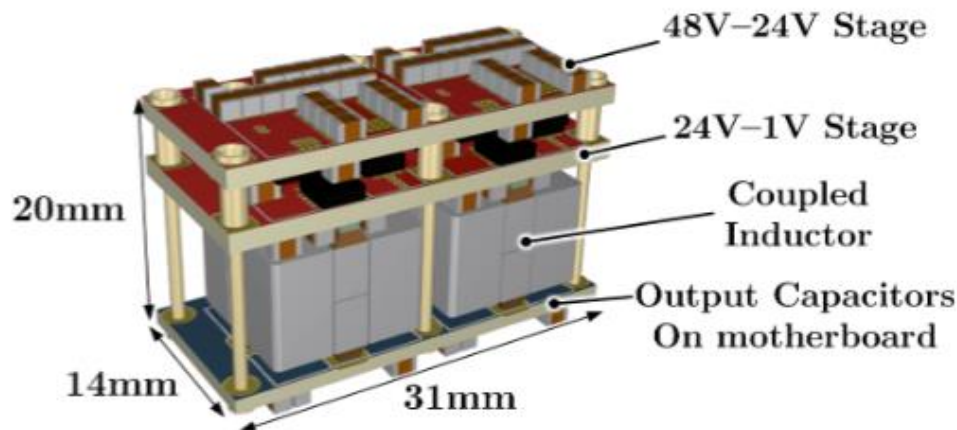
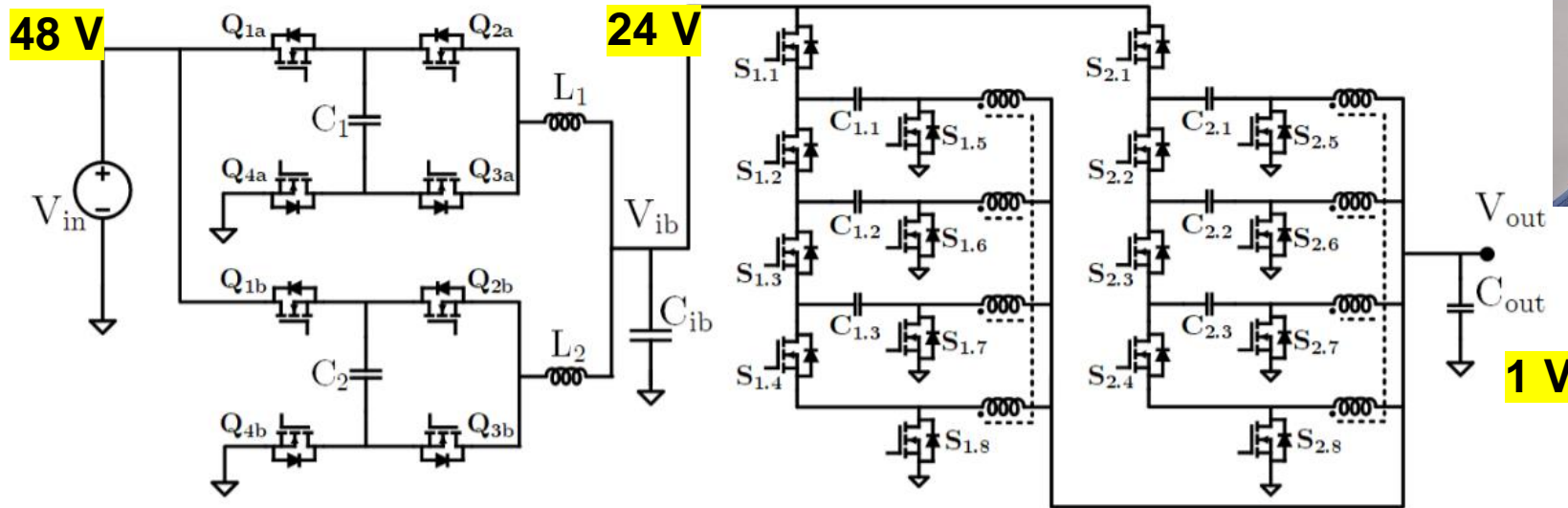
Y. Elasser



Other High Performance PoL Designs

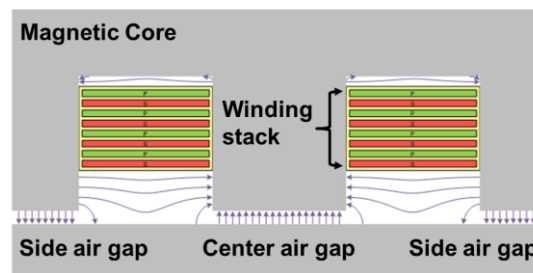
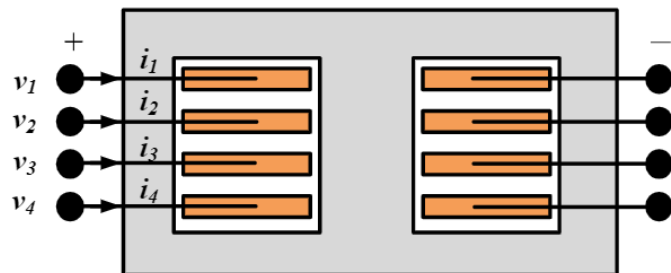


Y. Chen

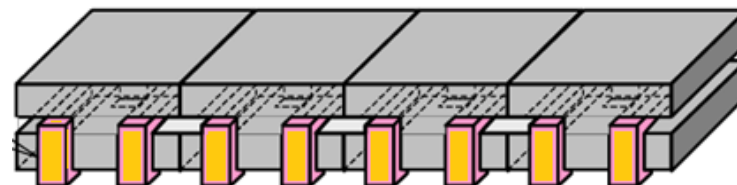
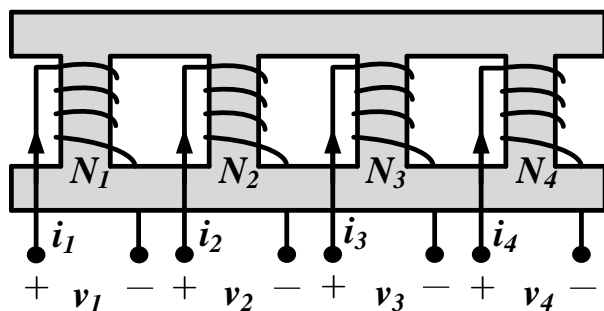


- Y. Chen, M. Chen et al., "Two-Stage 48V-1V Hybrid Switched-Capacitor Point-of-Load Converter with 24V Intermediate Bus," *COMPEL 2020*. **[Best Paper Award]**

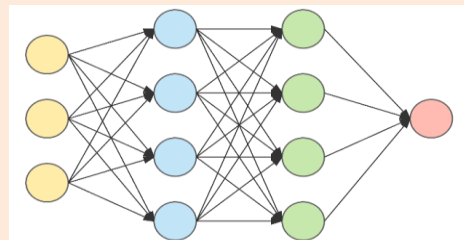
□ Design methodologies for series coupled structure (planar core)



□ Design methodologies for parallel coupled structure (ladder core)



□ Machine learning based magnetic core loss modeling methods



❑ **Generalized Steinmetz Equation (GSE)**

$$P_v = k f^\alpha \hat{B}^\beta \quad \text{three parameters, sine wave} \quad k, \alpha, \beta$$

❑ **Improved GSE (iGSE)**

three parameters, non-sine wave

$$P_v = \frac{1}{T} \int_0^T k_i \left| \frac{dB}{dt} \right|^\alpha (\Delta B)^{\beta-\alpha} dt \quad k_i, \alpha, \beta$$

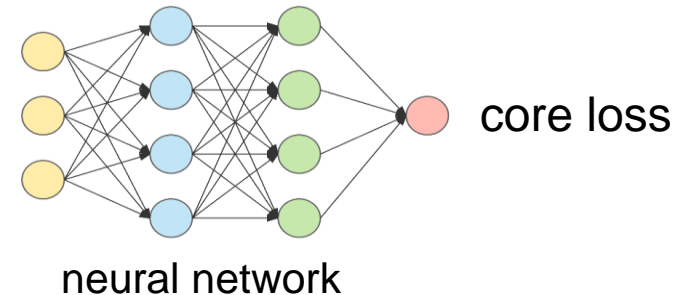
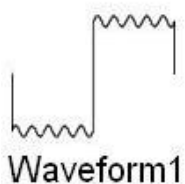
❑ **Improved – improved GSE (i²GSE)**

eight parameters, non-sine wave

$$P_v = \frac{1}{T} \int_0^T k_i \left| \frac{dB}{dt} \right|^\alpha (\Delta B)^{\beta-\alpha} dt + \sum_{l=1}^n Q_{rl} P_{rl} \quad k_i, \alpha, \beta, \alpha_r, \beta_r, k_r, \tau, q_r$$

❑ **Machine Learning based Methods**

lots of parameters automatically trained

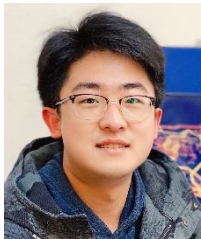
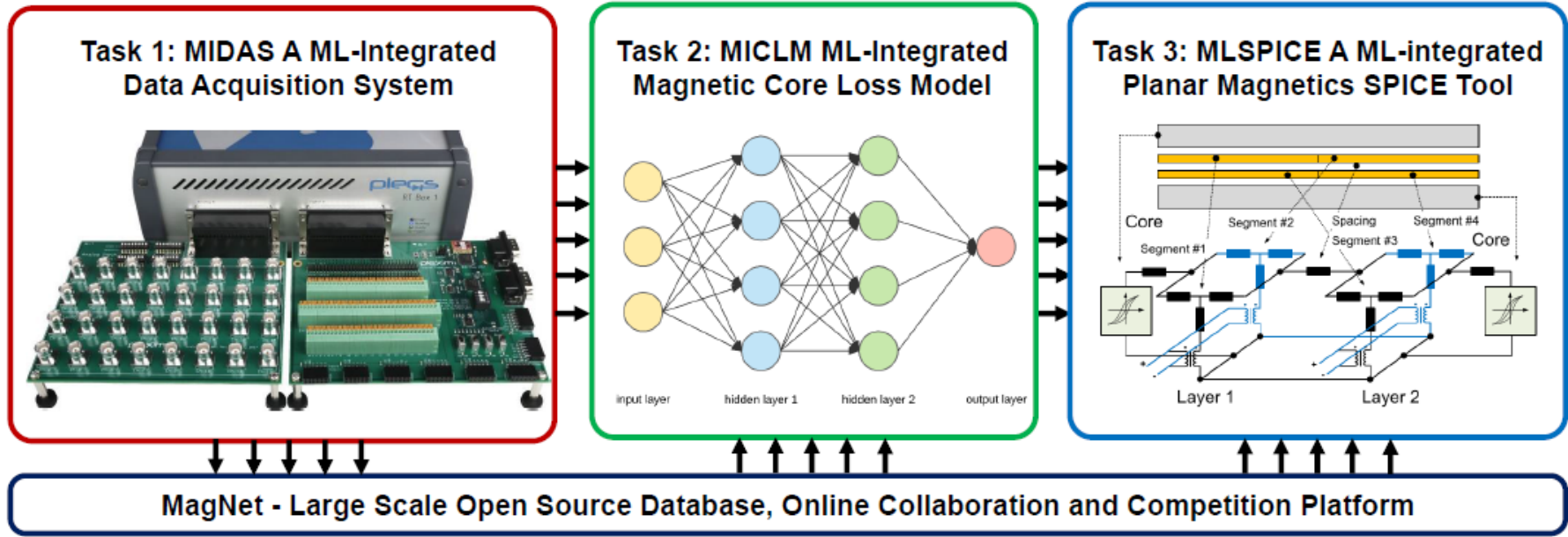


dc bias, temperature, memory effect, minor loops

Automatic Data Acquisition

Neural Network Training

SPICE Lumped Circuit



H. Li

Princeton
MagNet

Open source at:

GitHub

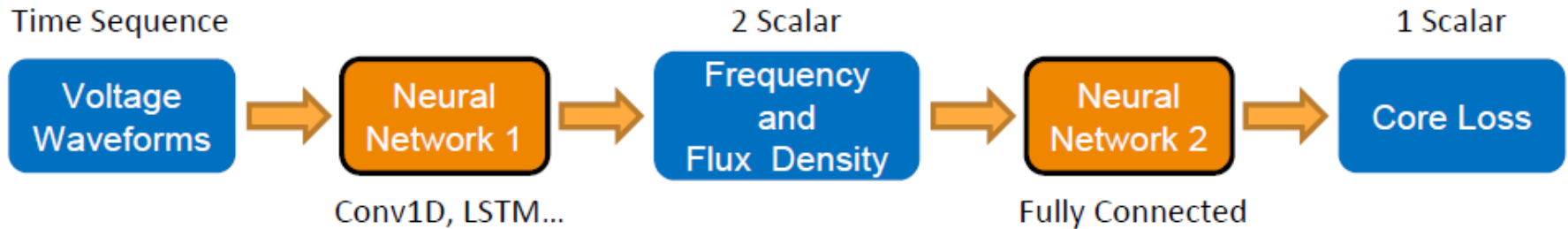


Dartmouth



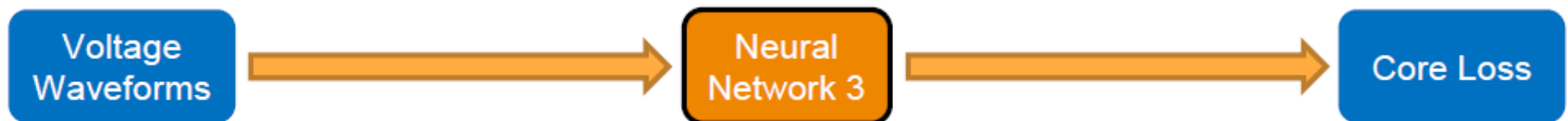
- H. Li, M. Chen et al. "MagNet: A Machine Learning Framework for Magnetic Core Loss Modeling," *COMPEL'20*.

- **Supervised learning: use ML to replace existing design steps**



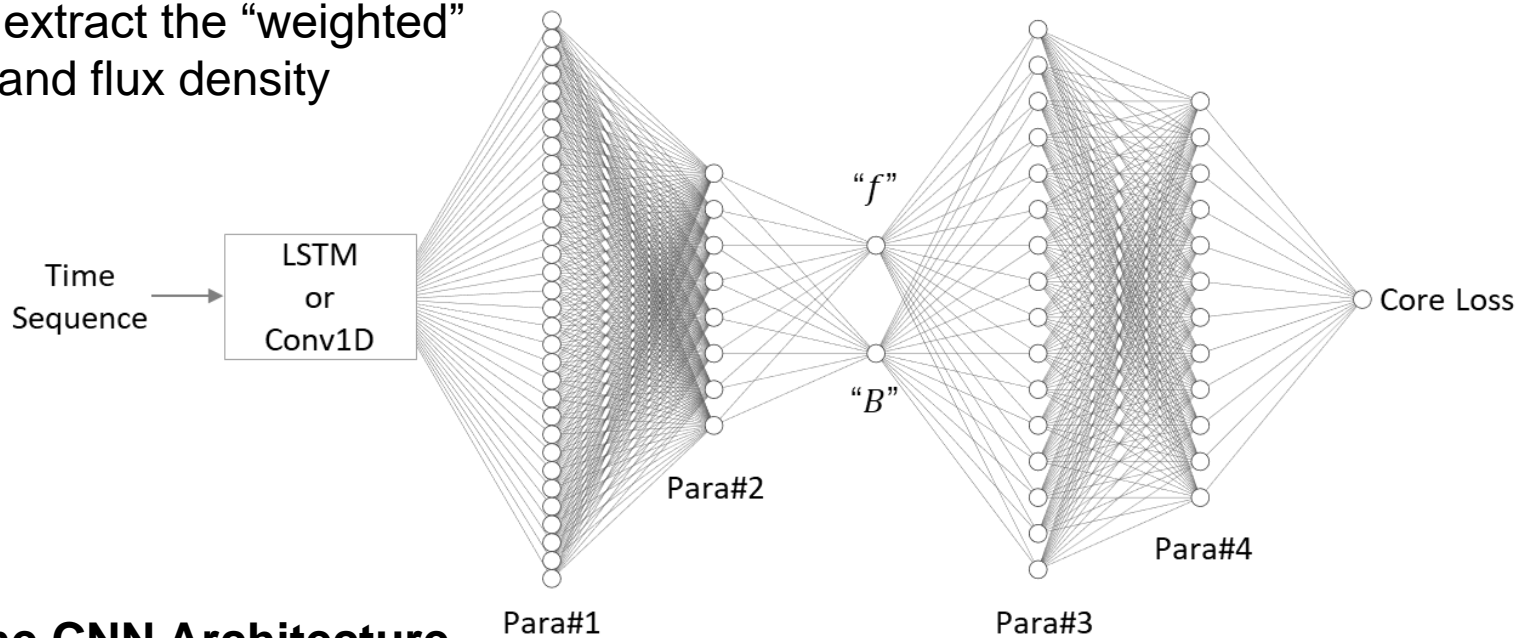
Limitation: constrained by existing knowledge on magnetic core loss

- **Unsupervised learning: end-to-end fully autonomous ML**

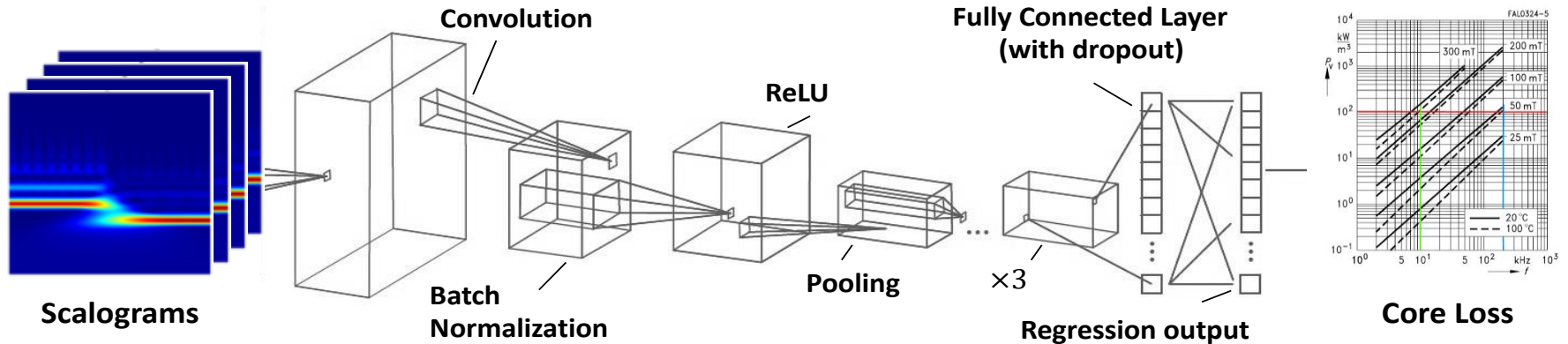


Limitation: all information hidden, hard to interpret the results

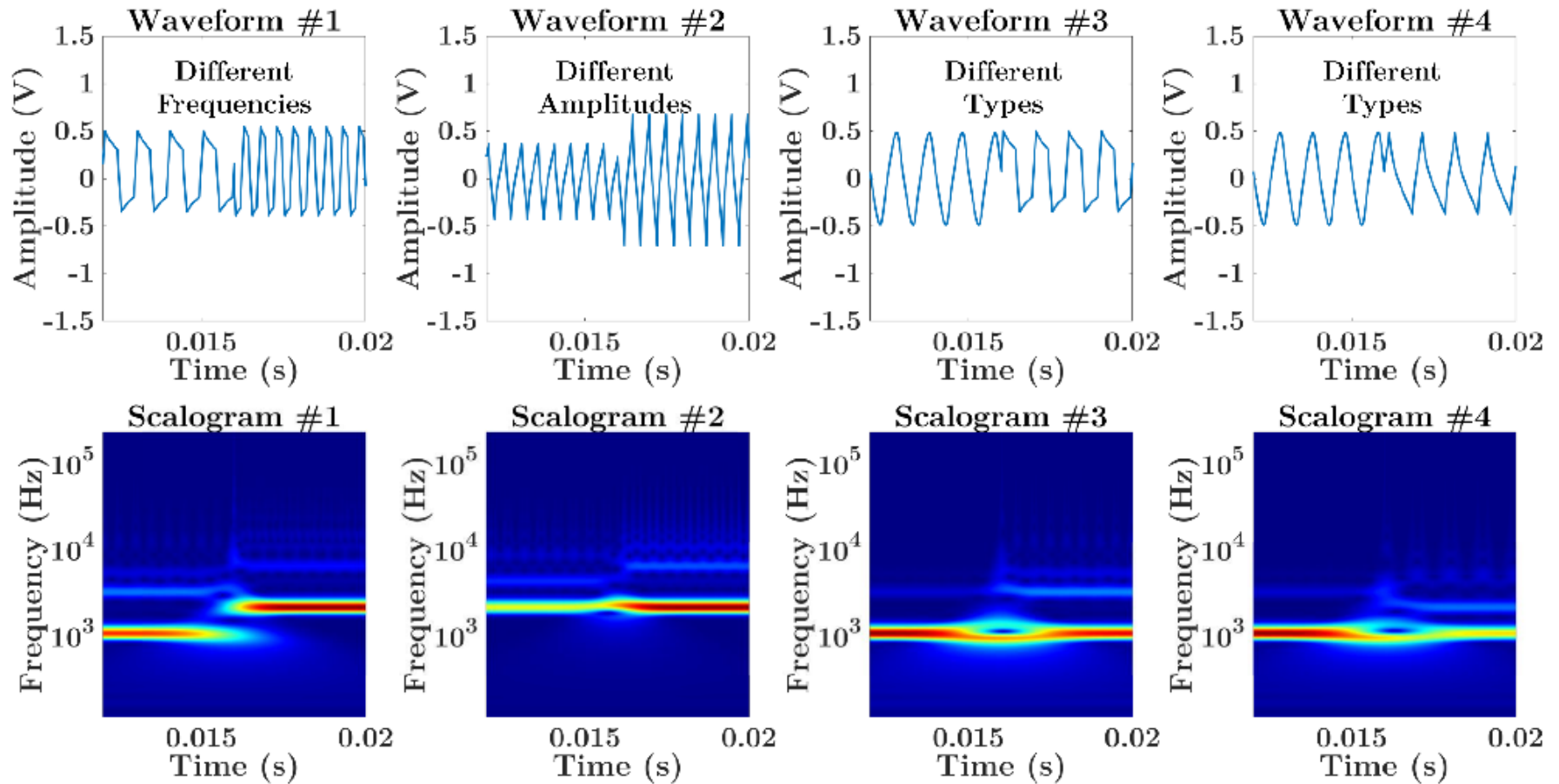
- Use ML to extract the “weighted” frequency and flux density



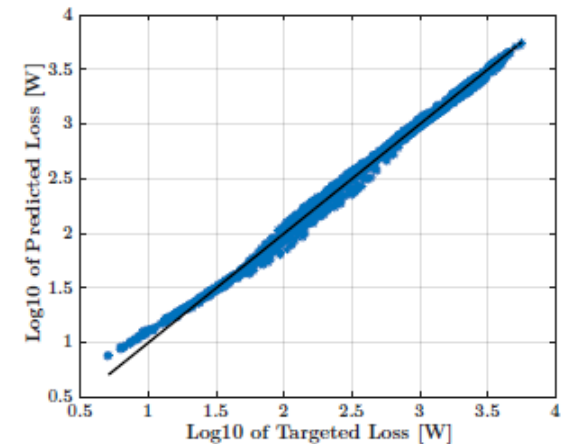
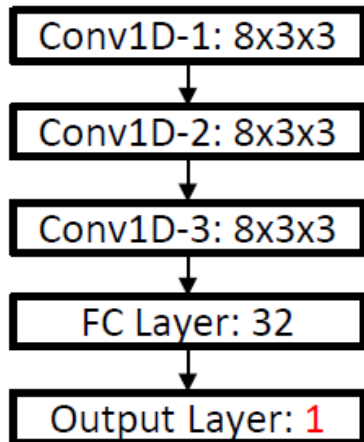
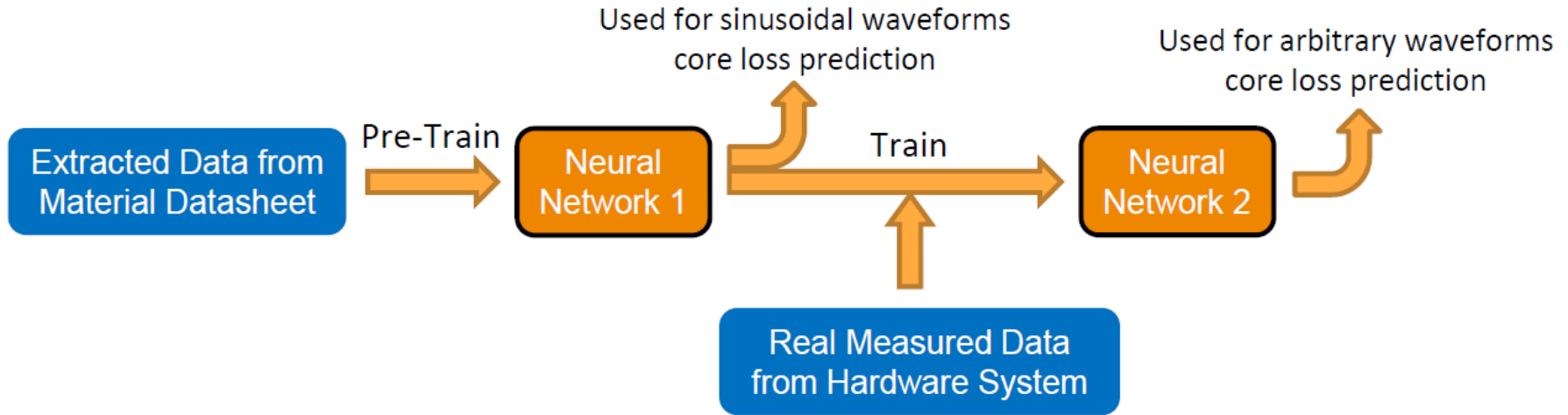
Optimizing the CNN Architecture



Example 2D Scalograms and CNN

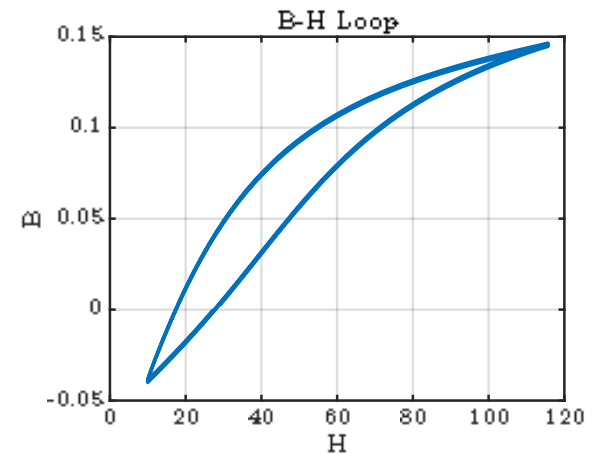
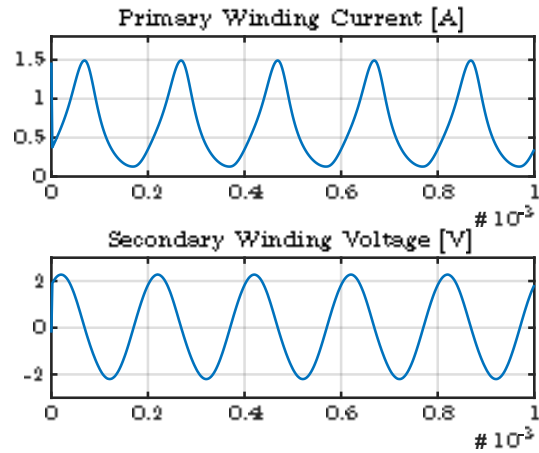
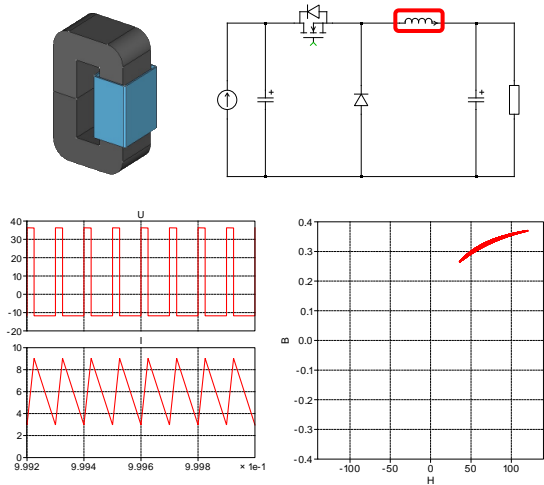


Overall Machine Learning Architecture



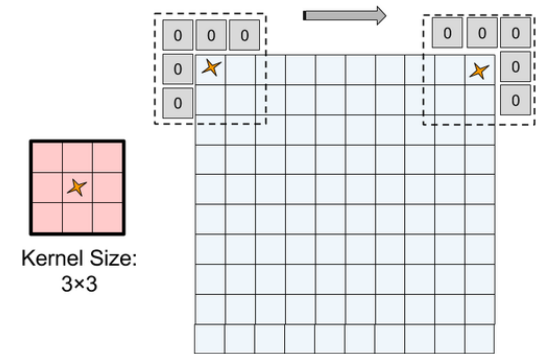
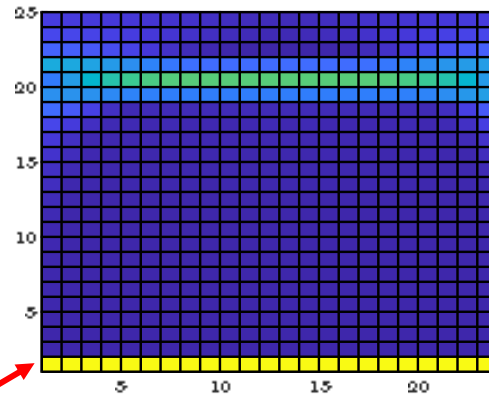
~2% average error for sine wave
~7% average error for arbitrary wave

Impacts of DC Bias on Core Loss

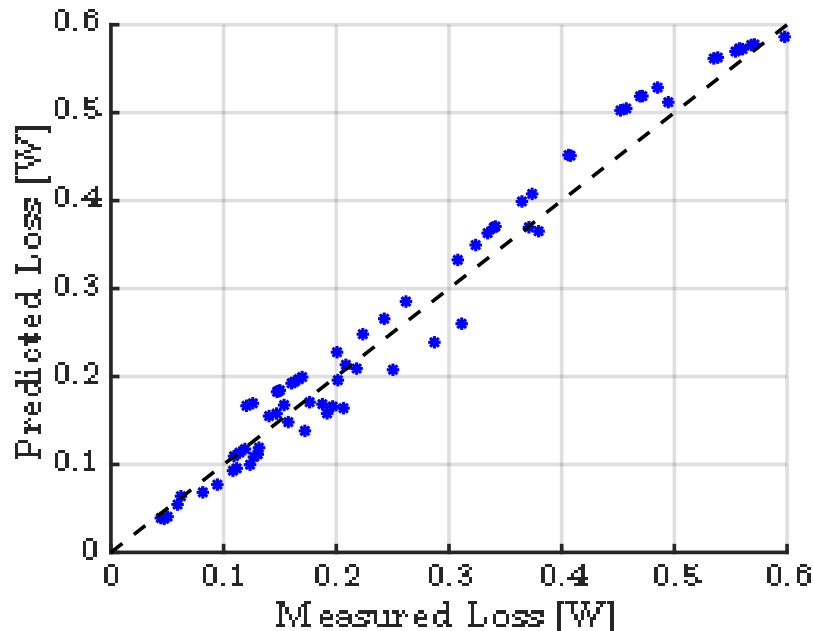


$$\text{scalogram} = \begin{bmatrix} \text{scalogram} \\ K \cdot \text{DC bias} \end{bmatrix}$$

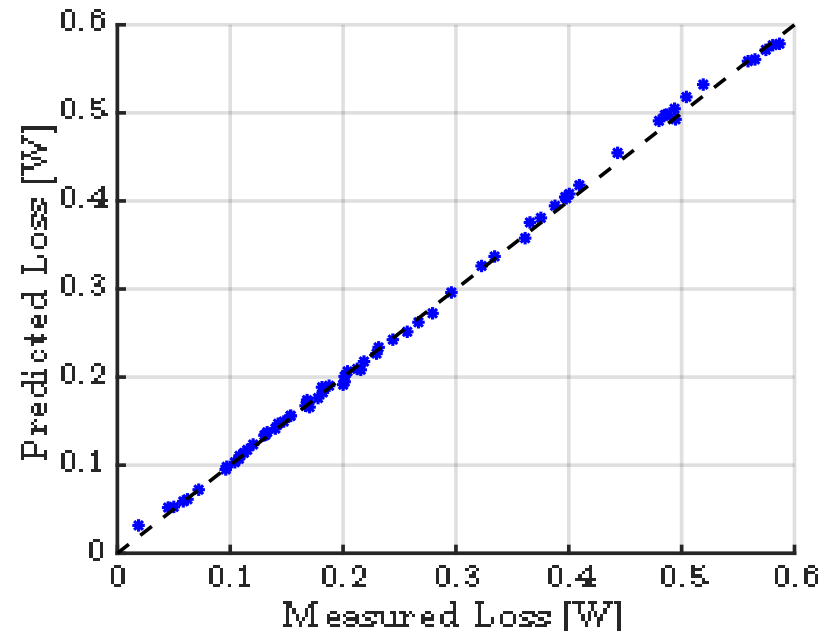
Modeling the dc bias



$$\text{scalogram} = \begin{bmatrix} \text{scalogram} \\ 0 \dots 0 \dots 0 \\ \text{DC bias} \end{bmatrix}$$



Before including the DC
bias information: 11.12%

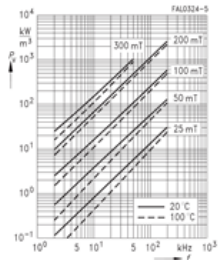


After including the DC bias information
by modifying the scalogram: 5.23%

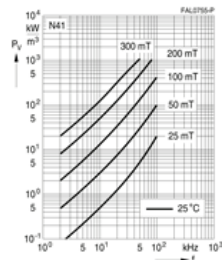
This is just scratching the surface of ML-based core loss modeling methods:
dc-bias, temperature, air gap, harmonics, degradation, etc...

Transfer learning method:

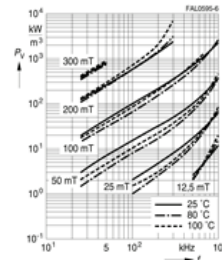
- Train a neural network architecture with data of material A
- Update the neural network parameters with **training data** of material B
- Test the model accuracy with **testing data** of material B



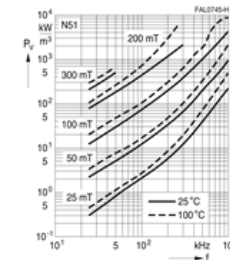
N27: 3.47%



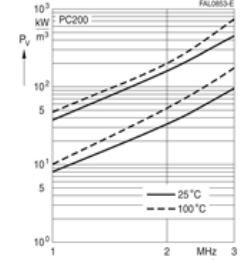
N41: 3.12%



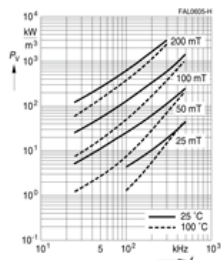
N49: 7.24%



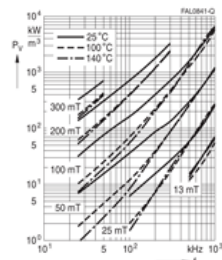
N51: 8.66%



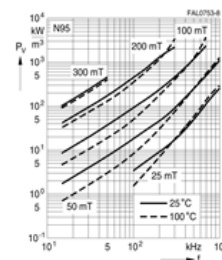
N59: 4.88%



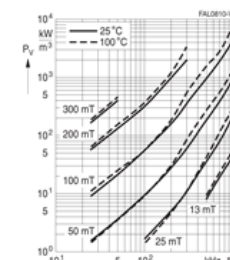
N87: 3.65%



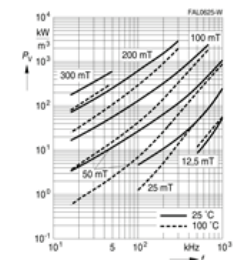
N88: 9.75%



N95: 9.02%

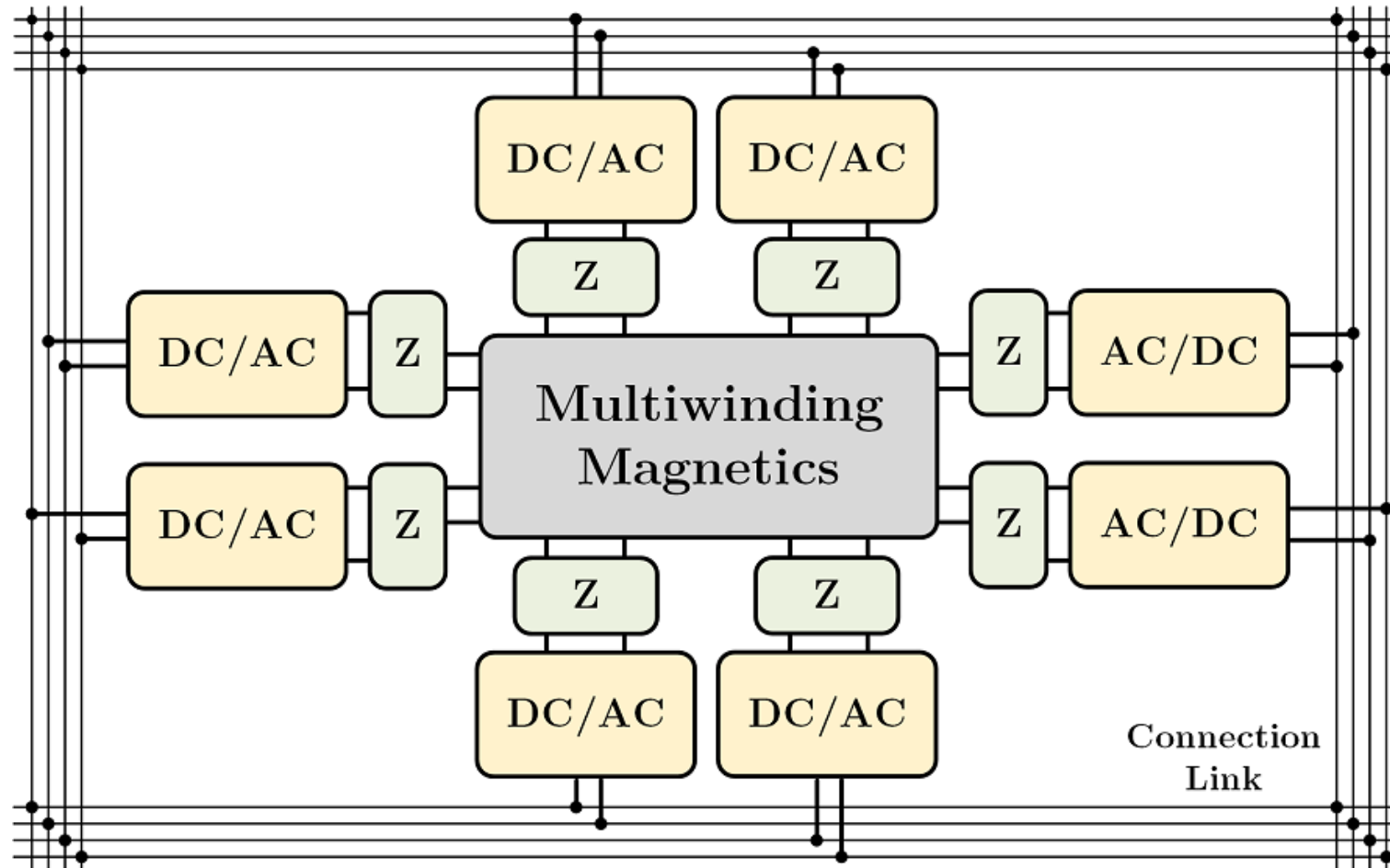


N96: 7.62%

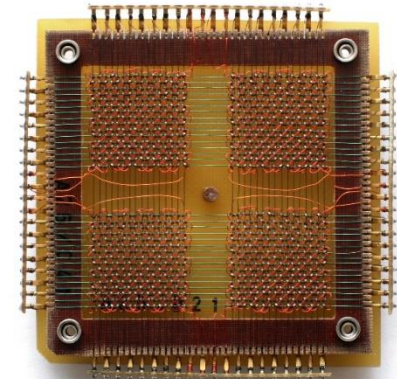
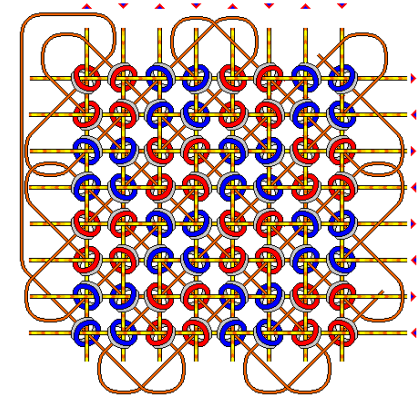
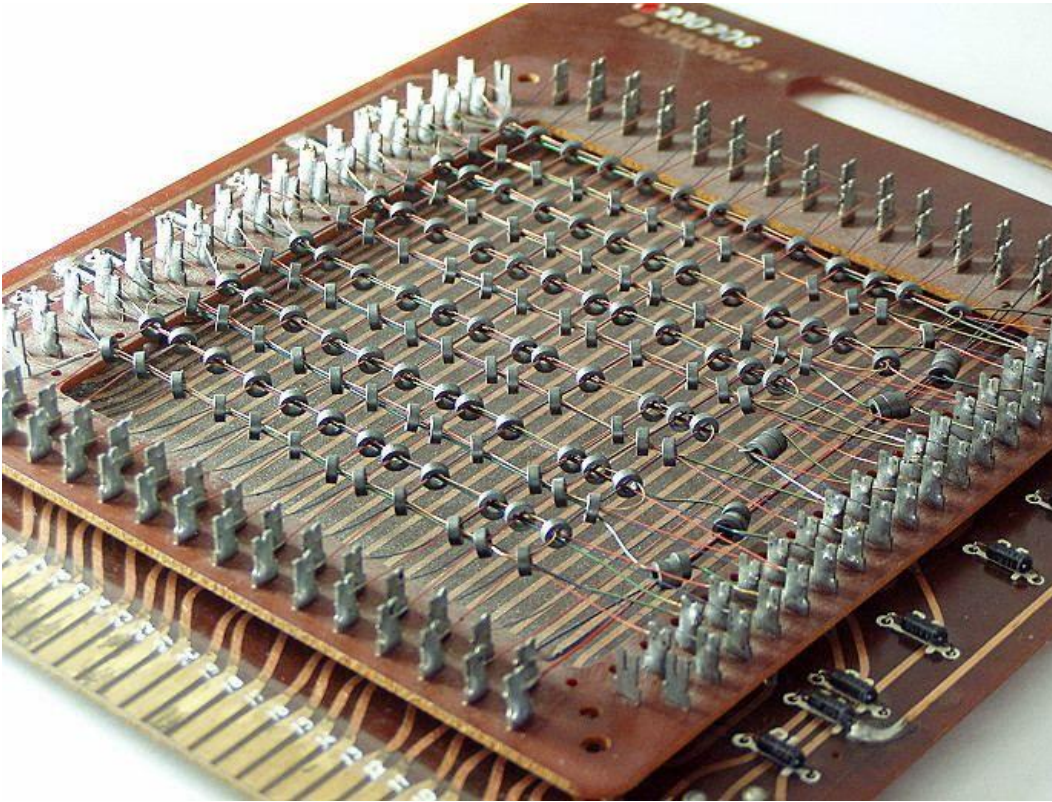


N97: 7.35%

Towards a MIMO Magnetic Energy Processor



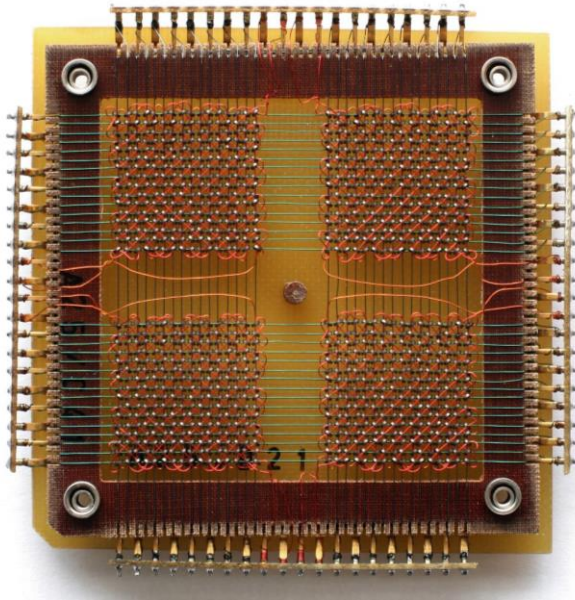
A Magnetic Register in 1960s (Memory)



- A 32 x 32 core memory storing 1024 bits of data
- Instead of processing information, we process energy

Emerging Opportunities for More Sophisticated Magnetics

Information Processor

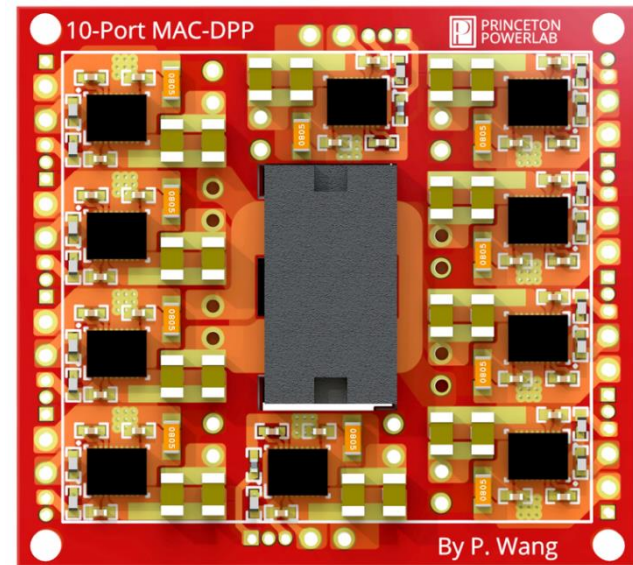


32 x 32 Magnetic Memory



10101
01010
10101

Energy Processor



10-Port MIMO Power Converter



- **Series Coupled Multiwinding Magnetics: Design Methodologies**

- M. Chen, M. Araghchini, K. K. Afridi, J. H. Lang, C. R. Sullivan and D. J. Perreault, "A Systematic Approach to Modeling Impedances and Current Distribution in Planar Magnetics," in *IEEE Transactions on Power Electronics*, vol. 31, no. 1, pp. 560-580, Jan. 2016.

- **Series Coupled Multiwinding Magnetics: Applications**

- M. Chen, S. Chakraborty and D. J. Perreault, "Multitrack Power Factor Correction Architecture," in *IEEE Transactions on Power Electronics*, vol. 34, no. 3, pp. 2454-2466, March 2019.
- Y. Chen, P. Wang, Y. Elasser and M. Chen, "Multicell Reconfigurable Multi-Input Multi-Output Energy Router Architecture," in *IEEE Transactions on Power Electronics*, vol. 35, no. 12, pp. 13210-13224, Dec. 2020.
- P. Wang, Y. Chen, J. Yuan, R. C. N. Pilawa-Podgurski and M. Chen, "Differential Power Processing for Ultra-Efficient Data Storage," in *IEEE Transactions on Power Electronics*, vol. 36, no. 4, pp. 4269-4286, April 2021.
- M. Liu, Y. Chen, Y. Elasser and M. Chen, "Dual Frequency Hierarchical Modular Multilayer Battery Balancer Architecture," in *IEEE Transactions on Power Electronics*, vol. 36, no. 3, pp. 3099-3110, March 2021.

- **Parallel Coupled Multiwinding Magnetics : Design Methodologies**

- Chen, Minjie; Sullivan, Charles (2020): Unified Models for Multiphase Coupled Inductors. TechRxiv. Preprint. <https://doi.org/10.36227/techrxiv.12477269.v4>
- D. Zhou, Y. Elasser, J. Baek, C. R. Sullivan and M. Chen, "Inductance Dual Model and Control of Multiphase Coupled Inductor Buck Converter," *IEEE 21st Workshop on Control and Modeling for Power Electronics (COMPEL)*, Aalborg, Denmark, 2020.

- **Parallel Coupled Multiwinding Magnetics: Applications**

- Y. Chen, D. M. Giuliano and M. Chen, "Two-Stage 48V-1V Hybrid Switched-Capacitor Point-of-Load Converter with 24V Intermediate Bus," *IEEE 21st Workshop on Control and Modeling for Power Electronics (COMPEL)*, Aalborg, Denmark, 2020.
- J. Baek, P. Wang, Y. Elasser, Y. Chen, S. Jiang and M. Chen, "LEGO-PoL: A 48V-1.5V 300A Merged-Two-Stage Hybrid Converter for Ultra-High-Current Microprocessors," *IEEE Applied Power Electronics Conference and Exposition (APEC)*, New Orleans, LA, USA, 2020, pp. 490-497.

- **Machine Learning Methods for Core Loss Modeling**

- H. Li, S. R. Lee, M. Luo, C. R. Sullivan, Y. Chen and M. Chen, "MagNet: A Machine Learning Framework for Magnetic Core Loss Modeling," *2020 IEEE 21st Workshop on Control and Modeling for Power Electronics (COMPEL)*, Aalborg, Denmark, 2020.